Technical Report

on the

Olympias Project

Au Pb Zn Ag Deposit, Northern Greece

European Goldfields Limited
Suite 200, Financial Plaza
204 Lambert Street
Whitehorse, Yukon
Canada Y1A 3T2

Patrick Forward
Vice President, Projects & Exploration FIMMM
Antony Francis
Senior Group Metallurgist, FIMMM
Neil Liddell
Senior Group Mining Engineer, MIMMM

14 July, 2011

CONTENTS

EUROPEAN GOLDFIELDS

TABLES

FIGURES

APPENDICES

1. SUMMARY

The Olympias project is a gold-lead-zinc-silver mine on care and maintenance in Northern Greece (Olympias Project) in which European Goldfields Limited (EGL) has an indirect majority interest of 95%. The company has a phased approach to developing the Olympias Project:

- The existing gold concentrates have all been marketed and in the current phase the existing Olympias process plant will be refurbished to process the existing tailings;
- The reprocessing of existing tailings whilst refurbishing and developing the existing underground infrastructure;
- The processing at Olympias of ore from underground producing gold, lead and zinc concentrates;
- A production ramp-up on completion of the underground connection to a new surface concentrator plant at a brown field site in the nearby Stratoni Valley allowing early rehabilitation of historic stockpiles and infrastructure in the Olympias Valley.

Exploration data quoted in this report was collected by the Olympias Project's previous owners, TVX Hellas SA (TVX). Inspection of the Quality Assurance and Quality Control (QAQC) data and original assay sheets by the authors of this report has confirmed the integrity of the data. The mineral resource and reserve estimates follow the Canadian Institute of Mining, Metallurgy & Petroleum (CIM) guidelines currently utilised by Canadian National Instrument 43-101 (NI 43-101), use current cost and financial factors in reserve definitions and can be viewed as current.

EGL's mineral properties in Northern Greece, which include the Olympias Project, are located in the Chalkidiki peninsula. The properties comprise a group of granted mining licences, covering 317 square kilometres (km^2), approximately 100 kilometres (km) east of Thessaloniki. The Olympias Project itself is located within mining concessions numbered F13 and F14 which have an overall area of 49.7 km^2.

The road network in the area is among the best in Northern Greece. The Olympias Project lies 9 km north-northwest of the company-owned Stratoni port and loading facility, along a paved road running parallel to the coast.

Power lines of 110-kilovolt (kV) capacity run directly to the site and water is available from inflow to the existing underground development. Skilled labour, some of whom worked on the mine historically is available in the village of Olympiada located about 1 km from the mine. The company owns the land on which all the existing and proposed mine infrastructure is located and this is sufficient to allow the future operation of the mine without further land acquisition.

The area is wooded with oak, beech and pine being the principal species, while inland there are vineyards and farmlands. The main farming products of the region are wines, honey, olives and oil. The Chalkidiki Peninsula climate is generally mild with limited rainfall. The terrain is characterised by hills rising to about 600 metres (m) above sea level with steeply incised valleys.

There is a long history of mining in the area dating back to the 4th Century BC. Modern-era mineral exploration in the Olympias area commenced in 1954. A ramp was started by the then owner of the property in 1970 and full production commenced at Olympias in the West orebody. During this period lead concentrates and zinc concentrate was sold and gold bearing pyrite / arsenopyrite concentrate was stockpiled. The stockpile of gold bearing pyrite / arsenopyrite concentrate has since been sold to off-takers by EGL. The historic recovery of gold bearing pyrite / arsenopyrite concentrate was inefficient and a significant quantity reported to the tailings management facility (TMF) adjacent to the mine. The owning company (Hellenic Fertilizer Company) went into receivership in 1991 though production continued.

TVX successfully won the bidding for the property in 1995 and, shortly afterwards, production at Olympias was suspended so that drilling could be conducted to confirm and expand the mineral resources. By February 1999, TVX had completed a drill programme comprising 760 holes totalling 91,319 m. A resource estimation completed in June 1998 was updated in December 1998 and again in 1999 to take account of all drilling completed to that date. In 1998 and 1999 Kvaerner Metals produced and then updated a feasibility study on the Olympias Project. During 1999-2000, SNC Lavelin of Toronto was commissioned to conduct a basic engineering study on the Olympias Project.

The Olympias polymetallic ore consists of stratabound replacement mineralisation hosted within marble horizons within the Serbo-Macedonian Massif and may be categorised as distal skarn type deposit whose emplacement relates to a tertiary intrusive to the southeast of the orebody. The deposit consists of massive sulphide, carbonate (marble) and aplite replacement lenses interlayed with biotite gneiss and schist. The majority of the orebody exhibits a north-south strike, with plunge to the southeast.

The sulphide ore comprises both undeformed massive sulphides and deformed sulphide ore with the latter characterised by brecciation, mylonitisation, folding and shearing. The most abundant ore minerals are pyrite, sphalerite, galena, arsenopyrite and minor chalcopyrite.

The mineralisation occurs within two orebodies. The West orebody is approximately 250 m wide and plunges 1,500 m to the southwest. The East orebody lies some 150 m east of the West orebody. Its width averages 75 m and its average thickness is 7 m. The east mineralisation has been traced for 600 m down plunge.

Only those holes drilled by TVX, since 1996, were utilised for resource estimation purposes as there is no means of validating those drilled by earlier operators. The orebody at Olympias is drilled on a nominal 25 m to 45 m spacing and is open down dip and along strike to the west. The drill orientation with respect to ore is variable since most of the holes were drilled in fans from mine infrastructure close to the orebody. All drilling for the current mineral resource estimate was conducted by TVX but the logs to the drilling and the sample QAQC have been validated by the author.

The company’s facility at the Stratoni laboratory was used for sample preparation. All samples were routinely assayed for gold, silver, lead, zinc and arsenic at accredited independent laboratories. A rigorous programme of QAQC was applied with duplicate core samples, duplicate core splits, duplicate pulp samples, duplicate assays, blanks and standards used throughout the programme. Following a detailed review of the documentation, including a review of the QAQC data, the author is satisfied that the sampling work was conducted to a high professional standard and that there is no significant bias in the sample database. The author is satisfied that the procedure in place at the time of drilling and the subsequent high standard to which material is preserved are indicative of a high level of sample security. The author has viewed the cores and has checked original assay certificates against database entries for repeats and standards as well as original assays. In the authors opinion the sample database is representative with no significant bias. Two audits carried out by independent authors at the time of the exploration corroborate this view.

Resource estimation was carried out in the following steps:

- Construct lithology geological solid models

- Composite drillhole samples into 1 m intervals
- Conduct basic statistics on both the raw and composite assay data sets
- Conduct geostatistical analysis for each element for each lithology
- Generate unconstrained three dimensional resource block models
- Validate the resource block model with primary data

Surface mineral resources are in the form of existing tailings from which gold bearing pyrite / arsenopyrite concentrates can be reclaimed. The mineral resources at Olympias can be summarised in Table 1-1.

Table 1-1 Updated Olympias Mineral Resources

	'000t	Au g/t	Au Moz	Ag g/t	Ag Moz	Pb %	Pb '000t	Zn %	Zn '000t
Measured Underground	8,137	10.0	2.60	147	38.5	4.9	400	6.6	535
Indicated Underground	4,298	10.0	1.39	161	22.3	5.4	230	7.1	304
Total M+I Underground	12,435	10.0	3.99	152	60.8	5.1	630	6.7	839
Measured Tailings	2,408	3.4	0.27	14	1.1	-	-	-	-
Total M+I	**14,843**	**-**	**4.26**	**-**	**61.9**	**-**	**630**	**-**	**839**
Inferred Underground Inside block model	793	12.4	0.32	179	4.6	5.9	47	6.8	54
Inferred Underground Outside block model	873	5.6	0.16	133	3.7	4.9	43	7.5	65
Total Inferred	1,666	8.9	0.47	155	8.3	5.4	90	7.2	120

Mineral Reserves are included in Measured and Indicated Mineral Resources.
Mineral Resources that are not mineral reserves do not have demonstrated viability.
Figures in the tables may not sum due to rounding.

As part of the phased approach, the rehabilitation of the existing concentrator plant to treat the existing tailings at up to 720,000 tonnes per annum (tpa) has commenced. The underground works are to be refurbished and developed and run of mine (ROM) ore will be processed at the Olympias concentrator once the tailings reserve is depleted. Ore production will reach 400 ktpa producing three concentrates for gold, lead-silver and zinc respectively. Production will be increased to 700 ktpa to 850 ktpa in year 9 on completion of an 8.5 km decline linking the underground works at Olympias to a new concentrator to be built in the Stratoni valley (the Stratoni Decline).

The process at both concentrators is broadly the same with efficiencies of process and most particularly scale incorporated at the newer site. The crushed ore will be transferred to the fine ore bin ahead of the rod mill and the secondary ball mill. The overflow from the hydro-cyclones classifier will be directed to the flotation circuit. The flotation section will produce three concentrates, firstly lead/silver; secondly zinc, and thirdly the gold bearing pyrite / arsenopyrite concentrate. Separation of the minerals into the three concentrates is achieved through a combination of pH control and conventional reagents for the depression and activation of the various mineral species. There is no long-term surface disposal requirement for the coarse tailings as, by removing approximately 20% of the material as fines, the remaining coarse tailings balance the underground backfill requirement. The fine tailings will be filtered and transported as filter cake to the Stratoni Tailings Management Facility (TMF). The facilities at Olympias include a water treatment plant. There is minimal risk associated with the concentrator process as the Olympias plant has operated successfully for many years in the past, producing concentrates within the set metallurgical parameters.

The recovery of the lead, silver, zinc and gold to their respective concentrates will be in the range +/- 90% based on previous operating history at Olympias. It is anticipated that with modern equipment and automated process control, the historical recoveries could be exceeded.

Previous mining at Olympias was in the West Orebody. The proposed mining will complete the mining of mineral reserves remaining in these areas, but mainly mining the fully explored down dip extension to the West Orebody and the unexploited East Orebody. There are 13.6 million tonnes (Mt) of proven and probable underground mineral reserves remaining in the Olympias mine which will support a maximum mining rate of approximately 850 ktpa in the later phase.

The chosen mining method is drift and fill based on the geotechnical conditions, environmental requirements and it was the method previously used in the mine and is currently used at EGL's nearby Stratoni operation. It is seen as a low risk method, given the companies experience in using it, and ensures there is no subsidence due to the use of cemented backfill.

The mineral reserves defined by the application of the above mining method can be summarised in Table 1-2.

Table 1-2 Updated Olympias Mineral Reserves

	'000t	Au g/t	Au Moz	Ag g/t	Ag Moz	Pb %	Pb '000t	Zn %	Zn '000t
Proven Underground	8,886	8.7	2.47	128	36.5	4.3	380	5.7	508
Probable Underground	4,686	8.7	1.32	140	21.2	4.7	219	6.2	288
Total underground	13,572	8.7	3.79	132	57.7	4.4	599	5.9	796
Proven Tailings	2,408	3.4	0.27	14	1.1	-	-	-	-
Total	15,980	-	4.06	-	58.8	-	599	-	796

Mineral Reserves are included in Measured and Indicated Mineral Resources.
Figures in the tables may not sum due to rounding.

Ore supply to the Olympias concentrator will commence at an annualised rate of approximately 400,000 tpa over the first four years. Ore production to the new Stratoni processing plant will commence at 700 ktpa in year nine for the first year and then increase to some 800 ktpa to 850 ktpa thereafter.

Based on this report's estimates of mineral resources and reserves of the Olympias deposit the authors conclude that there are sufficient mineral reserves currently defined to sustain an approximate 25 year mine life.

The mineral resources and reserves can be viewed as current and meet CIM and JORC (Joint Ore Reserves Committee) standards. The clean geological contact between high-grade sulphide ore and waste rock ensures that the mineral resources convert well to mineral reserves with the minimum loss of material.

The mining methods proposed are similar to those employed by EGL at the nearby Stratoni operation and therefore the parameters used for both the technical and economic evaluation of mineral reserves are well known and have little risk. The mineral reserve offers a high economic return at conservative metal prices and meets the company criteria for development.

Studies to date indicate that there are no environmental risks foreseen and that the Olympias Project will be a major employer in the region. The phased approach allows for the complete rehabilitation of the Olympias Valley after only 8 years of production, after which the surface infrastructure will be concentrated at the brown field site of the Stratoni Valley.

It should be noted that the financial analysis included in this report is made on the basis of sale of gold concentrates using a conservative return of 45% of the contained gold value net of transport and processing costs plus the sale of the base metal concentrate streams.

EGL has submitted an Environmental Impact Study (EIS) which has been recently approved and includes a gold plant using the flash smelting route to process the gold bearing pyrite / arsenopyrite concentrates once full ramp up is achieved. It is the intention of the company to investigate the viability of this process route with future testwork and engineering studies. The implementation of a gold plant could be brought forward by stockpiling of gold concentrate or if additional ore streams are produced from deposits currently being explored in the area. The current level of testwork and engineering of flash smelting for this application does not provide capital and operating costs within a sufficiently accurate range to allow inclusion in this evaluation but it is noted that testwork to date has indicated recoveries of more than 90% gold. It is also noted that off-takers for the Olympias gold bearing pyrite / arsenopyrite concentrate in the past included smelters and a recent trial on Olympias gold concentrate by a potential off-taker using copper smelting technology also showed excellent recovery, reflected in terms of 97% plus payability.

A discounted cash flow with the current 25% corporate tax rate decreasing to 20% by 2014 in increments of 1%, (no royalties apply under the contract with the state that governs the Olympias Project) of the Olympias Project gives a post tax internal rate return of greater than 35% and therefore meets the company criteria for a viable project.

In line with EU directives, and to ensure that they remain appropriate to the operations, EIS approvals in Greece are refreshed every five years to reflect prevailing conditions such as new mineral resources, metal prices, employment levels, etc. Accordingly, this presents an opportunity, at that time, for EGL to re-assess the extraction approach, so as to ensure that in the context of the then prevailing conditions and the best available techniques are applied for the remainder of the mine life.

With the estimates of mineral resources and reserves of the Olympias deposit detailed in this report, the authors conclude that there are sufficient mineral reserves currently defined at the Olympias operation in order to sustain an approximate 25 year mine life and as such this report has met its objectives.

Mine life could be extended by in-fill drilling of the inferred mineral resources. Furthermore the planned decline from the Olympias deposit to the Stratoni mine site passes through a corridor of ground which is highly prospective.

The mineral resources are based on an extensive programme of diamond drilling. The programme of QAQC was well run and confirmed that there were no significant biases in the data. Drill spacing is sufficient to allow a high level of confidence in the geological interpretation. The resource block interpolation has been the subject of several audits and has been found to be robust and the kriging profiles correct. The mineral resource and reserve estimate can be viewed as current and meets CIM and JORC standards.

The mining methods proposed are similar to those employed by EGL at the nearby Stratoni operation and therefore the parameters used for both the technical and economic evaluation of mineral reserves are well known and have little risk. The reserve offers a high economic return at conservative metal prices and meets the company criteria for development.

The phased approach proposed by EGL has been endorsed by the Greek State in the recent approval of an EIS for all EGL's projects in Northern Greece.

Studies to date indicate that there are no environmental risks foreseen and that the Olympias Project will be a major employer in the region. The phased approach allows for the early rehabilitation of the Olympias Valley after only 8 years of the Olympias Project, after which the surface infrastructure will be concentrated at the brown field site of the Stratoni Valley.

Key parameters from the project are as follows:

Table 1-3 Key Cash flow Parameters

	Units	Life of Mine	Average
Olympias			
ROM production	kt	**13,573**	**543**
ROM production Au grade	g/t	**8.70**	**8.70**
ROM production Ag grade	g/t	**132.35**	**132.35**
ROM production Pb grade	%	**4.42**	**4.42**
ROM production Zn grade	%	**5.89**	**5.89**
Au Contained in Concentrate	k oz	**3,629**	**145**
Ag Contained in Concentrate	k oz	**53,313**	**2,133**
Pb Contained in Concentrate	kt	**542**	**22**
Zn Contained in Concentrate	kt	**727**	**29**
Operating Costs	USD m	**1,005.3**	**40.2**
Capital Costs	USD m	**388.8**	**15.6**
Net Revenue (1)	USD m	**3,614.2**	**144.6**
Undiscounted Operating Income	USD m	**2,608.9**	**104.4**
Discounted cash flow @5%	USD m	**1,040.4**	**41.6**

The cash flow for the Olympias Project gives a post tax internal rate return of greater than 30% and therefore meets the Company criteria for a viable project. Payback is achieved in year 6 of the operation but is a flawed measure of the returns on the project due to the phased development of the project. Returns are expected to be considerably improved with the implementation of gold processing, currently scheduled in year 9, but which could be brought forward if gold concentrate is stockpiled or alternative streams are produced as a result of exploration in the area which is currently underway. The Olympias Project is therefore sufficiently robust to progress to the basic engineering and implementation phase.

It is recommended that additional drilling is carried out within the inferred mineral resource and further along strike to the south and down plunge where the deposit is open in order to extend the mine life of the Olympias Project.

Further engineering work is needed to provide an estimate of costs for a gold concentrate processing plant which will add further value to the project and it is recommended that the required testwork and engineering studies for a flash smelting route be conducted as soon as possible.

2. INTRODUCTION

The Olympias Project is a gold-lead-zinc-silver massive sulphide mine in Northern Greece in which EGL currently has an indirect majority interest of 95%. This report was prepared for EGL by its employees and its primary objective is to present current mineral resources and mineral reserves for the Olympias Project in accordance with the CIM code based upon current and historic exploration data. EGL is a mining, development and exploration company listed on the Toronto and London AIM stock exchanges with operations in Greece

Mineral resources are presented on the basis of existing drillhole data dating from the late nineties, plus mapping and knowledge built up during the mine's period of operation between 1974 and 1994. Current mineral reserves are presented on the basis of realistic long-term metal prices and a cut-and-fill mining operation which will be developed in phases by EGL's local subsidiary, Hellas Gold SA (Hellas Gold).

The Qualified Person with responsibility for the overall preparation of this report and specifically sections covering Summary, Introduction, Reliance on Other Experts, Property Description and Location, Accessibility, Climate, Local Resources, Infrastructure and Physiography, History, Geological Setting and Mineralisation, Deposit Types, Exploration, Drilling, Sample Preparation, Analyses and Security, Data Verification, Mineral Resource Estimates, Market Studies and Contracts, Environmental Studies, Permitting and Social or Community Impacts, Capital and Operating Costs, Financial Analysis Adjacent Properties, Other Relevant Data and Information, Interpretation and Conclusions, Recommendations and References is Mr Patrick Forward, BSc (Mining Geology), FIMMM, who is an employee of EGL. Mr. Forward also co-authored the Project Infrastructure section with Mr. Liddell. Patrick Forward is a geologist with 19 years experience in the mining and exploration industry and has been involved in the design and implementation of exploration programmes and estimation of mineral resources for the past 15 years. Mr Forward has visited the site frequently from November 2004 to the date of this report and has spent approximately 20% of his time based there during this period. During this time Mr Forward has had access to all results, drill core, plans, sections, mining data, reports and personnel on the site.

The Qualified Person with responsibility for the reporting of Mineral Processing and Metallurgy and Recovery Methods is Mr Antony Francis, CEng, BSc (Eng) (Metallurgy), FIMMM, who is an employee of EGL. Tony Francis is a metallurgist with 38 years experience in the mining industry and has been involved in the design and construction of process plants on various projects during the past 38 years. Mr Francis has visited site on numerous occasions between April 2004 and the date of this report. During these visits Mr Francis has had access to all reports and results from the plant operations.

The Qualified Person with responsibility for the reporting of Mineral Reserve Estimates and Mining Methods is Mr Neil Liddell, CEng, BSc (Mining Engineering), MIMMM, who is an employee of EGL. Mr. Liddell co-authored the Project Infrastructure section with Mr. Forward. Neil Liddell is a mining engineer with 36 years experience in the mining industry and has been involved in the operation, design and construction of mines on various projects during the past 36 years. Mr Liddell has visited site on numerous occasions between July 2007 and the date of this report and has spent approximately 30% of his time based there during this period. During these visits Mr Liddell has had access to all reports and results from the operations.

3. RELIANCE ON OTHER EXPERTS

Exploration data quoted in this report was collected by the Olympias Project's previous owners, TVX Hellas. In the author's opinion and based on examination of core and data, the historic work was conducted professionally to industry standards. Inspection of the QAQC data and original assay sheets has confirmed the integrity of the data. The mineral resource and reserve estimates follow the CIM guidelines currently utilised by Canadian National Instrument 43 101 – Standard of Disclosure for Mineral Projects (NI 43-101), use current cost and financial factors in the reserve definition and can be viewed as current.

4. PROPERTY DESCRIPTION AND LOCATION

EGL's mineral properties in Northern Greece, which include the Olympias Project, are located in the Chalkidiki peninsula. The properties comprise a group of granted mining licences, covering 317 km^2, approximately 100 km east of Thessaloniki (Figure 4-1). The area is centred on coordinates 478,650E and 4,492,600N of the Hellenic Geodetic Reference System HGRS '87, (approximately Latitude 40° 35'10" and Longitude 23°44'50").

The group of properties includes the Olympias Project, which is a mine currently on care and maintenance, the Madem Lakkos and Mavres Petres Mines (collectively Stratoni), which are currently in production and the Skouries copper-gold porphyry deposit.

The Olympias Project itself is located within mining concessions numbered F13 and F14 (highlighted on Figure 4-1) which have an overall area of 49.7 km^2. The concessions were granted until 6th March 2026 and can be renewed a further two times for durations of 25 years each. No expenditure is required to keep the concessions. No royalty is payable on future production. In order for production to commence an environmental permit is needed following submission and acceptance of an EIS to the Greek Authorities and an operating permit following submission and acceptance of a technical study to the Greek Authorities. EGL has recently received the approval of the EIS.

The concessions give all mineral rights and in addition the company owns the land containing the entire surface infrastructure associated with the Olympias Project and this is sufficient to allow the future operation of the mine without further land acquisition.

The contract between the Greek state and EGL's subsidiary Hellas Gold stipulates that Hellas Gold is not liable for any historic environmental liabilities.

The Olympias Project was acquired from the Greek state in 2004 by Hellas Gold. EGL holds a controlling interest of 95% in Hellas Gold, who in turn holds a 100% interest in the Olympias Project.

At the time of writing the authors are not aware of any factors which will affect access to title or right and ability to perform work on the property.

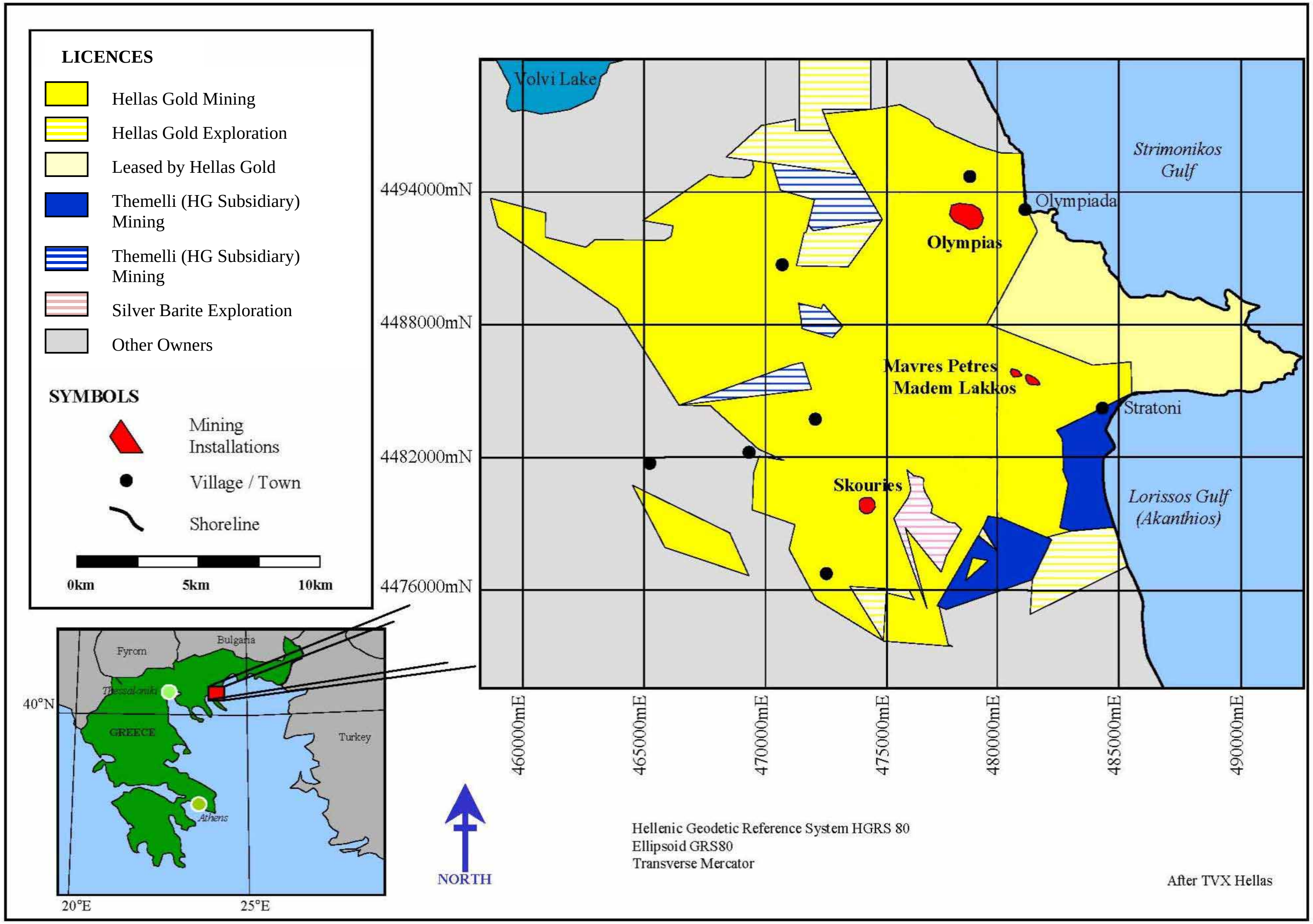


Figure 4-1 Kassandra Location and Property Map

5. ACCESSIBILITY, CLIMATE, LOCAL RESOURCES, INFRASTRUCTURE AND PHYSIOGRAPHY

The Olympias Project lies in the Chalkidiki Prefecture about 100 km by road from Thessaloniki, the second largest city in Greece, which has its own airport. It is readily accessible by car and bus, with regular bus schedules. The road network in the area is among the best in Northern Greece and a major highway has been constructed extending east from Thessaloniki to 15 km north of the property. The Olympias Project lies 9 km north-northwest of the company owned Stratoni port and loading facility, along a paved road along the coast.

The area is wooded with oak, beech and pine being the principal species, while inland there are vineyards and farmlands. The main farming products are wines, honey, olives and oil. The terrain is characterised by hills rising to about 600 m above sea level with steeply incised valleys.

The Chalkidiki Peninsula climate is generally mild with limited rainfall. Over 300 days or around 3,000 hours of sunshine are recorded on average annually. Average temperatures have limited fluctuations during the year. The lowest temperatures occur during December to February ranging between 3.5°C to 19°C, while highest temperatures occur during summer months ranging between 23°C and 34°C. Temperatures below 0°C are limited to the mountainous areas.

The area is well served by main 110 kV power supplies via the Public Power Corporation (PPC) with power supply right to the mine site. Communications are good. Telephone and broadband are available in the area and Hellas Gold has the original microwave phone link at Stratoni giving additional access to broadband data communications. There is sufficient water available to support the operation from creeks, re-circulated clean water from milling operations and high groundwater levels.

Water is available from ingress to the existing underground development, which is currently pumped to surface. Skilled labour, some of whom worked on the mine historically is available in the village of Olympiada which is located about a kilometre from the mine. Other nearby villages also have a pool of skilled and semi skilled labour available. The company owns the land on which all the existing and proposed mine infrastructure is located and this is sufficient to allow the future operation of the mine without further land acquisition.

The mine site comprises mine offices and change house, trackless decline, shaft, underground development, mill and flotation plant (Figure 5-1).

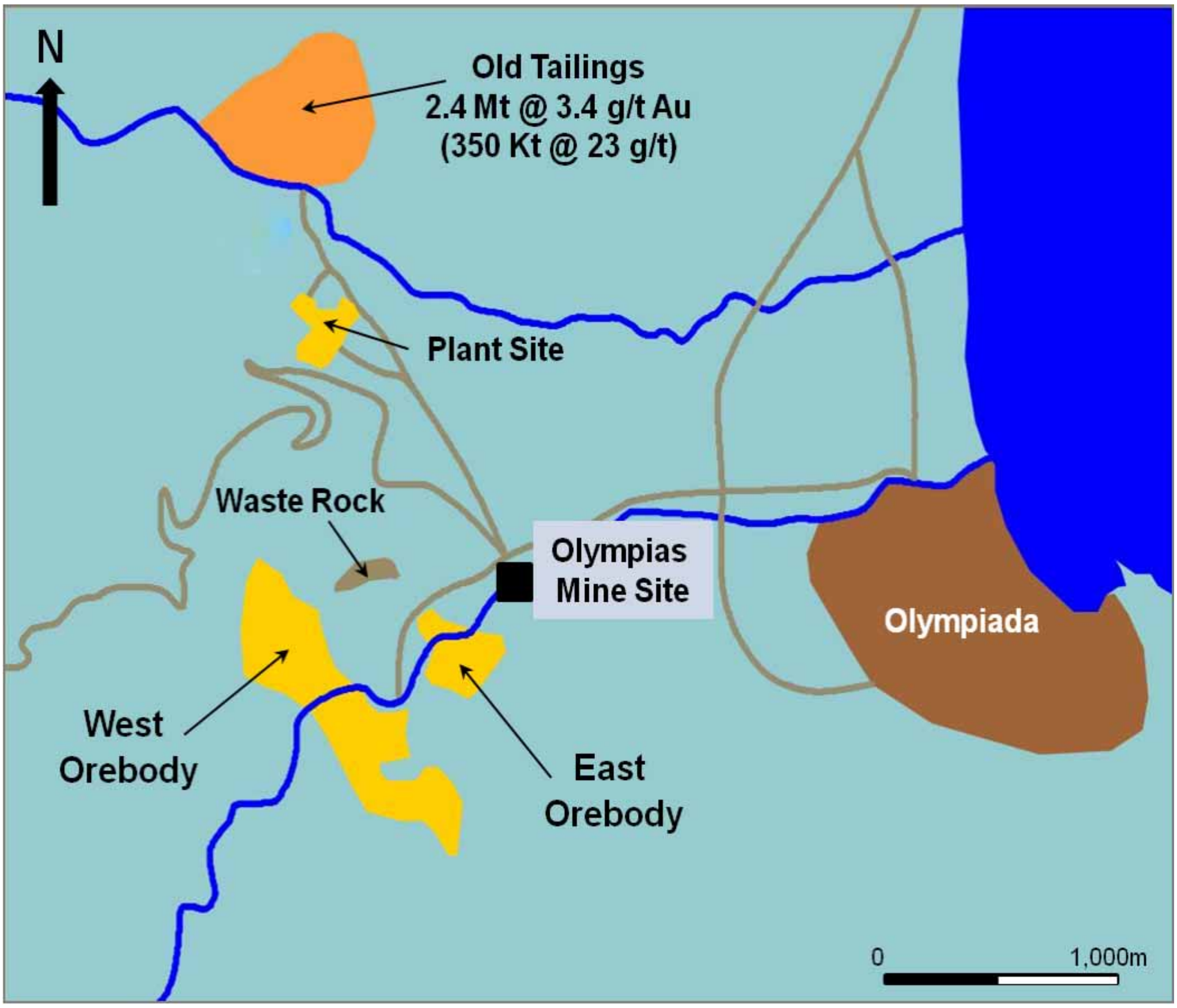


Figure 5-1 Olympias Site Layout Schematic

6. HISTORY

There is a long history of mining in the Kassandra area. Ancient mining reached a peak during the time of Phillip II and Alexander the Great, at which time silver and gold financed their conquests of the then known world during the 4th century BC. It is believed that by 300 BC, the bulk of the ores above the water table at the Olympias Project had been extracted, though the nearby Stratoni mine continued to be exploited through the Roman, Byzantine and Turkish periods.

In 1933, a shaft was sunk to 74 m depth at Olympias by the then owners, with lateral development to intersect a marble/gneiss contact. The drift encountered ancient workings which were largely exhausted.

In 1954, the owners commenced exploration in the Olympias area. Their drilling encountered numerous discontinuous lenses of sulphide mineralisation 10 cm to 20 cm in width, and many old workings were intersected. In 1965, further drilling commenced and in 1966 a 10 m intersection of lead-zinc mineralisation was encountered 20 m below the 1933 shaft, which proved to be exploitable.

By the early 1970's ownership of the mines had transferred to the Hellenic Fertilizer Company. A ramp was started in 1970 and full production commenced in the West orebody. From 1974 to 1984 the shaft was sunk to the –312 m below mean sea level (MSL) level and high grade mineralisation, termed the East orebody was intersected at –254 m MSL. The first ten years of production proved highly profitable when sub-level caving could be used, but excessive dilution, ground subsidence and problems with water influx resulted in a change to more expensive drift and fill mining. During this period lead concentrates and zinc concentrate was sold and gold bearing pyrite / arsenopyrite concentrate was stockpiled. The stockpile of gold bearing pyrite / arsenopyrite concentrate has since been sold to off-takers by EGL.

The Hellenic Fertilizer Company went into receivership in 1991 and the Government subsidised the operation until development and production fell behind schedule. Following three separate international auctions, TVX successfully won the bidding in 1995 and shortly afterwards, production at the Olympias Project was suspended so that drilling could be conducted to confirm and expand the mineral resources. Extraction had been from all levels between –32 m to –218 m MSL. The main ramp had reached a depth of –230 m and the lowest developed level was –228 m. From 1976 to 1995, records indicate that some 3.64 Mt of ore were mined, though grades are not available. However, between 1987 and 1995, records indicate that 970,150 t had passed through the mill with average feed grades of 8.19 g/t Au, 126.64 g/t Ag, 3.90% Pb, 5.63% Zn, 16.79% S, 3.49% As, 13.97% Fe and 0.17% Sb. Production prior to 1996 was carried out by different means to that proposed by EGL and without gold revenue and therefore historic mineral resources and reserves are not seen as relevant to this report which incorporates current estimates.

By February 1999, TVX had completed a drill programme comprising 760 holes totalling 91,319 m. A resource estimation completed in June 1998 was updated in December 1998 to take account of all drilling completed to that date. In 1998 and 1999, Kvaerner Metals produced and then updated a feasibility study on the Olympias Project. During 1999-2000, SNC Lavelin of Toronto was commissioned to conduct a basic engineering study on the Olympias Project. Previous historic mineral resource and reserve estimates from the TVX period considered different processing routes from those proposed here and therefore it is not considered to be appropriate to reproduce them here.

Figure 6-1 below shows the existing and proposed Olympias mine infrastructure.

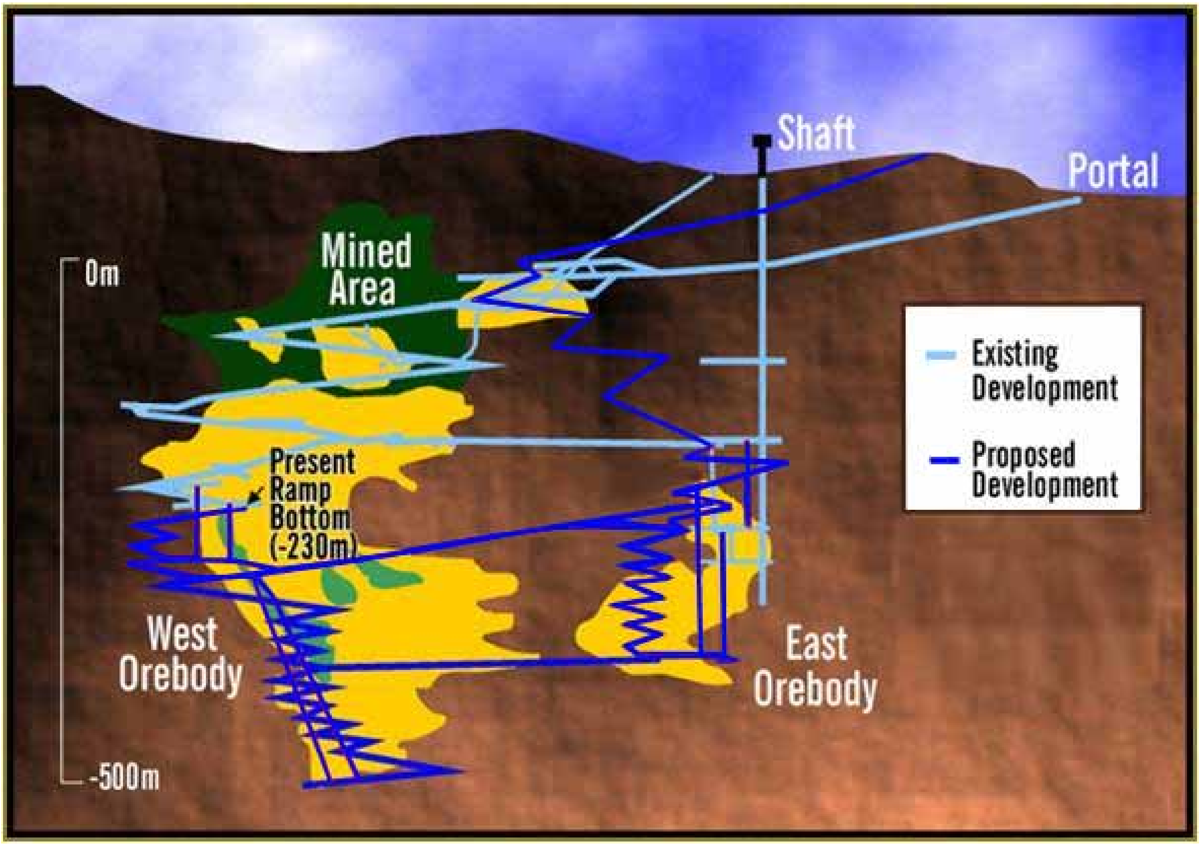


Figure 6-1 Olympias Mine Underground Infrastructure Schematic

7. GEOLOGICAL SETTING AND MINERALISATION

7.1. REGIONAL GEOLOGY

The tectonic structure of Greece consists of elongated tecto-magmatic belts of variable metamorphic grade which trend northwest to southeast. These broadly coincide with the trend of the main mountain ranges of the country. These zones represent successive episodes of subduction, resulting from the northeast movement of the African plate during the Tertiary period. The rocks that comprise these orogenic zones consist of gneiss, schist and acid igneous intrusives. These rocks host the mineral deposits of the Kassandra Mining District.

Three main geotectonic units, following the same trend dominate northeastern Greece; the Rodope massif to the east, the Serbo-Macedonian massif and the Vardar Zone to the west (Figure 7-1). The Rodope and the Serbo-Macedonian massifs are considered part of a metamorphic core complex in the Carpathian-Balkan Alps. A major detachment separates the massifs.

The Serbo-Macedonian massif is sub-divided into two litho-stratigraphic tectonic units, the upper Vertiskos formation to the south and west, with the Kerdilia formation to the north and east, which hosts Olympias itself. A faulted contact named the Stratoni separates the two formations.

The Vertiskos formation is composed mainly of “two mica” schist with intercalation of quartz lenses. It lacks the pegmatite that characterises the Kerdilia formation. A large less deformed meta-basic body termed amphibolite is located at the contact with the Kerdilia formation.

The Kerdilia formation is sub-divided into two units; the Upper and Lower. The Lower Unit mostly consisting of amphibolite gneiss, with lenses of foliated migmatitic rocks, named as Pegmatites (and

Aplite). The Upper unit consists mostly of biotite gneiss and schist interlayered with marble horizons, irregular pegmatite lenses and Aplite. The marble horizons of the Upper Kerdilia formation host the ore zones at Olympias. Both the Kerdilia and the Vertiskos rocks were affected by early ductile and later brittle deformation during the mid-Cretaceous to mid-Tertiary. This resulted from the metamorphic dome type uplift that occurred in the area, manifesting itself as a series of folds and faults bounding the metamorphic core. One such fault is the Stratoni fault, a major feature that dominates the area. During the early Oligocene the district was subjected to extensional tectonics allowing for the intrusion of a post tectonic/metamorphic suite of plugs and dikes. These intrude both the Vertiskos and the Kerdilia formations. Chemically, rocks are in the range of syenite/trachyte to dacite. Examples of these post tectonic intrusives include the Skouries and Fisoka deposits, both of which host gold-copper porphyry mineralisation.

7.2. LOCAL AND PROPERTY GEOLOGY

The Olympias polymetallic ore consists of stratabound replacement mineralisation hosted within the marble horizons of the Upper Kerdilia formation. The Kerdilia formation is separated from the Vertiskos formation by the Stratoni fault, an east-west to northwest southwest, southerly dipping structure which is still active (Figure 7-2) and which lies to the south of the Olympias deposit. Recent movement along the fault is normal though it is thought that this was originally a reverse movement fault that placed the Vertiskos on top of the Kerdilia. Recent zircon dating (Himmerkus et al. 2006 and 2003) has established that the Vertiskos Formation is Silurian in age and is thus older than the Upper Jurassic to Lower Cretaceous Kerdilia Formation, which is consistent with the Stratoni Fault originally being a major thrust fault bounding separate geologic terrains. This reverse movement is also supported by kinematic indicators in the rock (Cameron, unpublished company report 2007). The Kerdilia formation comprises a series of biotite, biotite hornblende and leucocratic gneisses, amphibolites and marbles. A greywacke parent is suggested for some of the biotite gneisses and an igneous origin for the remaining biotite, biotite hornblende and leucocratic gneisses and for the amphibolites. Retrograde mineral assemblages in these gneisses and schist indicate a post metamorphic thermal event.

The Olympias deposit consists of massive sulphide carbonate (marble) and aplite replacement lenses interlayed with biotite gneiss and schist. The rocks of the Upper Kerdilia formation have been folded and over thrust which has thickened and fractured the marble units. The whole of the formation was then subject to uplift with subsequent gravity collapse of the uplifted block along a series of north-northwest to north-south trending arcuate, listric faults dipping to the east. This has provided a series of fluid pathways which have allowed mineralising hydrothermal fluids to penetrate the structurally prepared marbles resulting in massive sulphide lenses. The majority of the orebody exhibits a north-south strike, with plunge to the south-east.

A common feature in the district is the presence of irregular lenses and vein type intrusions of aplite which post dates both the ore and host rocks. Figure 7-3 is a typical long section along the West Olympias orebody.

7.3. MINERALISATION

The Olympias mineralisation is a massive stratabound polymetallic replacement deposit hosted in the marble-gneiss contact of the Kerdilia Formation. The deposit comprises pyrite, arsenopyrite, sphalerite, galena, tetrahedrite-tenantite, boulangerite and chalcopyrite with secondary cerussite, chalcocite and covellite. Manganese oxides represent alteration of rhodochrosite. Gangue minerals include quartz, calcite, rhodochrosite, feldspar, kaolinite, chlorite, ankerite and graphite. The ore minerals are mainly massive in form. Kaolinisation is the main type of alteration associated with the deposit. Hydrothermal brecciation is common and chloritisation and silicification of host rocks immediately around the mineralised section is frequently observed.

The mineralisation occurs within two orebodies. The West orebody is approximately 250 m wide and plunges 1,500 m to the southwest. It has been intersected from surface to a depth of 500 m and is open down plunge. Its width varies between 5 m to 15 m, with dips averaging 30° to 35° east. The East orebody lies some 150 m east of the West orebody, has an anticlinal structure, exhibiting axial thickening, with steeper dips toward the peripheries. It dips an average 25° to 30° to the southeast. Its width averages 75 m and its average thickness is 7 m. The mineralisation has been traced for 600 m down plunge. Figure 7-3 is a cross section of the Olympias deposit.

Figure 7-1 **Schematic Structural Zones of Greece**

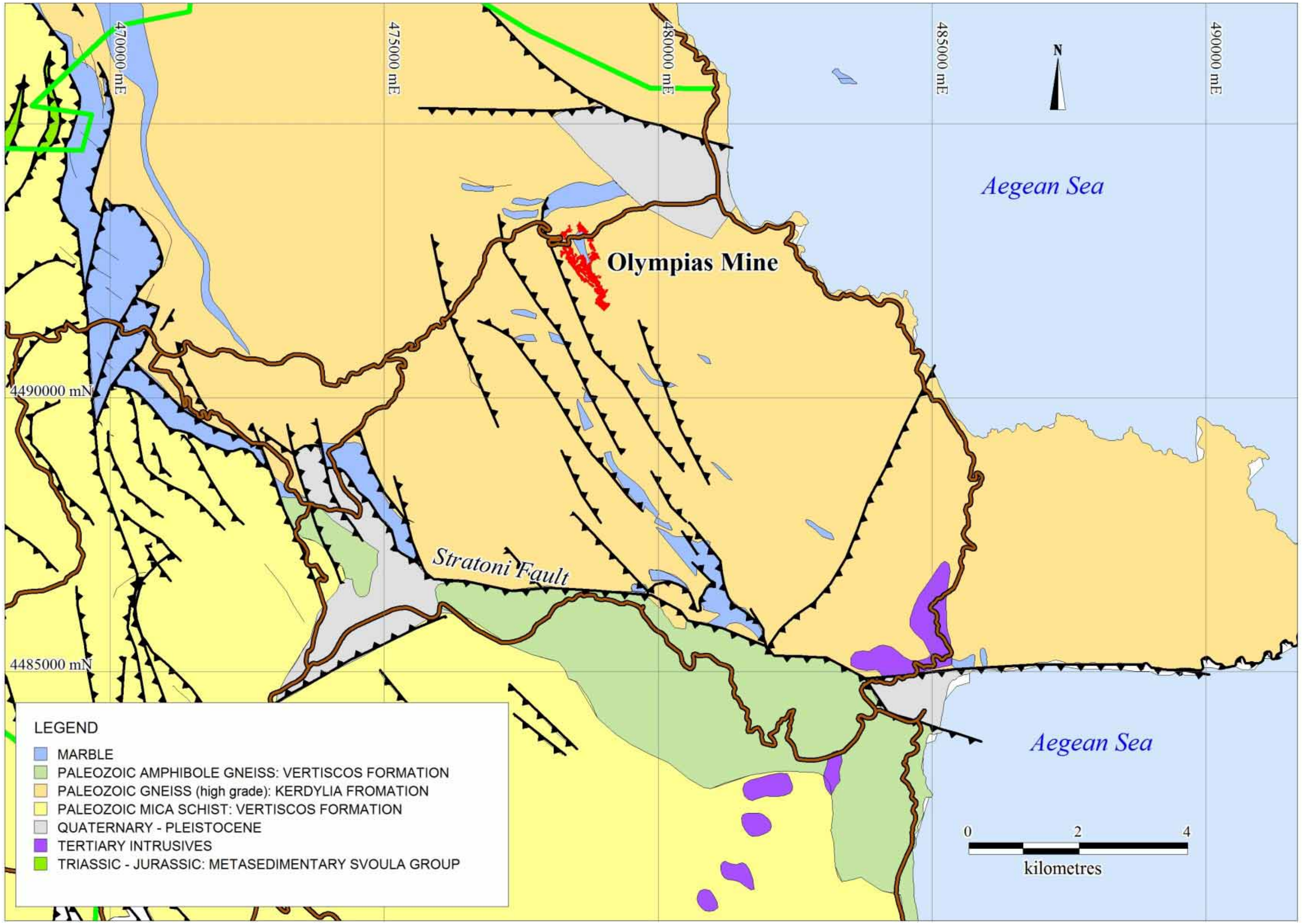


Figure 7-2 Local Geology

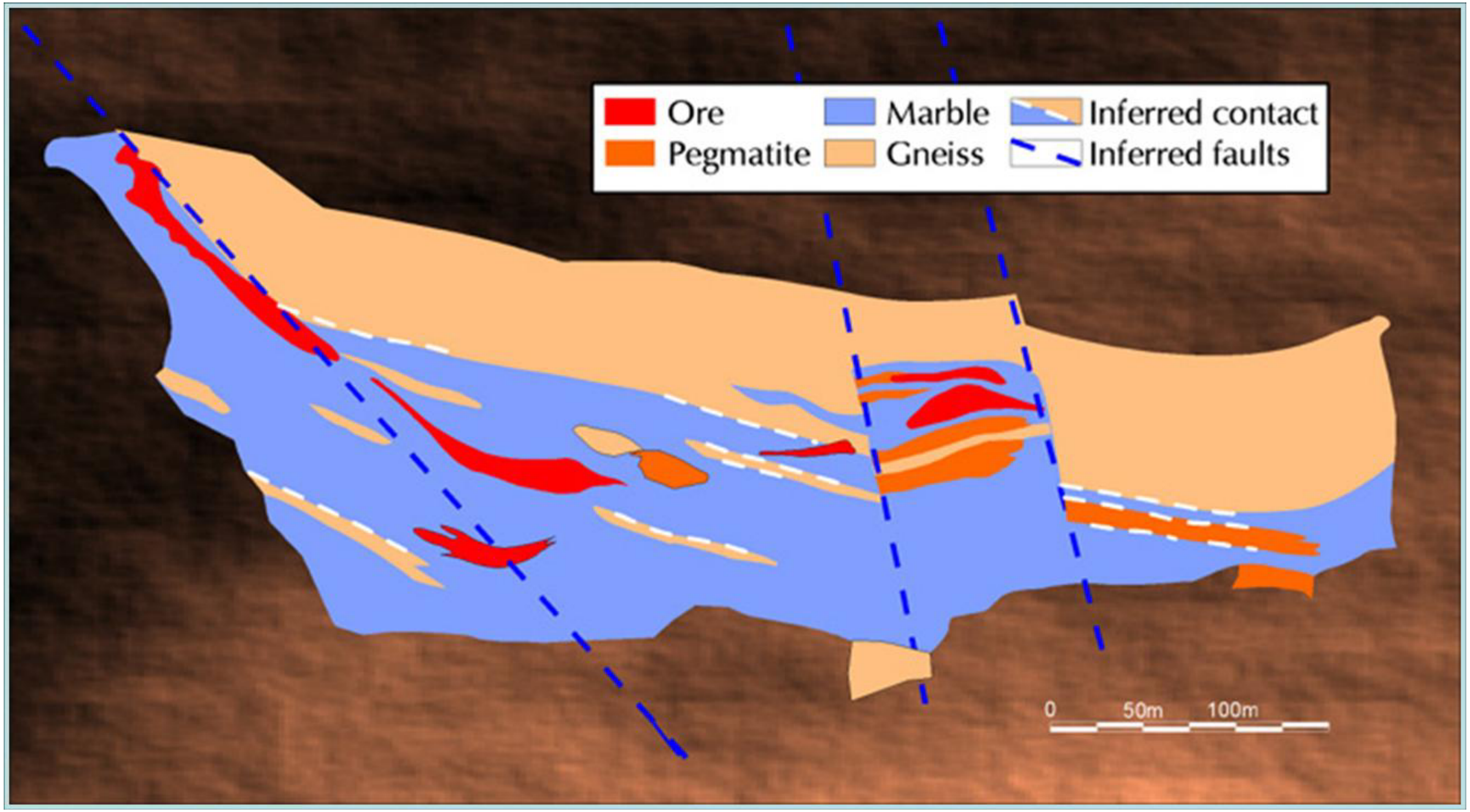


Figure 7-3 Long Section of the West Olympias Orebody

8. DEPOSIT TYPES

The sulphide ore comprises both undeformed massive sulphides and deformed sulphide ore with the latter characterised by brecciation, mylonitisation, folding and shearing. The most abundant ore minerals are pyrite, sphalerite, galena, arsenopyrite and chalcopyrite. Similar chemistry and fine zoning of sphalerite in both deformed and undeformed ore suggest that they come from the same system and were deposited after the onset of regional metamorphism. In addition copper-lead-zinc– silver bulk ore chemistry and together with lead silver relations, irrespective of deformation, indicate similarity to recognised skarn – replacement type deposits (Kalogeropoulos, Kilias and Bitzios, 1989).

Fluid inclusion work indicates that both deformed and undeformed sulphide ore were formed from H_2O rich CO_2 bearing fluids with medium to low salinities of 2.5 to 6.5 equivalent weight percent NaCl at fluctuating pressures of less than 500 bar and temperatures of 300°C to 400°C at Olympias (Kilias, Kalogeropoulos, and Konnerup Madsen 1996).

The narrow range of sulphur isotopes and the rare occurrence of sulphates at the more proximal of the deposits suggests high ratios of reduced oxidised/sulphur species ratios, high temperature whilst low $\delta^{34}S_{initial}$ to $\delta^{34}S$ values indicate an igneous origin for the sulphur. (Kalogeropoulos, Kilias and Bitzios, 1989). It is therefore interpreted that a primarily magmatic fluid source for both the deformed and undeformed sulphide ores at Olympias and the source of these fluids is thought to be a Tertiary sub-alkaline intrusive and is most likely a granodiorite, located some 8 km to the south-southeast. These fluids have migrated along the Stratoni fault and through axial planar axes relating to earlier deformation and then into the marble horizons at Mavres Petres and Madem Lakkos. The earlier deformation has also resulted in a structural thickening and preparation of the marble units. The Olympias deposit occurs within an uplifted block which has been subjected to footwall collapse with the bounding faults acting as conduits to the mineralising fluids.

9. EXPLORATION

The Hellenic Fertiliser Company carried out extensive programmes of surface and underground drilling in order to define orebody dimensions and to explore the area around them. Partial logs are available for this work but none of the original cores are available in labelled boxes, none of the holes were surveyed and no assays, certifiable or otherwise have been found. It is believed that ore was identified solely by visual assessment of the core. Where available the partial logs of this work have been entered in to the database but only in order to guide exploration work and for use in the modelling of major geological units. After 1996 TVX conducted an intense programme of drilling as detailed in the following paragraphs.

By February 1999 TVX had completed a drill programme comprising 760 holes totalling 91,319 m. A mineral resource estimation was completed in June 1998 and used in a feasibility study completed by Kvaerner Metals. The resource estimate was updated in May 1999 and an update of the feasibility was also done at this time. The TVX historic mineral resources and reserves were based on different processing routes for the gold concentrate and are therefore not seen as relevant to this report, which includes current estimates.

The Olympias Project was acquired by EGL (through its 95% owned subsidiary Hellas Gold) in 2004. No exploration has been carried out by EGL, however the author has viewed the cores and has checked original assay certificates against database entries for repeats and standards as well as original assays. The results from the TVX exploration were used in the current mineral estimates and are detailed in sections 11 to 15 and 17 of this report. A summary of the intercepts from this data is given in Appendix 1. Key areas of the orebody have had the interpolation checked and the overall geostatistical parameters have been checked. The mineral resource and reserve estimate was audited at that time by Behre Dolbear.

10. DRILLING

Only those holes drilled by TVX since 1996 were utilised for resource estimation purposes, as there is no means of validating those drilled by earlier operators. TVX drilled some 760 holes totalling 91,319 m. Excluding samples with less than 60% recovery, which were eliminated from the resource estimation, the overall recovery averaged 88.6%.

Drill core was logged lithologically, all sulphides were logged as blende (another name for sphalerite), pyrite, galena (BPG), mixed ore (pyrite > blende/galena) and pyritic/arsenopyrite ore. Lithologies logged were gneiss of various types, marble and aplite. Structural as well as minor geotechnical information was also logged. The orebody at Olympias was drilled on a nominal 25 m to 45 m spacing and the orebody is open down dip and along strike to the west. The drill orientation with respect to ore was variable since most of the holes were drilled in fans from mine infrastructure close to the orebody. Angles to the strike and dip of the orebody range from perpendicular, where drill widths represent true widths, to as low as 30° where drill widths can represent twice the true widths. For this reason particular attention was paid to compositing of the 1 m samples during the resource estimation process discussed in Section 19. All drilling in the current mineral resource was conducted by TVX but the logs to these drillholes and the sample QAQC (see Section 12) have been validated by the author.

11. SAMPLE PREPARATION, ANALYSES AND SECURITY

Only core drilled and sampled by TVX since 1996 has been used in the estimation of mineral resources. Intercepts on a one metre basis are given in Appendix 1 together with the location of each intercept as local mine coordinates.

After the core was brought from the underground or the surface drilling rig, geological and geotechnical logging was completed. During this stage, samples were defined by marking 'from' and 'to' points on the core. A detailed lithological and mineralogical description was given for each sample, which was then summarised in a two digit numeric code.

The sampling interval through the ore zone was 1 m, except when lithological changes occurred. The sampling interval was adjusted so that different rock types were sampled separately. In general, 5 m to 10 m of waste into the hanging wall and footwall was sampled using 2 m regular intervals and analysis of fully sampled cores has shown that this was sufficient to verify any low grade mineralisation in the country rocks around the main zones. This sampling policy led to some 13,500 samples being taken over the 1,500 m strike of the orebody. No factors were found to have affected the accuracy of the sampling and they have been found to be representative (see section 12).

After geological mapping and geotechnical logging, samples were defined as described above and the core was split longitudinally by diamond saw. Samples were then placed in labelled plastic bags and sent to the Stratoni laboratory for sample preparation. The remaining half core was stored in a core shed until 2002 and was then containerised and these containers are kept locked on site.

The sample preparation facility at the Stratoni laboratory was rebuilt in late 1996. The facility includes a drying oven, two jaw crushers, a roll crusher, a Jones riffle splitter, a 300 gramme (g) ring pulveriser and a 2,000 g ring pulveriser. The facility was used for all TVX Hellas samples which comprise the entire database used in this estimate.

The procedure followed by TVX Hellas was as follows:

Following sample drying at 85°C for 8 hours, the samples passed through an initial jaw crusher which reduced 95% of each sample to -2 centimetre (cm). A second jaw crusher further reduced this to –0.2 cm. The samples passed through the Jones splitter, which produced two samples. One sample weighed 400 g and was pulverised to –150 mesh and split into two. The second sample weighed 2 kilogramme (kg) to 5 kg and was placed in a coarse reject store.

All samples were routinely assayed for gold, silver, lead, zinc and arsenic. Initially SGS Laboratories (SGS) in Carcassonne, France were used for gold assays (certification ISO 9001), while the remaining elements were determined at the TVX-Stratoni laboratory in Greece. The Stratoni laboratory used for primary assays was certified according to the ISO 9002 standard under the scope "*Preparation and Chemical Analysis of Geological Mining, Metallurgical and Environmental Monitoring Samples, Certificate No 53987*" for data up to 2003, which includes all data relating to Olympias. This procedure was followed for the first 2000 in-fill samples. Approximately 12% of these were sent to the ALS Chemex Laboratories (Chemex) in Canada an ISO-9001 certified laboratory, to be assayed for all five elements as part of the quality control procedure. Both assay houses used fire assay with Atomic Absorption (AAS) finish on 50 g samples for gold determination. AAS was used for the base metals. Gold showed satisfactory results, but silver and lead determined at Stratoni showed high negative bias compared to Chemex, while zinc and arsenic results showed no bias. It was decided to keep the SGS laboratory gold assays for the first 2000 samples but to re-assay all ore samples for Ag, Pb, Zn and As at Chemex and use Chemex for the remainder of the Olympias Project.

Subsequently, 9% of pulps were submitted on a routine basis to ALS-Geolab in Chile (certification ISO 9001) for check assaying. Statistical analysis of check assays for zinc and arsenic were within acceptable standards. Gold assays varied by 2% with Chemex again the more conservative.

Some 4% of the coarse rejects were submitted under a different name to the Stratoni sample preparation facility and, following homogenisation, were split using the Jones splitter and a 400 g sample pulverised and split into two. The results from the coarse reject re-assays indicated that the Stratoni preparation facility was run to high procedural standards.

In the opinion of the authors the sampling and sample representativeness of the assays utilised in the Mineral Resource Estimate detailed in this report were carried out to industry standards and did not introduce any material bias to the assay database. The security of sampling was also sufficiently rigorous to ensure integrity of the data. Assay methodologies and lab accreditations also meet industry norms and the check assaying does not indicate any bias in the results contained in the database.

11.1. QUALITY ASSURANCE AND QUALITY CONTROL

The QAQC system applied at Olympias is schematically shown in Figure 11-1 Sample Preparation and Quality Control. It consisted of duplicate assays by a different laboratory, "blind" coarse reject checks, "blind" duplicate assays and standard samples. The QAQC system can be described as follows:

- Approximately 9% of left over pulps labelled 'A2' or second bottle were submitted to ALS-Geolab for the check assaying programme. The purpose of this analysis is to detect any biases between laboratories as well as to calculate if the assaying error is within industry standards.
- Approximately 4% of coarse rejects of samples labelled B were submitted, under a different number, to the routine sample preparation laboratory for splitting of a second sub-sample to be pulverised, labelled 'B1' and re-assayed by the main laboratory (Chemex). The aim of

this work is to validate the complete sample preparation and assaying procedure as well as to calculate the total error involved.
- Approximately 6% of left over pulps labelled 'A2' or second bottle were submitted, under a different number, to Chemex for blind duplicate assays.

A size analysis of coarse rejects labelled ‘B1’ was done periodically to ensure that the first sample split was done when samples are below 2 mm, which ensures that the total sample preparation error is maintained within acceptable industry standards.

As QC results consist of pairs of original and repeat values, the following notation was used: -

Original Assay = Variable A
Duplicate Assay = Variable B

The following calculations were performed for each pair of values:

Difference between original and duplicate value: -
Difference = A-B

Mean of original and duplicate values: -

Mean = (A + B) / 2

Relative error variance between original and duplicate values: -

Relative Error Variance = Variance / $(\text{mean})^2$
Relative Error Variance = 2 * $(A-B)^2 / (A+B)^2$

Relative Difference %: -

Relative Difference % = 200 * (A-B) / (A+B)

Absolute Relative Difference %: -

Absolute Relative Difference % = 200 * Absolute Value ((A-B) / (A+B))

The following statistical analyses were carried out: -

- Standard statistics for each variable, their differences and relative error variances.
- To obtain the global relative error variance, the relative error variances of the pairs were pooled and the global relative error variance is calculated as: -
- Global Relative Error (%) = √(Pooled Relative Error Variance) * 100
- Student's T test to assess any bias between the mean values of the original and duplicate results. The T test is calculated from the difference statistics as follows:
- T = mean difference * √(number of pairs / standard deviation of differences)

If the T statistic lies within the -1.96 to +1.96 interval, for more than 30 samples, it can be concluded that there is no significant bias.

- Regression analysis between the original and duplicate results.

Statistical comparisons between samples with grade values close to the detection limit can give misleading statistical results. For example, if the original assay is 0.01 g/t Au and its duplicate is 0.03 g/t Au, the percent relative difference amounts to 100%. This is meaningless since both samples are waste and close to the detection limit. To avoid the adverse effects of very low grade samples in the statistics, cut-off grades of 0.20 g/t for gold, 1.0 g/t for silver, and 0.10% for lead, zinc and arsenic were applied to the mean value of each pair.

In order to have a clear idea about the distribution of paired data results a scatter plot, a Q-Q plot, an absolute relative difference (%) vs. percent data plot and a relative difference (%) vs. mean grade plot were prepared for each data set. These figures are referred to in the corresponding tables.

The following results derived from the examination of the previously mentioned tables and figures are considered acceptable:

- The T Test result should lie within the range -1.96 to +1.96. This indicates that the means of duplicate values are similar. However, the T statistic must be analysed with caution since data very closely scattered about the first bisector can show high T values, since the standard deviation of the differences is in the denominator of the formula.
- The mean relative error should be below 20%.
- Correlation coefficients should be above 0.950.
- The intercept should be close to 0.000 and the slope close to 1.000.
- The scatter plot should be visually tightly distributed about the first bisector.
- The Q-Q plot should be close to the first bisector in all grade ranges.
- The percent of data with absolute relative differences below 20% should be above 90%.
- The relative difference vs. mean value plot should have a trumpet-like shape, since large relative differences occur for low grades, and should be symmetric about the abscise axis.
- In general, coarse reject results are expected to be slightly poorer than check assays since these include the sample preparation as well as the analytical error. On the other hand, blind duplicates should show the best results since the same pulp is analysed by the same laboratory.

11.2. ANALYSIS OF DUPLICATE RESULTS

This section deals with the analysis of: -

- Check assays between Chemex and ALS Geolab
- Blind duplicates within Chemex
- Coarse rejects assayed at Chemex

Results are presented in Table 11-1, Table 11-2 and Table 11-3 , for check assays, blind duplicates and coarse rejects respectively. Scatter plots and Q-Q plots for the Chemex vs. ALS Geolab results are shown in Figure 11-2, Figure 11-3, Figure 11-4 and Figure 11-5.

The following conclusions can be made:

- Gold results are overall acceptable. Outliers (above 40 g/t Au) did show a much worse correlation but this is likely due to the nugget effect.
- Silver results are acceptable, except for a few abnormal results in the very high grade range. This could be due to a nugget affect or the fact that Chemex analyses samples above 350 g/t by fire assay and ALS Geolab uses acid digestion and atomic absorption for all samples. Chemex fire assays should be considered the more reliable and these were used in the resource estimation.
- Of the revenue generating elements, lead shows a slight bias (3.4%) between Chemex and ALS Geolab, Chemex reporting higher values. This mainly occurs in samples containing lead greater than 25% and is not considered material to the Olympias Project. Otherwise, results are acceptable.
- Zinc results are acceptable. No overall bias was detected between laboratories.

Table 11-1 Check Assay Statistical Analysis - All Elements

ITEM	Au-Chx	Au-Geo	Ag-Chx	Ag-Geo	Pb-Chx	Pb-Geo	Zn-Chx	Zn-Geo	As-Chx	As-Geo	Fe-Chx	Fe-Geo	S-Chx	S-Geo
Number	903	903	914	914	835	835	820	820	884	884	343	343	98	98
Minimum	0.21	0.02	0.2	0.5	0.01	0.01	0.01	0.02	0.08	0.04	0.79	0.69	1.97	0.12
Maximum	121.24	151	2880	3970	56.4	56.6	37.6	37.57	33.6	31.61	37.1	39.6	46.1	45.9
Mean	13.77	13.78	152.1	156.4	5.2	5.03	6.29	6.33	6.47	6.08	16.67	17.23	26.65	23.79
Std Dev	14.03	14.38	227	250.3	6.58	6.35	6.12	6.36	6.81	6.47	8.22	9.05	8.92	9.12
Mean Diff (%)	99.93		97.23		103.38		99.37		106.41		96.75		112.02	
T Test	0.12		2.71		6.34		1.41		13.33		3.29		10.62	
Mean Rel. Err (%)	13.95		19.07		14.34		10.91		12.26		12.19		18.15	
Correlation (R)	0.979		0.984		0.994		0.992		0.993		0.939		0.956	
Intercept	0.609		12.44		0.007		0.246		0.124		1.987		4.399	
Slope	0.955		0.893		1.031		0.955		1.044		0.852		0.935	
%Data <20% Abs	90		91		95		95		97		88		62	
Relative Diff Figures	4.1 to 4.4		4.5 to 4.8		4.9 to 4.12		4.13 to 4.16		4.17 to 4.20		4.21 to 4.24		4.25 to 4.28	

Table 11-2 **Chemex Blind Duplicate Statistical Analysis -All Elements**

ITEM	Au-Chx1	Au-Chx2	Ag-Chx1	Ag-Chx2	Pb-Chx1	Pb-Chx2	Zn-Chx1	Zn-Chx2	As-Chx1	As-Chx2	Fe-Chx1	Fe-Chx2	S-Chx1	S-Chx2
Number	628	628	635	635	609	609	619	619	624	624	364	364	13	13
Minimum	0.04	0.21	0.2	1.3	0.01	0.12	0.02	0.02	0.01	0.09	0.11	0.11	17.1	17.2
Maximum	111.7	112.95	1475	1040	40.1	38.7	39.8	40	28.4	28	36.1	36.8	32.7	33.3
Mean	13.29	13.34	195.9	192.5	7.06	7.12	8.25	8.18	6.35	6.36	18.46	18.43	26.78	26.63
Std Dev	13.33	13.27	199.9	191.4	6.81	6.85	6.74	6.76	6.78	6.76	7.7	7.52	5.23	5.14
Mean Diff (%)	99.63		101.8		99.16		100.86		99.84		100.16		100.56	
T Test	0.55		1.5		3.42		1.1		0.24		0.2		0.93	
Mean Rel. Err (%)	17.48		19.9		16.4		22.71		15.86		14.15		1.66	
Correlation (R)	0.985		0.957		0.998		0.977		0.977		0.941		0.993	
Intercept	0.312		12.98		0.034		0.092		0.182		1.48		0.477	
% Data <20% Abs	91		92		95		91		96		94		100	
Slope	0.98		0.916		1.004		0.981		0.973		0.918		0.976	
Relative Diff Figures	4.29 to 4.32		4.33 to 4.36		4.37 to 4.40		4.41 to 4.44		4.45 to 4.48		4.49 to 4.52		4.53 to 4.56	

Table 11-3 **Coarse Reject Statistical Analysis - All Elements**

ITEM	Au-Chx1	Au-Chx2	Ag-Chx1	Ag-Chx2	Pb-Chx1	Pb-Chx2	Zn-Chx1	Zn-Chx2	As-Chx1	As-Chx2	Fe-Chx1	Fe-Chx2	S-Chx1	S-Chx2
Number	506	506	518	518	466	466	481	481	503	503	155	155	98	98
Minimum	0.04	0.04	0.5	0.2	0.04	0.01	0.02	0.08	0.01	0.03	1.1	1.08	1.97	0.12
Maximum	120	121.7	1190	1145	43.6	41.7	25.7	26.5	33.5	35.1	33.6	35.5	46.1	45.9
Mean	11.89	12.02	106.8	108	3.75	3.76	5.36	5.43	5.5	5.67	16.02	16.71	26.65	23.79
Std Dev	11.6	11.81	150.5	148.7	4.89	4.86	5.67	5.78	6.36	6.62	8.01	7.87	8.92	9.12
Mean Diff (%)	98.92		98.92		99.73		98.71		97		95.87		112.02	
TTest	1		1.8		0.9		1.52		2.67		4.83		10.62	
Mean Rel. Err (%)	14.45		17.35		15.67		13.37		17.65		9.12		18.15	
Correlation (R)	0.971		0.995		0.996		0.993		0.974		0.975		0.956	
Intercept	0.258		2.958		0.055		-0.01		0.105		1.375		4.399	
Slope	0.989		0.983		0.99		1.012		1.013		0.957		0.935	
% Data <20% Abs	94		86		93		80		95		96		5	
Relative Diff Figures	4.57 to 4.60		4.61 to 4.64		4.65 to 4.68		4.69 to 4.72		4.73 to 4.76		4.77 to 4.80		4.81 to 4.84	

11.3. GOLD CHECK ASSAYS BETWEEN CHEMEX AND SGS

As mentioned above, the first 2,000 samples were assayed for gold at the SGS-Carcassonne laboratory in Southern France using a 30 g sample. As part of the quality control program, 245 of these were sent to Chemex for re-assaying using 50 g samples with an atomic absorption finish. Statistical comparisons are presented in Table 11-4, which includes analyses with and without cut-off grade.

Figure 11-6 shows a scatter plot of the SGS gold data versus the Chemex data. A few erratic samples, especially above 40 g/t can be seen which are interpreted as being due to the nugget effect.

The quantile-quantile (QQ) plot is presented in Figure 11-6 and the mean values show that there is a slight bias of approximately 2%, SGS being the higher of the two laboratories. This bias is likely to be due to the differences observed in the high-grade samples.

The absolute relative difference (%) vs. percent data shows that 86% of the data have absolute relative differences lower than approximately 20 %. The mean relative error is 19.24% which is slightly higher than the acceptance limit.

The relative difference vs. mean value plot shows normal behaviour, except for the few erratic samples mentioned earlier.

Table 11-4 Chemex vs. SGS Check Assay Statistical Analysis - Au

Item	Au-Chemex	Au-SGS	Au-Chemex	Au-SGS
Cut-Off Grade	None		0.2	
Number	245	245	228	228
Minimum	0.02	0.03	0.11	0.36
Maximum	105.3	98.1	105.3	98.1
Mean	10.89	11.12	11.7	11.95
Std Dev	11.61	11.9	11.64	11.93
Mean Diff (%)	97.93		97.91	
T Test	-1.97		-1.98	
Mean Rel. Err (%)	19.24		15.83	
Correlation (R)	0.988		0.987	
Intercept	0.098		0.115	
Slope	1.012		1.012	
Relative Diff Figures	4.81 to 4.84		4.85 to 4.88	

11.4. QUARTER CORE CHECK ASSAYS BY KVAERNER METALS

During the 1999 feasibility study Kvaerner Metals appointed SRK Cardiff Office as auditor of the mineral resource estimation study.

As part of the audit, 35 core samples were selected and one quarter of the core was split with a diamond saw and sent to OMAC Laboratories in the UK for sample preparation and assaying. The aim of this work was to ensure that there was no tampering with samples. Comparative results between the original TVX half core samples and Kvaerner Metals quarter core samples are shown in

Table 11-5. Comparative statistical analysis for each element is shown in Table 11-6. Statistical analysis was done in a similar manner as was done for check assays and coarse rejects in the previous sections. Scatter plots of the data are shown in Figure 11-7, Figure 11-8, Figure 11-9 and Figure 11-10.

The following general comments stem from the above analysis:

- All elements, except zinc, are distributed about the first bisector and therefore there is no bias.
- Zinc results are as expected; the distributions are similar for all grade ranges.
- The absolute relative difference plots show that the percentage of data with less than 20% absolute relative difference is between 35% and 66% for the different elements. This scatter is considered fairly large. However the large scatter and deviation from the first bisector are due mainly to a few erratic values. These, in turn, are due to the large difference in support size of the samples considered.

The general conclusion of the quarter core assay comparisons is that the distribution of half core and quarter core values are similar enough to ensure that tampering did not occur.

Table 11-5 Quarter Core Checks by Kvaerner Metals

DDH Properties			TVX Original Half Core Sample						Kvaerner Metals Quarter Core Sample					
Hole	From-To	Sample	Au g/t	Ag g/t	Cu %	Pb %	Zn %	As %	Au g/t	Ag g/t	Cu %	Pb %	Zn %	As %
01-531	51-52	22452	3.57	312	0.14	12.3	20.4	0.46	3.15	348	0.08	14.4	22.71	0.21
01-531	48-49	21949	1.47	180	0.08	6.98	22.5	0.4	1.5	219	0.07	8.48	22.71	0.28
01-532	50.45-51.2	22415	32.34	30.4	0.01	1.06	1.36	14.7	34.88	45.6	0.01	1.66	2.03	13
01-532	47.4-48.4	22413	18.03	113	0.04	3.72	3.46	6.4	19.92	91.7	0.03	3.32	4.54	8.7
01-550	74.5-75.5	25884	10.17	172	0.05	4.38	2.12	15.7	12.44	159	0.06	4.72	1.86	15.8
01-550	75.5-76.5	25885	7.68	71.1	0.05	2.18	1.05	7.1	7.8	53.6	0.01	1.89	1.04	8.4
01-550	76.5-77.5	25886	9.15	2.9	0.01	0.06	0.04	16.2	9.6	7.6	0	0.21	0.09	13.8
01-568	113.1-114.0	26204	20.91	381	0.06	9.96	11.8	1.76	8.8	306	0.37	8.28	11.36	0.83
01-568	114-115	26205	15.57	107	0.02	2.73	3.24	6.47	14.32	141	0.02	4.16	5.03	5.5
01-568	115-116	26206	16.53	23.1	0.01	1.73	5.31	4.65	16	21.8	0.02	1.42	7.5	3.5
01-568	116-117	26207	29.55	19.7	0.05	1.02	19.9	6.22	33.76	19.7	0.04	1.69	19.31	5
01-568	117-118	26208	6.55	65.7	0.03	1.96	10.9	2.05	6.2	197.8	0.04	5.56	14.2	1.56
01-568	118-119	26209	16.87	164	0.02	4.47	3.87	5.91	19.92	95.3	0.05	3.4	2.23	5.7
01-568	119-120	26210	6.65	23.7	0.02	0.57	2.86	2.75	7.76	49.3	0.02	1.51	3.81	2.74
01-568	120-121	26211	15.09	319	0.05	8.63	9.69	1.27	14.52	219	0.03	6.28	7.18	1.19
01-568	121-122	26112	15.05	871	0.06	24.2	6.68	1.86	15.04	427	0.06	13.6	8.52	1.25
01-617	49.3-50.3	26868	44.16	60.3	0.01	1.87	0.71	28.1	36	68.5	0.01	2.85	1.67	16
01-617	50.3-51.3	26869	46.05	346	0.01	9.94	0.1	29.1	52.96	298	0	8.76	0.06	20.1
01-617	51.3-52.3	26870	75.77	97.5	0.01	3.07	0.72	29.8	74.4	111	0.01	3.28	0.81	21.8
0-617	52.3-53.3	26871	68.23	127.5	0.06	4.11	4.65	18.8	56.32	78.2	0.03	2.78	4.22	14.5
01-582	222.0-222.7	25821	8.57	30.1	0.02	0.75	1.96	2.55	4.94	36.9	0.02	0.41	1.4	2.31
01-582	226.6-227.5	25825	27.94	140	0.15	5.32	5.39	10.6	30.72	271	0.27	7.92	6.04	9.2
01-550	86.2-87.2	25895	120	176	0.03	4.55	0.99	0.88	22.56	121	0.02	3.64	0.71	1.26
01-648	20.85-22.85	28149	10.08	983	0.25	2.6	3.24	2.03	6.56	508	0.11	1.46	2.23	1.06
01-648	22.85-24.5	28150	4.73	272	0.06	1.8	0.19	3.38	8.12	177	0.04	1.94	0.44	4.7
01-676	257-258	28186	12.65	66.9	0.01	2.46	0.54	22.7	13.92	54.5	0.01	2.16	0.41	21.5
01-676	258-259	28187	12.14	209	0.03	8.17	5.89	6.7	10.96	218	0.03	7.68	7.46	4.9
01-676	253.9-254.3	28182	11.18	514	0.05	20.4	7.36	15	8.16	88.8	0.04	3.32	5.27	11.3
01-676	198-199	28159	7.13	185	0.04	6.7	5.26	2.3	5.64	209	0.03	6.88	5.44	1.9
01-676	199-200	28160	10.35	66.3	0.03	2.37	4.65	4.48	8.36	65.6	0.02	2.56	5.56	4.3
01-676	200-201	28161	7.95	16.2	0.03	0.46	4.47	6.05	8.6	12.8	0.02	0.4	3.37	6.6
01-676	201-202	28162	5.31	107.5	0.24	3.94	3.41	3.02	7.44	57.3	0.12	1.82	5.15	2.34
01-676	202-203	28163	5.21	18.6	0.04	0.63	10.3	2.27	7.44	55.3	0.14	1.74	4.95	2.53
01-676	203-204	28164	4.87	197.5	0.09	7.31	17.4	0.81	4.37	250	0.1	7.92	16.22	0.56
01-676	204-205	28165	1.92	265	0.44	9.17	6.85	0.44	9.28	317	0.31	8.56	11.36	0.94

Table 11-6 Comparative Statistical Analysis for each Element - TVX vs. KM

Item	TVX-Au	KM-Au	TVX-Ag	KM Ag	TVX-Pb	KM-Pb	TVX-Zn	KM-Zn	TVX-As	KM-As
Number	35	35	35	35	35	35	35	35	35	35
Minimum	1.47	1.5	2.9	7.6	0.06	0.21	0.04	0.06	0.4	0.21
Maximum	120	74.4	983	508	24.2	14.4	22.5	22.71	29.8	21.8
Mean	20.27	17.21	192.4	154.3	5.19	4.48	5.98	6.2	8.08	6.72
Std Dev	24.55	16.58	219.99	125.65	5.35	3.57	6.03	6.21	8.68	6.51
Mean Diff %	15.1		19.8		13.7		-3.7		16.8	
T Test	1.07		1.64		1.17		-0.74		2.76	
Mean Rel. Error	28.64		35.16		35.86		26.52		23.78	
Correlation (R)	0.73		0.82		0.74		0.96		0.97	
Intercept	7.28		64.14		1.9		0.3		0.87	
Slope	0.49		0.47		0.5		0.99		0.72	
Relative Diff Figures	4.89 to 4.92		4.93 to 4.96		4.97 to 4.10		4.101 to 4.104		4.105 to 4.108	

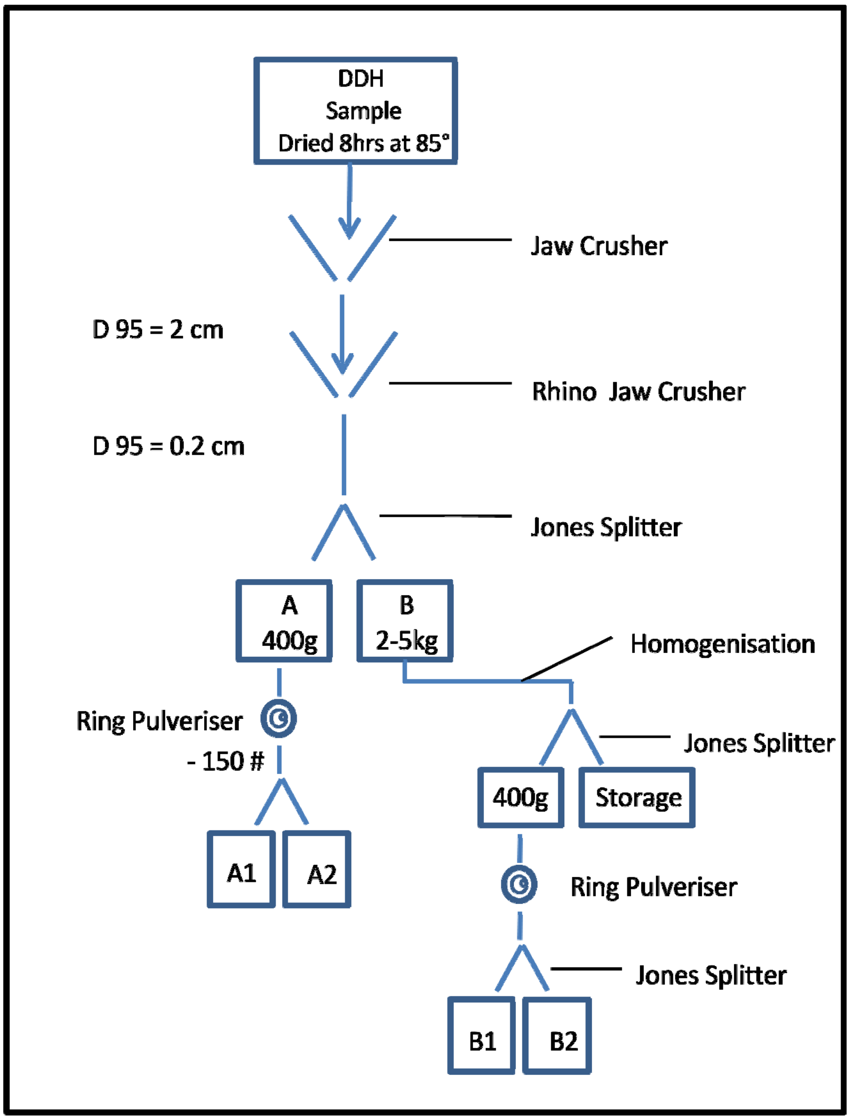


Figure 11-1 Sample Preparation and Quality Control

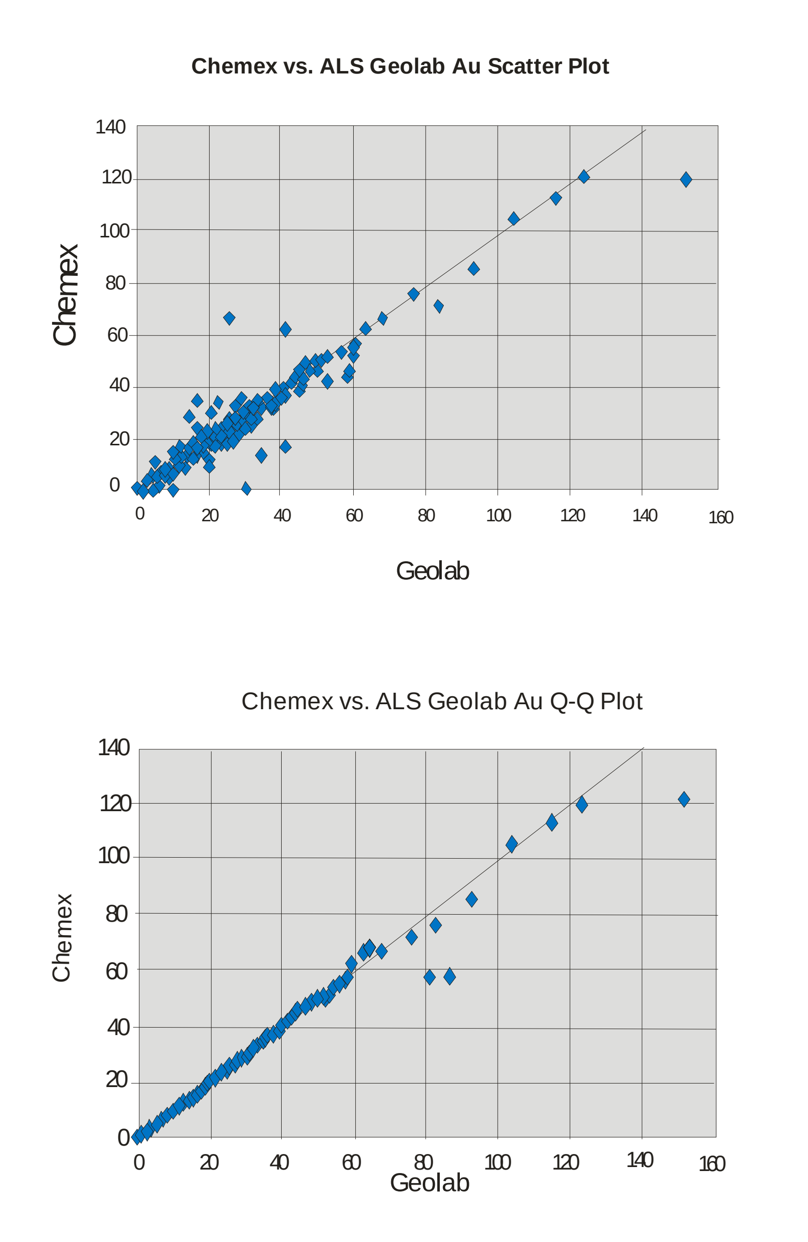
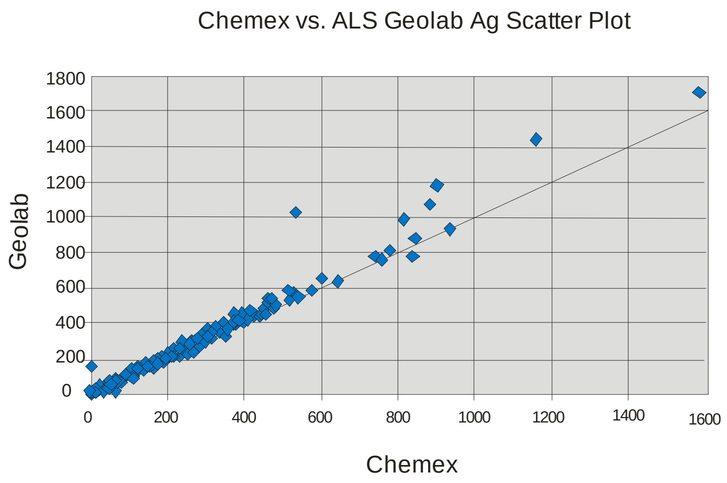


Figure 11-2 Chemex vs. ALS Geolab Au Scatter and Q-Q Plots.



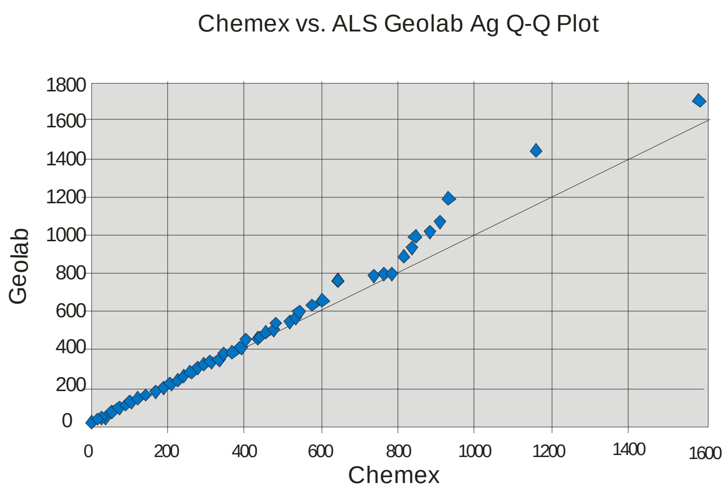


Figure 11-3 Chemex vs. ALS Geolab Ag Scatter and Q-Q Plots.

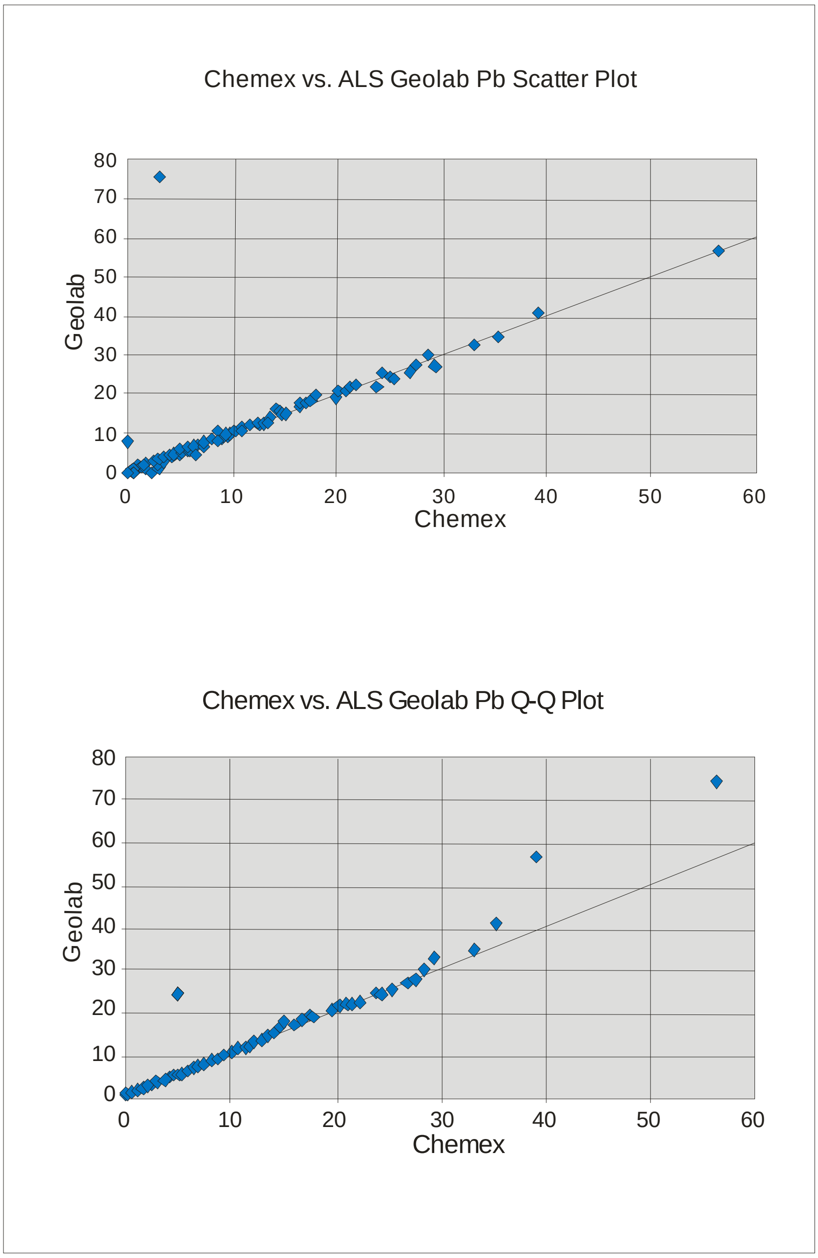


Figure 11-4 Chemex vs. ALS Geolab Pb Scatter and Q-Q Plots.

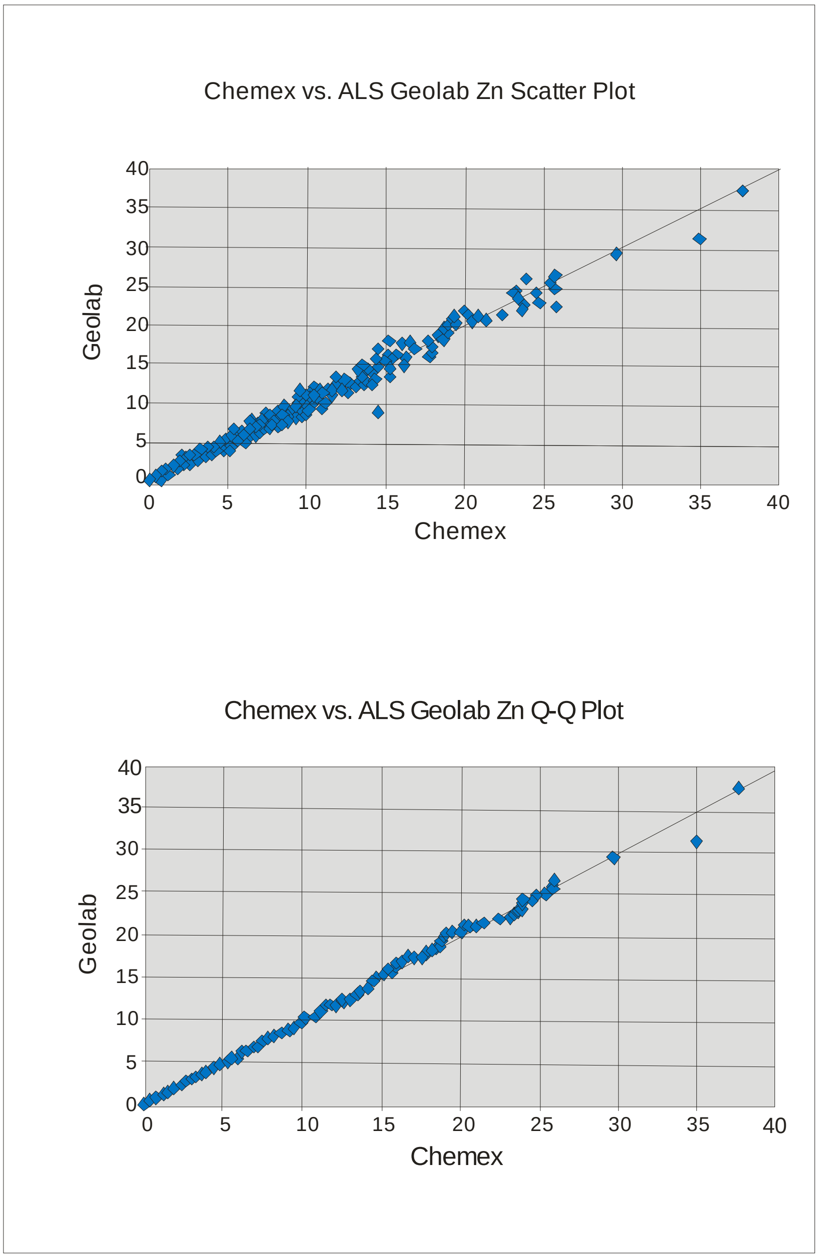


Figure 11-5 Chemex vs. ALS Geolab Zn Scatter and Q-Q Plots.

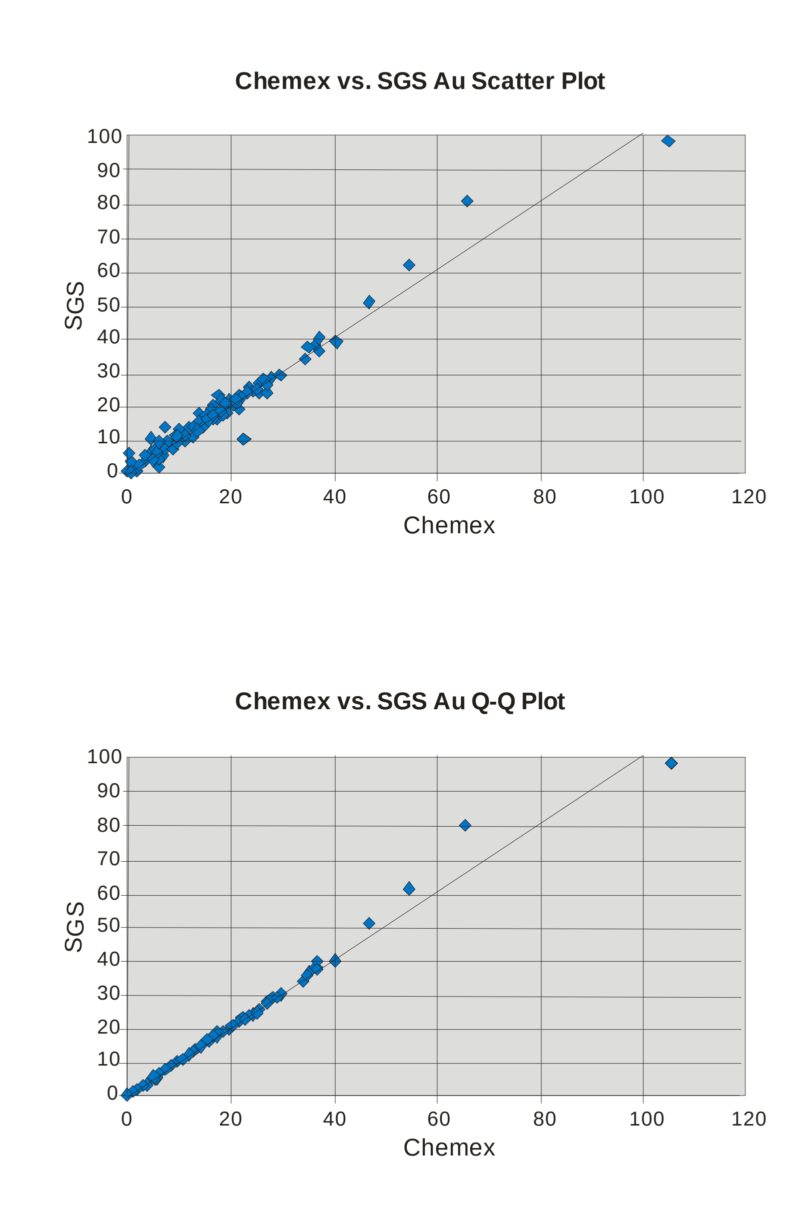


Figure 11-6 Chemex vs. SGS Carcassonne Au Scatter and Q-Q Plots

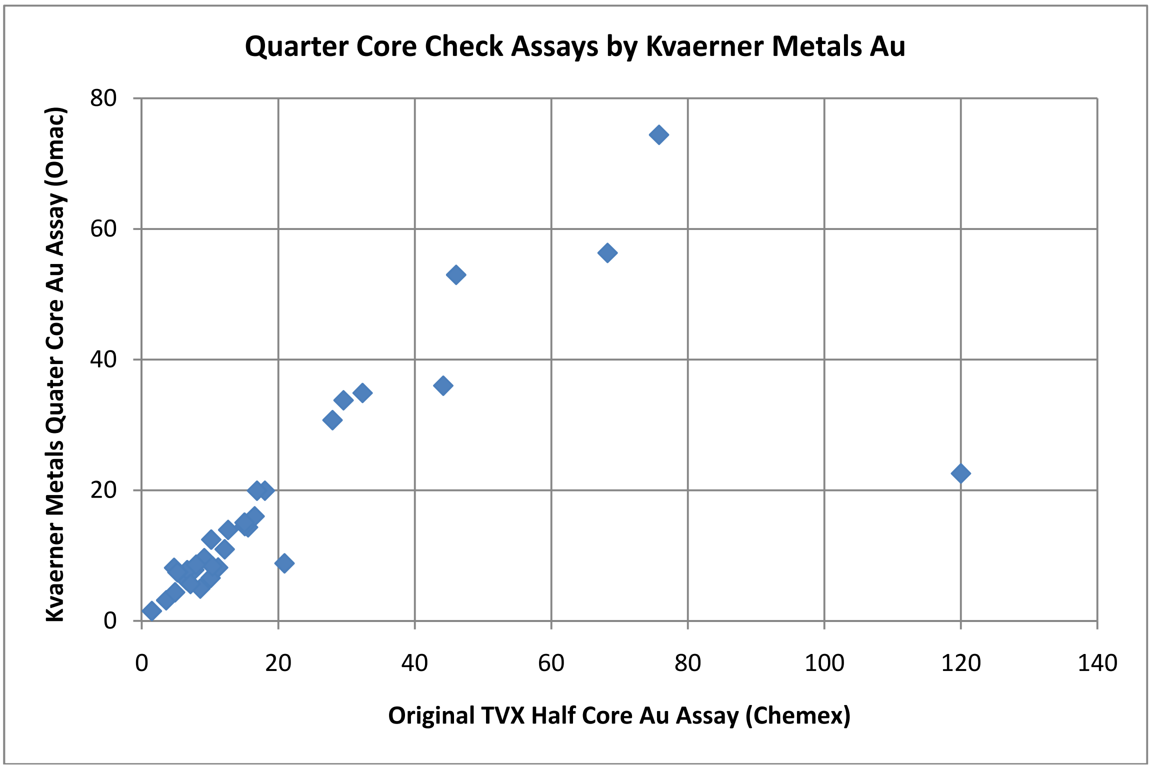


Figure 11-7 Quarter Core Check Assays by Kvaerner Metals Au

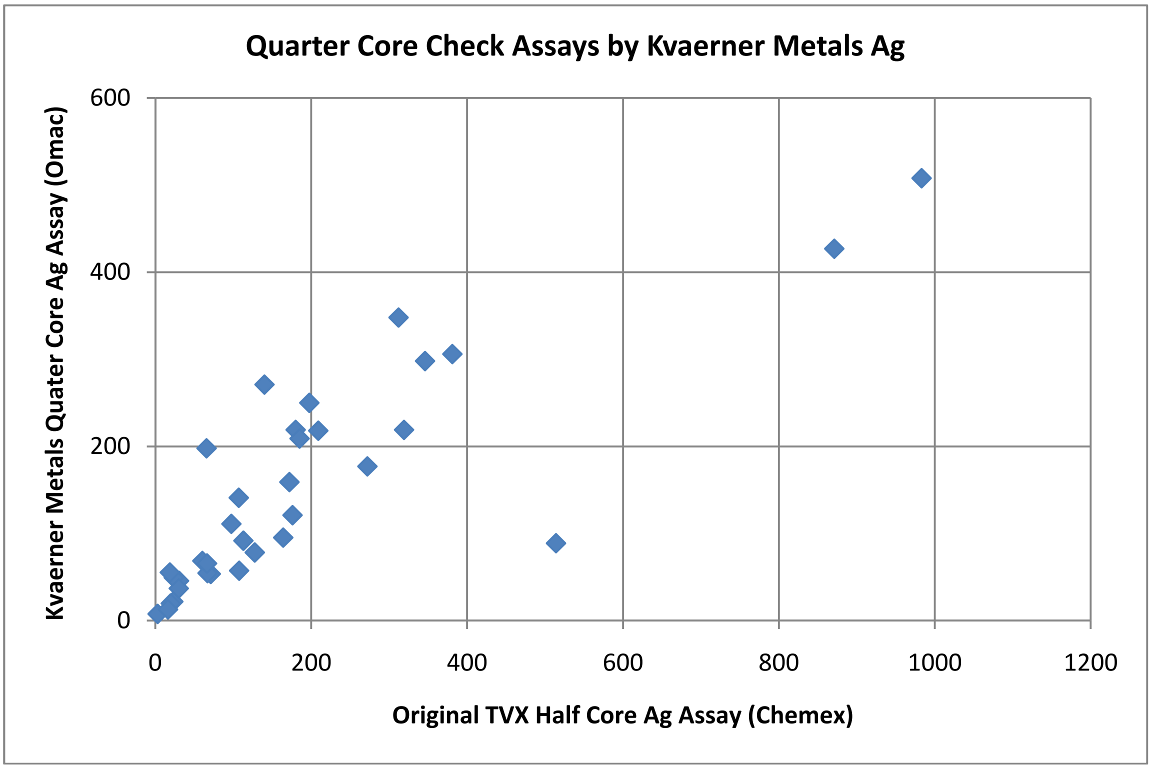


Figure 11-8 Quarter Core Check Assays by Kvaerner Metals Ag

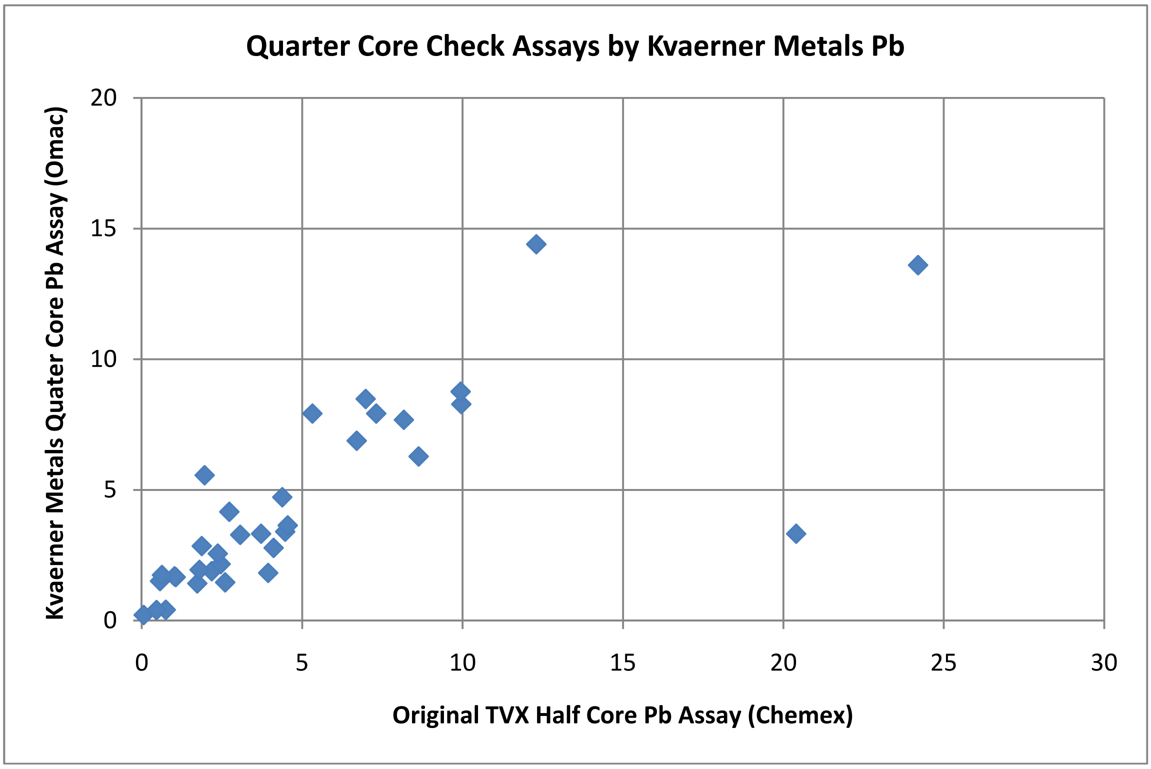


Figure 11-9 Quarter Core Check Assays by Kvaerner Metals Pb

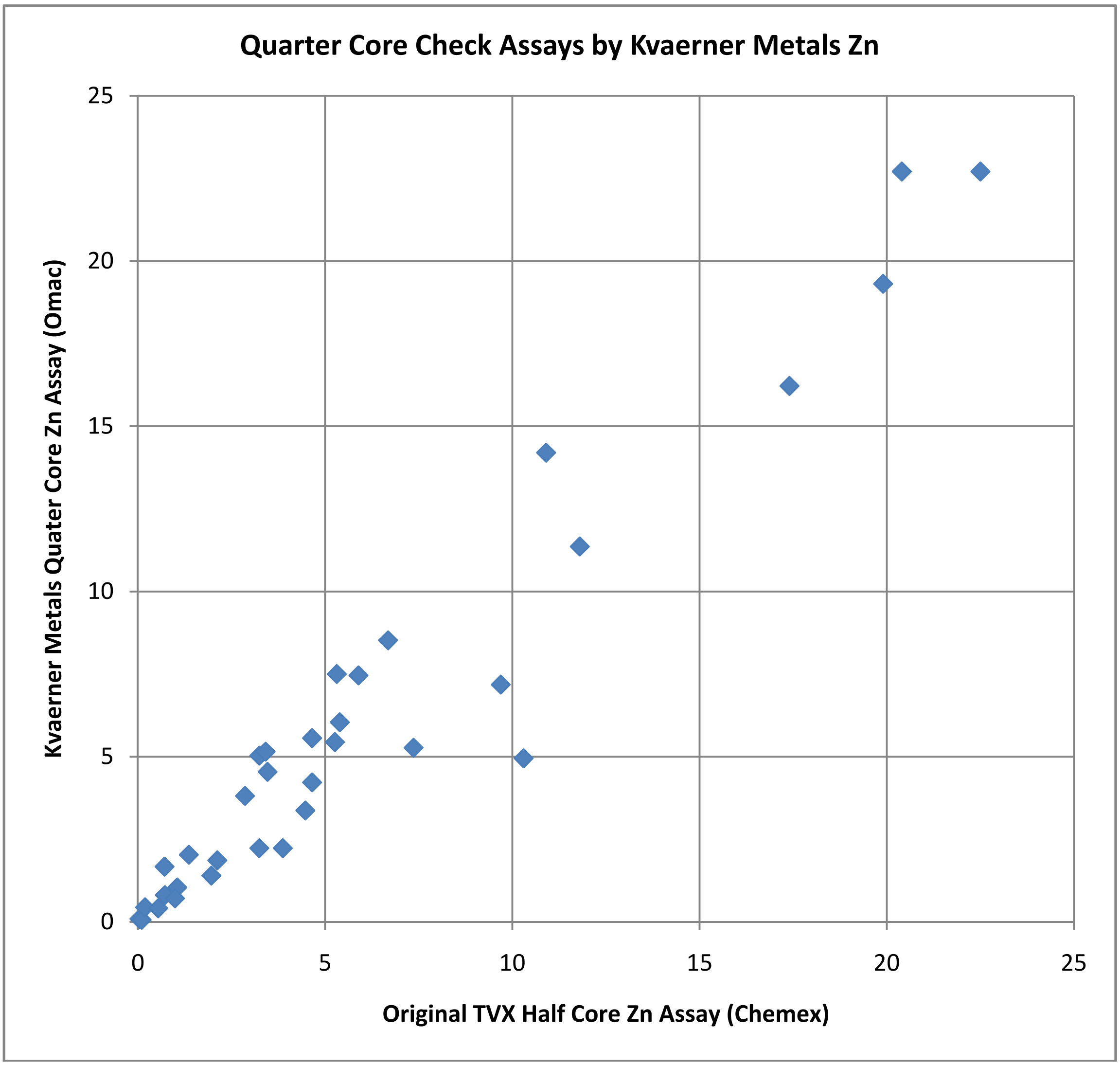


Figure 11-10 Quarter Core Check Assays by Kvaerner Metals Zn

12. DATA VERIFICATION

No exploration has been carried out by EGL however the authors have viewed the cores and have checked original assay certificates against database entries for repeats and standards as well as original assays. In the authors' opinion the sample database is representative with no significant bias.

The assay facilities at Chemex, SGS and ALS-Geolab of Chile were internationally accredited at the time of the sampling and original assay certificates have been inspected by the author.

12.1. CONCLUSIONS ON QUALITY ASSURANCE AND QUALITY CONTROL

The analysis of quality control data lead to the following conclusions:

- There is a 3.4% bias for lead between Chemex and ALS-Geolab with Chemex being the higher one.
- Analytical errors deduced from check assays were within acceptable standards.

- Sample preparation and analytical errors deduced from coarse reject analyses gave good results, reflecting that the sample preparation protocol and workmanship were of high standard.
- A slight bias of approximately 2% was observed between Chemex and SGS for gold assays, Chemex being the more conservative of the two laboratories. This bias is considered to be within acceptable limits.

Following a detailed review of the documentation including a review of the QAQC data the authors of this report are satisfied that the sampling work was conducted to a high professional standard and that there is no significant bias in the sample database. The authors of this report are satisfied that the procedure in place at the time of drilling and the subsequent high standard to which material is preserved are indicative of a high level of sample security.

In 1999, Behre Dolbear completed an audit of the mineral resources at Olympias on behalf of TVX which has been reviewed by the authors. This included:

- Review of drill hole locations and surveys;
- Review of drilling, logging, sampling, and splitting procedures;
- Review of assay procedures, the qualifications of laboratories utilised, and the frequency of submission of check samples;
- Review of drill hole logs for accuracy related to plotting of geologic units, plotting of assayed intervals and grades, and incorporation of relevant features related to mineralisation and structures;
- Review of procedures for cutting and capping grades;
- Review of whether any bulk samples had been taken and results;
- Review of geostatistical procedures;
- Review of the adequacy of drill hole spacing
- Review of all geologic cross sections; and
- Review of reserve calculation parameters:
- Justification of the density factor used;
- Inclusion of dilution;
- Criteria used in categorising mineral reserves.

A report entitled 'A Review of the Data and Methodology Used in a Resource Estimate, Olympias Project, Stavros, Chalkidiki, Greece.' By Behre Dolbear in 1999 concluded:

"That the assays in the TVX database are reliable."

The work carried out for this report indicates that there is no bias relating to the sampling, sample preparation, sample analysis and assay reporting, therefore the author corroborates the view that assays are reliable. The author of this report Section concurs with this conclusion.

13. MINERAL PROCESSING AND METALLURGICAL TESTING

EGL have not carried out any flotation processing testwork but a number of extensive independent reports were commissioned by TVX Hellas SA, as listed in Section 27, References. On review of the reports it is the authors' opinion that the testwork was carried out in an unbiased manner on representative samples from the Olympias deposit. In general the testwork confirmed the anecdotal evidence form historic operations that the ore responds well to flotation with high recoveries, as stated on Section 17, Recovery Methods, of this report. In the opinion of the authors the testwork demonstrates that the ore responses to flotation are well understood and the proposed processing route is appropriate.

14. MINERAL RESOURCE ESTIMATES

The Olympias mineral resources were previously estimated in 1999 as part of the feasibility study conducted by Kvaerner Metals for TVX. This estimate was also reviewed by Behre Dolbear and SRK Consulting, both of whom concluded that the estimate was to industry standards.

EGL has recalculated the geological mineral resource tonnage and grade using geostatistical methods within Gemcom mining software for this report. The estimates were not affected by environmental, permitting, legal, title, taxation, socio-economic, marketing, political, mining, metallurgical infrastructure or other relevant factors other than those disclosed herein. The main steps of the geological estimation process were as follows:

14.1. AVAILABLE DATA

Only drilling conducted by TVX since 1996 was included in the estimation of mineral resources since earlier data was not subjected to the QAQC described earlier in this report and could therefore not be validated.

14.2. LITHOLOGICAL CODES

Lithology and mineralisation descriptions were simplified for all rock types.

Two digit numerical codes are assigned to each sample in order to describe the main characteristics.

Lithology Codes for the Olympias Deposit

First Digit

1 Massive sulphide or arsenopyrite mineralisation
2 Aplite or pegmatite
3 Marble
4 Breccia
5 Rhodochrosite
6 Gneiss
7 Schist
8 Lamprophyre
9 Unknown

Second Digit

0 None (no important secondary characteristic)
1 Disseminated or mainly arsenopyrirte mineralisation if following a 1 as first digit
2 Pervasive argillic alteration (mainly kaolinite)
8 Not sampled
9 Very low recovery

14.3. CORE RECOVERY

Core recoveries were recorded in the geotechnical logs for all definition and infill drillholes. Recovery data were recorded as metres recovered in each core barrel. The average recovery of each barrel was assigned to all the samples contained within it. In those cases where samples were contained partly in one barrel and partly in the following one, a weighted recovery was calculated. The overall average recovery was 88.6% which is considered to be within industry standards.

14.4. SPECIFIC GRAVITY DETERMINATIONS

Specific gravity determinations were obtained by both volumetric and geometric methods. During the first phase of the project, volumetric measurements were done over split core specimens. The method involved drying the sample, weighing the sample in air and weighing the sample submerged in water. Therefore, this method did not take into account the rock porosity and voids. This was subsequently replaced by geometric method. The method consists of drying the sample, weighing the sample accurately in air and measuring the volume of the core probes directly. Generally, this was done on whole core probes and occasionally on half core probes. This method is preferred since it reflects the true in-situ specific gravity.

In order to assess both methods a comparison between volumetric and geometric determinations was carried out.

To validate the measurement methodology used by TVX on-site, 82 whole core specimens were sent to Robertson Research Laboratories in the UK in 1998, where a wax-coated volumetric-type method was used. A comparison of results obtained by TVX-volumetric, TVX-geometric and Robertson Research is shown in Table 14-1.

Table 14-1 Statistics of Specific Gravity (SG) Comparisons: TVX Hellas and Robertson Research

SG From	SG To	Number of Samples	SG (Geometric)	SG (Volumetric)	% Difference geometric to volumetric	SG (Wax-Coated)	% Difference geometric to wax coated
2.00	2.50	3	2.40	2.68	11.68	2.63	9.60
2.50	3.00	16	2.72	2.85	4.75	2.81	3.16
3.00	3.50	19	3.24	3.42	5.41	3.33	2.61
3.50	4.00	14	3.80	4.07	7.23	3.89	2.57
4.00	4.50	20	4.24	4.37	3.18	4.29	1.16
4.50	6.00	10	4.75	4.69	-1.23	4.59	-3.22
All Data		82	3.63	3.78	4.10	3.69	1.51

- TVX-volumetric method shows the highest specific gravity values and TVX-geometric the lowest. Robertson Research values lie in between. This trend is consistent throughout all ranges except the highest (4.50 to 6.00 g/cc), due to the presence of one erratic result.
- The overall trend shown above was as expected since the volumetric method (non-waxed) failed to take into account porosity and voids, the wax-coated method eliminated the effect of porosity but not of voids, and the geometric method took both phenomena into account.

From this analysis it was concluded that the geometric methodology used by TVX on-site was adequate. Therefore, the geometric measurements were used for the mineral resource estimation.

14.5. CLASSIFICATION OF SPECIFIC GRAVITY DATA BY ROCK TYPE

Density determination is critical to this project since these values vary from approximately 2.1 to 6.7 g/cc. These variations are explained by the mineralogical content of the different rock types.

Specific gravity determinations of the Upper West, Olympias West and Olympias East zones were treated separately due to:

- In the Upper West there is a great proportion of weathered material, which is more porous and has less sulphide content than that observed in deeper zones, and therefore the average specific gravity is lower than in the rest of the deposit.
- The sulphide content is considerably higher in Olympias East than in Olympias West being the average grade of samples within the mineralised horizons.

Care was taken to perform specific gravity determinations on all rock types.

The following comments can be made regarding the classification of specific gravity data for each mineralised zone:

- The Upper West zone has a lower specific gravity than Olympias West and Olympias East, the differences being of 3.3% and 9.0% respectively.
- As expected, the massive sulphide (BPG) and arsenopyrite (AsPy) samples have considerably higher specific gravity values than the remaining populations. These higher values are undoubtedly due to the lead, zinc and iron content in mineral species present in both types of mineralisation.

14.6. MULTIPLE REGRESSION OF SPECIFIC GRAVITY VERSUS GRADES

Specific gravity measurements varied widely within the mineralised zone depending on the rock types encountered. The massive sulphide (BPG) had the highest SG values due to the abundance of lead and zinc mineral species. The arsenopyrite zones (ASPY) had the second highest average SG due to the high arsenic and iron content.

Following the review of density and rock type, it was not appropriate to assign an average specific gravity value to each of the mineralised zones. Instead a variable density was applied, reflecting the highly variable sulphide and iron content.

It is clear that gold and silver values do not affect in great measure the specific gravity values. The proportion of these elements is approximately four orders of magnitude lower than the lead, zinc, arsenic and iron content.

Multiple regression analyses were done between specific gravity values and lead, zinc, arsenic and iron grades for the Upper West, Olympias West and Olympias East. Stepwise multiple regression was used so that non- significant variables would not be included in the model. Lead, zinc, arsenic and iron grades were found to be significant and therefore, were included in the regression. The equations and multiple regression coefficients were as follows:

Table 14-2 Multiple Regression Analysis - Specific Gravity

Mineralised Zones	Constant	Fe (%)	Pb (%)	As (%)	Zn (%)	Multiple R
Upper West	2.80342	0.0331261	0.0554123	0.0171990	0.0000000	0.76
West	2.68670	0.0470274	0.0479368	0.0165954	0.0098262	0.82
East	2.58853	0.0429445	0.0461936	0.0283254	0.0207768	0.89

- The variables are shown in order of importance, iron being the most significant variable and zinc the least significant.
- The regression model explained approximately 70% of the variability.

- It is worth noting that the free terms were well within the range of expected specific gravity values for barren rock types.

Block grades were estimated by kriging. The specific gravity of each block was then estimated by applying the regression equations tabulated above to give a specific gravity value for each sample interval and these were then composited and kriged to give specific gravity estimations for each block.

14.7. ESTIMATION METHOD FOR MINERAL RESOURCES

The mineral resource tonnage and grade has been calculated using geostatistical methods within Gemcom mining software. The main steps of the geological estimation process are as follows:

- Construct lithology geological solid models
- Composite drillhole samples into 1 m intervals
- Conduct basic statistics on both the raw and composite assay data sets
- Conduct geostatistical analysis for each element for each lithology
- Generate unconstrained three dimensional resource block models
- Validate the resource block model with primary data

14.7.1. GEOLOGICAL INTERPRETATION AND SOLID GENERATION

Due to the complex geometry and grade variability of the Olympias deposit, detailed three dimensional modelling was required in order to define accurately the boundaries of the mineralisation.

The three dimensional solids were generated based on plans and sections drawn every 25 m where the geology had been previously interpreted at a 1:500 scale. The geological interpretation employed in the construction of plans and sections was conservative and the limits of the deposit were only rarely extrapolated beyond 25 m of the drillhole intersections. The methodology used to generate the solids was triangulation.

Each mineralised zone of the Olympias deposit was modelled separately due mainly to their location, quantity and type of information available for each zone. Therefore, three major separate models were built:

- Upper West
- Olympias West
- Olympias East

14.7.2. DRILLHOLE DATA WITHIN 3-D SOLIDS

14.7.2.1. Olympias West

Some 67,508 m of core were drilled in Olympias West of which 4,309 m were within the solids defined in plan and section. Mean sample grades within the west were: 9.86g/t Au, 134.6 g/t Ag, 4.29% Pb and 5.53% Zn.

14.7.2.2. Olympias East

Of 23,811 m drilled in the Olympias East zone, 445 m were within the defined three dimensional solids. Mean sample grades within the solids were: 15.01 g/t Au, 181.3 g/t Ag, 5.84% Pb and 6.49% Zn.

14.8. COMPOSITING

In order to estimate mineral resources using geostatistical methods it is necessary to ensure that equal sample support is obtained and this is generally achieved by compositing samples.

A study was carried in order to assess any possible biases introduced by the elimination of low recovery samples. The study showed that there was no correlation between core loss and grade and it was concluded that the use of samples with core recoveries less than 60% would not introduce biases in the mineral resource estimation. Nevertheless, for audit purposes it was decided to eliminate them prior to compositing. In order to avoid biases in the mineral resource estimation, below detection limit values were assigned to all elements in the intervals excluded due to poor recovery. This is considered conservative.

14.8.1. COMPOSITE STATISTICS

After the samples with core recoveries below 60% were eliminated and the non-sampled intervals with barren material were assigned below detection limit grades, 1 m composites were generated within the solids, eliminating all composites with lengths below 0.40 m. A summary of the composites for all of the drilling is given in Appendix 1. Table 14-3 summarises the composite statistics within each zone.

Table 14-3 Composited Data - Average Grades Within Each Zone

Mineralised Zone	Au (g/t)	Ag (g/t)	Pb (%)	Zn (%)	As (%)	Fe (%)
Olympias West	9.96	138.2	4.38	5.68	4.62	15.18
Olympias East	14.89	178.7	5.77	6.43	8.23	14.76

Equal weighted histograms, equal weighted normal probability plots and declustered mean versus cell size plots were prepared for each element in each of the five mineralised zones.

The following was concluded:

- The shape of the distributions observed in the histograms showed positive skewness in all cases.
- The normal probability plots showed that the normal model was obviously not applicable. The lognormal model fits the data distribution better; nevertheless, it was not considered a "good fit". Therefore, if simulation studies are required, a normal score transform would have to be used.
- The coefficients of variation were moderately low (of the order of 1.0), except for silver, lead and arsenic in Olympias West where they reached approximately 1.4. It is worth noting that in all the mineralised zones the coefficients of variation of lead and silver were very similar. This is due to the high degree of correlation between these two variables.
- As mentioned previously, a large proportion of the drilling was done as fan drilling from a few underground stations, therefore, clustering was unavoidable. It should be stressed, however, that clustering was not oriented to high-grade areas.

14.8.2. CORRELATION ANALYSIS

Simple correlation analyses were carried out between all elements for each mineralised zone. The highest observed correlations were between gold and arsenic, gold and iron, and silver and lead.

These correlations relate well to the known mineralogy with the presence of gold associated to arsenopyrite and arsenical pyrite, which explains the high correlation between gold-arsenic and gold-iron and the high correlation between silver and lead is due to the occurrence of silver bearing galena.

14.8.3. VARIOGRAPHY AND KRIGING PLAN VALIDATION

The 37 separate lenses of mineralisation in the West of Olympias were separated in to five domains according to their geometric characteristics and the lenses of mineralisation of the East zone were considered as a sixth group. Directional variograms, given in Table 14-4, and omni-directional variograms were run for each group.

Table 14-4 Variogram Calculation Parameters

			Variogram Angle Parameters		
Mineralised Domain	Strike	Dip	Direction	Strike Angle	Dip Angle
Olympias West Group 1	N50E	-20	Strike Dip Perpendicular	50 140 140	0 -20 70
Olympias West Group 2	N140E	-30	Strike Dip Perpendicular	140 50 50	0 -30 60
Olympias West Group 3	NS	-25	Strike Dip Perpendicular	0 90 90	0 -25 65
Olympias West Group 4	N160E	-30	Strike Dip Perpendicular	160 70 70	0 -30 60
Olympias West Group 5	N30E	-25	Strike Dip Perpendicular	30 120 120	0 -25 65
Olympias East Group 1	N25E	-25	Strike Dip Perpendicular	25 115 115	0 -25 65

The omni-directional variograms and the variograms perpendicular to the mineralised domain were calculated using 1 m lag distances with a tolerance of 0.6 m. The strike and down dip variograms were run using lag distances of 5 m with tolerances of 3 m. Angle tolerances of 22.5° were used for all the directional variograms.

The GSLIB non-ergodic algorithm was used to calculate directional variograms. This algorithm was chosen since it is less sensitive to outliers, moderate drifts and edge effects. This is important for small well confined deposits such as each of the Olympias zones.

In many cases, especially in Olympias East the directional variograms showed no consistent structures. In these cases omni-directional variograms were used for kriging.

The directional variograms perpendicular to the mineralised domain often gave similar results to the omni-directional variograms as they sub-parallel to drilling.

The best fitting variograms for each lens are given in Table 14-5:

Table 14-5 Olympias Project (1 - Non-Ergodic Correlograms)

Mineralised Domain	Element	Direction	Nugget(Co)	Type	Sill (C1)	Range (A1)	Sill (C2)	Range (A2)
Olympias West-G1	Au	Omni	0.20	Exp	1.00	9.0	-	-
Olympias West-G1	Ag	Omni	0.20	Sph	0.80	8.0	-	-
Olympias West-G1	Pb	Omni	0.20	Sph	0.80	9.0	-	-
Olympias West-G1	Zn	Omni	0.20	Exp	0.85	8.0	-	-
Olympias West-G1	As	Omni	0.15	Exp	0.85	10.0	-	-
Olympias West-G1	Fe	Omni	0.20	Exp	0.60	12.0	0.60	28.0
Olympias West-G1	SG	Omni	0.20	Exp	1.10	15.0	-	-
Olympias West-G1	S	Omni	0.20	Exp	1.10	12.0	-	-
Olympias West-G1	Sb	Omni	0.10	Exp	0.95	6.0	-	-
Olympias West-G2	Au	Omni-Perp	0.15	Exp	0.50	3.0	0.40	25.0
Olympias West-G2	Au	Strike	0.15	Exp	0.50	30.0	0.40	35.0
Olympias West-G2	Au	Dip	0.15	Exp	0.50	15.0	0.40	35.0
Olympias West-G2	Ag	Omni	0.20	Exp	0.40	8.0	0.50	45.0
Olympias West-G2	Ag	Strike	0.20	Exp	0.40	30.0	0.50	45.0
Olympias West-G2	Ag	Dip	0.20	Exp	0.40	10.0	0.50	45.0
Olympias West-G2	Pb	Omni	0.15	Exp	0.40	7.0	0.50	40.0
Olympias West-G2	Pb	Strike	0.15	Exp	0.40	30.0	0.50	40.0
Olympias West-G2	Pb	Dip	0.15	Exp	0.40	7.0	0.50	40.0
Olympias West-G2	Zn	Omni	0.20	Exp	0.40	5.0	0.40	20.0
Olympias West-G2	Zn	Strike	0.20	Exp	0.40	22.0	0.40	30.0
Olympias West-G2	Zn	Dip	0.20	Exp	0.40	5.0	0.40	30.0
Olympias West-G2	As	Omni	0.15	Exp	0.40	5.0	0.55	30.0
Olympias West-G2	As	Strike	0.15	Exp	0.40	30.0	0.55	45.0
Olympias West-G2	As	Dip	0.15	Exp	0.40	5.0	0.55	30.0
Olympias West-G2	Fe	Omni	0.10	Sph	0.35	3.0	0.55	25.0
Olympias West-G2	SG	Omni	0.10	Sph	0.40	3.5	0.55	25.0
Olympias West-G2	S	Omni	0.10	Exp	0.40	7.0	0.50	50.0
Olympias West-G2	S	Strike	0.10	Exp	0.90	60.0	-	-
Olympias West-G2	S	Dip	0.10	Exp	0.90	60.0	-	-
Olympias West-G2	Sb	Omni	0.10	Exp	0.90	13.0	-	-
Olympias West-G2	Sb	Strike	0.10	Exp	0.90	13.0	-	-
Olympias West-G2	Sb	Dip	0.10	Exp	0.90	13.0	-	-
Olympias West-G3	Au	Omni	0.15	Exp	0.80	8.0	-	-
Olympias West-G3	Ag	Omni	0.15	Exp	0.20	3.0	0.70	45.0
Olympias West-G3	Pb	Omni	0.15	Exp	0.20	3.0	0.65	45.0
Olympias West-G3	Zn	Omni	0.15	Sph	0.75	5.0	-	-
Olympias West-G3	As	Omni	0.15	Exp	0.90	6.0	-	-
Olympias West-G3	Fe	Omni	0.10	Exp	1.00	9.0	-	-
Olympias West-G3	SG	Omni	0.10	Exp	1.00	7.0	-	-
Olympias West-G3	S	Omni	0.10	Exp	0.40	4.0	0.60	25.0
Olympias West-G3	Sb	Omni	0.10	Sph	0.90	6.0	-	-
Olympias West-G4	Au	Omni	0.15	Exp	0.90	1.0	-	-
Olympias West-G4	Ag	Omni	0.20	Exp	0.30	4.0	0.60	45.0
Olympias West-G4	Ag	Strike	0.20	Exp	0.30	4.0	0.60	45.0
Olympias West-G4	Ag	Dip	0.20	Exp	0.30	4.0	0.60	28.0
Olympias West-G4	Pb	Omni	0.20	Exp	0.35	3.0	0.55	45.0
Olympias West-G4	Pb	Strike	0.20	Exp	0.35	20.0	0.45	50.0

Mineralised Domain	Element	Direction	Nugget(Co)	Type	Sill (C1)	Range (A1)	Sill (C2)	Range (A2)
Olympias West-G4	Pb	Dip	0.20	Exp	0.35	3.0	0.65	40.0
Olympias West-G4	Zn	Omni	0.15	Exp	0.40	6.0	0.45	12.0
Olympias West-G4	Zn	Strike	0.15	Exp	0.40	20.0	0.45	25.0
Olympias West-G4	Zn	Dip	0.15	Exp	0.40	6.0	0.45	12.0
Olympias West-G4	As	Omni	0.10	Exp	0.45	6.0	0.55	30.0
Olympias West-G4	As	Strike	0.10	Exp	0.40	10.0	0.50	30.0
Olympias West-G4	As	Dip	0.10	Exp	0.45	6.0	0.55	30.0
Olympias West-G4	Fe	Omni-Perp	0.15	Exp	0.80	6.0	-	-
Olympias West-G4	Fe	Strike	0.15	Exp	0.40	2.0	0.45	40.0
Olympias West-G4	Fe	Dip	0.15	Exp	0.40	2.0	0.45	40.0
Olympias West-G4	SG	Omni-Perp	0.15	Exp	0.73	6.0	-	-
Olympias West-G4	SG	Strike	0.15	Exp	0.20	4.0	0.65	40.0
Olympias West-G4	SG	Dip	0.15	Exp	0.20	4.0	0.65	40.0
Olympias West-G4	S	Omni-Perp	0.15	Exp	0.80	11.0	-	-
Olympias West-G4	S	Strike	0.15	Exp	0.80	35.0	-	-
Olympias West-G4	S	Dip	0.15	Exp	0.80	11.0	-	-
Olympias West-G4	Sb	Omni-Perp	0.10	Exp	0.80	13.0	-	-
Olympias West-G5	Au	Omni	0.15	Exp	0.85	7.0	-	-
Olympias West-G5	Ag	Omni	0.15	Exp	0.85	4.0	-	-
Olympias West-G5	Pb	Omni	0.15	Exp	0.80	6.0	-	-
Olympias West-G5	Zn	Omni	0.15	Exp	0.50	3.0	0.40	25.0
Olympias West-G5	As	Omni	0.15	Exp	0.85	7.0	-	-
Olympias West-G5	Fe	Omni	0.15	Exp	0.85	10.0	-	-
Olympias West-G5	SG	Omni	0.15	Exp	0.85	10.0	-	-
Olympias West-G5	S	Omni	0.10	Sph	0.60	5.0	0.30	18.0
Olympias West-G5	Sb	Omni	0.05	Exp	1.00	10.0	-	-
Olympias East	Au	Omni	0.05	Exp	0.80	7.0	0.25	25.0
Olympias East	Ag	Omni	0.20	Exp	0.60	6.0	0.20	30.0
Olympias East	Pb	Omni	0.20	Exp	0.60	8.0	0.20	28.0
Olympias East	Zn	Omni	0.05	Exp	0.70	8.0	0.40	45.0
Olympias East	As	Omni	0.05	Exp	0.80	8.0	0.22	25.0
Olympias East	Fe	Omni	0.15	Exp	0.90	12.0	-	-
Olympias East	SG	Omni	0.15	Exp	0.90	14.0	-	-
Olympias East	S	Omni	0.10	Exp	0.40	8.0	0.50	35.0
Olympias East	Sb	Omni	0.10	Exp	0.50	6.0	0.70	26.0

The following comments stemmed from the variogram analysis:

- The ranges shown in the above table are the experimental ranges. These had to be divided by three to obtain the range parameters for the exponential models.
- The variogram ranges lie between a few metres and 50 m. Olympias East and Olympias West groups 1 to 4 show similar continuity whilst Olympias West Group 5 (corresponding to Olympias Upper West shows shorter ranges.
- The observed nugget effects varied between 0.05 and 0.20, which is between 5% and 20% of the total sill. This was considered low and could be attributed to the continuity of the mineralisation and the small sampling, sample preparation and assaying errors.

14.8.4. CROSS VALIDATION

The cross validation technique was used for gold only to check the variography and kriging plans. Kriging search parameters employed were the same as were used later for the block estimation. For this study a search radius of 50 m was used since the vast majority of mineral resources are within this distance from sampling data. The following conclusions were drawn:

- The composite means and estimated values were very similar. The standard deviations of estimated values were lower than those of the composites due to the smoothing effect of kriging.
- The slope of the regression lines was slightly higher than 1.00, which is unusual. This is due to the non-sampled barren intervals within the solids, which were assigned below detection limit values. These locations were estimated with neighbouring composites.
- The conditional mean plots showed that the regressions were very close to the first bisector in all cases.
- The observed correlation coefficients were adequate and in general, the overall results were satisfactory.

14.8.5. BLOCK MODEL GENERATION AND ESTIMATION

A partial block model was generated using the Gemcom software. The main parameters of the model were as given in Table 14-6.

Table 14-6 Block Model Parameters

PARAMETER	Olympias West	Olympias East
E Bottom Left Corner	24,186.20	24,115.49
E Top Right Corner	23,566.77	23,620.52
N Bottom Left Corner	-19,245.37	-18,552.41
N Top Right Corner	-17,579.43	-17,350.33
Minimum Z	-646.00	-402.00
Maximum Z	-2.00	-2.00
Model Rotation	N45ºW	N45ºW
Number of Columns	185	125
Number of Rows	202	150
Number of Benches	161	100
Column Width	4.00	4.00
Row Height	8.00	8.00
Bench Height	4.00	4.00

The block size (4.0 m by 8.0 m by 4.0 m) was chosen to relate to mining units and to obtain good edge definition of the geological solids. The model was rotated so that the rows coincide with the direction of the sections, which are perpendicular to the mineralised domains.

Partial block models were generated for each element and for rock type. The partial model was chosen due to the complex geometry of the geological solids. Excavation solids were also generated, in order to allow removal of tonnage from the final block models.

Nine block models were estimated, for: Au, Ag, Pb, Zn, As, Fe, SG, Solid/Category and the partial block model. The estimation of the six grade models and the SG model were carried out using ordinary kriging for the measured and indicated categories. The kriging plans are shown in Table 14-7.

Table 14-7 Olympias Project - Kriging Plans

Parameter	Measured	Indicated	Inferred
Octant search	Yes	Yes	Yes
Min N octants	2	2	2
Max samples per octant	4	4	4
Max samples per hole	8	8	8
Min total samples	4	4	4
Max total samples	32	32	32
Search radius	25	50	200

A first approach for the mineral resource classification was to use of three different kriging radii for gold; these were designed to broadly define the three levels of resource confidence.

- Measured mineral resources were defined using a kriging radius of 25 m since the variograms of the main elements at Olympias West were of this order and because the drillhole spacing is at least of 25 m in the well explored areas.
- Indicated mineral resources were defined using a 50 m radius which represents the most sparsely drilled areas but where geological continuity has been interpreted.
- Inferred mineral resources were defined using a 200 m radius. This large search radius was chosen in order to fill-in those blocks located within the solid that had not been estimated as measured or indicated. It should be stressed that these blocks do not really correspond to the inferred category as defined by CIM and JORC because they lie within a well constrained volume which was interpreted conservatively, based solely on drillhole information, rather than potential geological continuity.

The mineral resource classification was reviewed later, using a data density and geological continuity criteria, rather than the strict statistical approach mentioned above.

14.8.6. BLOCK MODEL VALIDATION

The standard procedures for model validation consist of statistical and graphical checks.

Statistical Validation

This validation technique consists in comparing the grade distribution of the composites against the grade distribution of estimated blocks. The mean values should be similar, while the variability of the blocks should be smaller than that of the composites due to the smoothing effect of kriging. Results indicated that the mean estimated block values for all zones are within or very close to the declustered composite mean range and are satisfactory.

Graphical Validation

Graphical validation consisted of plotting plans and sections showing drillhole composites and block estimates using the same colour codes. The solid contours were also included in these plots. Results of this validation indicated that there was good correlation between composite data and block estimates for all elements. No serious problems in the estimation process were detected.

Drift Analysis

This validation technique consists of dividing the deposit into slices in different directions. For each slice the mean composite grade is compared to the mean block grade. Thereafter, these trends are plotted in order to assess the smoothing caused by kriging.

The main mineralised zones were sliced horizontally in order to obtain vertical trends. The mean composite grade was compared to the mean block grade for gold, silver, lead and zinc. 12 m horizontal slices were used.

In general, block and composite trends were similar, the former being somewhat smoother than the latter. Therefore, the kriging did not produce excessive smoothing.

The vertical trends of silver and lead are similar due to the high correlation between these two elements as mentioned in previous sections.

Validation by Inverse Distance Squared

The main mineralised zones, the Upper West - High Grade, Olympias West and Olympias East were also estimated using Inverse Distance Squared (ID^2), using the same 3-dimensional solids, data and search parameters as for kriging. The kriging and ID^2 estimates were compared for each mineralised zone. Scatter plots showing kriging v/s ID^2 estimates for each block and conditional means plots of kriging v/s ID^2 estimates grouped according to kriging estimates were prepared for gold.

In general, scatter plots show that points are tightly distributed about the first bisector, indicating that the two estimates for each block are similar. An important anomaly was observed in the Upper West - High-Grade zone, where some blocks have significantly higher kriged than ID^2 grade values.

From the validation work performed, it was concluded that the block model is a satisfactory representation of the geology and grade distribution observed in the drillholes.

14.9. SURFACE MATERIAL

The Olympias Project has surface mineral resources, which are scheduled to be processed once production commences. These are the now exhausted arsenopyrite stockpiles and the existing tailings.

The Olympias tailings pond consists of two cells (East and West) located in the flood plain 500 m North of the Olympias Mill. During the time that the Arsenopyrite stockpiles were being drilled, a drilling campaign was also conducted over the tailings pond to determine:

- Total tonnage of tailings
- Remaining storage capacity
- Grades of tails
- Specific Gravity
- Moisture

A total of 83 holes were drilled into the tails.

The calculations undertaken are summarised below:

- Survey of tails surface and soil berms to create the upper surface

- Use end-of-hole depths of the holes to create the lower surface
- Calculate volume using Gemcom
- Composite samples into equal lengths
- Definition of the block model
- Calculate block values through kriging
- Final tonnage and grade calculations.

Utilising the measured specific gravity of 1.6 g/cm^3, the tonnage and grades for the Olympias tailings are:

Table 14-8 Olympias Tailings

Tonnes	Grade	
	Au g/t	Ag g/t
2,408,403	3.42	14.25

14.10. DEFINITION AND TABULATION OF MINERAL RESOURCES

The first approach for classifying mineral resources for the Olympias deposit used search radii of 25 m for measured mineral resources, 50 m for indicated mineral resources, and 200 m for inferred mineral resources. This classification was done for all elements according to the gold block model.

This approach was considered conservative, and appeared impractical for the following reasons:

- Olympias west: the areas in the top levels, were interpreted using information derived from mapping of underground excavations and bazooka type in-fill drilling, a significant proportion of which was not used in the estimation due to poor core recovery, therefore these blocks were classified as inferred mineral resources. It was felt, however, that due to the high confidence in geological knowledge of the area and closeness to underground development, these blocks should be placed at least in the indicated category.
- The Upper West - High Grade zone is also well developed, however applying the definitions so strictly resulted in several blocks of inferred mineral resources within the block model.
- The Lower West solid also exhibits small inferred “islands” in what is a predominantly indicated resource solid, such categorisation does not make sense.
- As for Olympias West, the small inferred “islands” within indicated zones did not make sense.

After careful consideration, the decision was taken to use kriging radii based on drillhole density as a measure of resource confidence. The CIM and JORC classification has therefore been applied through the following set of practical definitions and guidelines:

Measured Mineral Resources: All such mineral resources contained within solids within a 25 m search radius.

Indicated Mineral Resources: All such mineral resources contained within solids measuring between a 25 m and a 50 m search radii. In addition the Upper West High-grade zone was included in the indicated mineral resource category since there are many underground workings and enough drilling in the remnant areas.

Inferred Mineral Resources: Inferred mineral resources have been defined in two ways:

All resource blocks greater than 50 m search radii. In some cases it was found that inferred blocks fell within stopes that were generally made up of measured or indicated and this is illogical. In these cases the inferred blocks were given an indicated classification. The total inferred mineral resource tonnage which was changed to indicated in this way was 46,017 t.

Lower confidence mineral resources, in solids but not block modelled. The estimated grade is extrapolated from the nearest blocks. The inferred mineral resources not included in the block model form the southern extension to the main western mineralised domain.

The estimation meets the CIM and JORC criteria for NI 43-101 and can be regarded as current.

Table 14-9 Updated Olympias Mineral Resources

	'000t	Au g/t	Au Moz	Ag g/t	Ag Moz	Pb %	Pb '000t	Zn %	Zn '000t
Measured Underground	8,137	10.0	2.60	147	38.5	4.9	400	6.6	535
Indicated Underground	4,298	10.0	1.39	161	22.3	5.4	230	7.1	304
Total M+I Underground	12,435	10.0	3.99	152	60.8	5.1	630	6.7	839
Measured Tailings	2,408	3.4	0.27	14	1.1	-	-	-	-
Total M+I	**14,843**	**-**	**4.26**	**-**	**61.9**	**-**	**630**	**-**	**839**
Inferred Underground Inside block model	793	12.4	0.32	179	4.6	5.9	47	6.8	54
Inferred Underground Outside block model	873	5.6	0.16	133	3.7	4.9	43	7.5	65
Total Inferred	**1,666**	**8.9**	**0.47**	**155**	**8.3**	**5.4**	**90**	**7.2**	**120**

Mineral Reserves are included in Measured and Indicated Mineral Resources.
Mineral Resources that are not mineral reserves do not have demonstrated viability.
Figures in the tables may not sum due to rounding.

The strict quality control procedures in place at Olympias and the numerous statistical checks at all stages of the resource estimation processes ensured that a high standard of data verification was in place at all times. The data and resource were verified and audited independently by Behre Dolbear of New York and SRK of the UK. The subsequent feasibility studies by Kvaerner Metals and NGL Ingenieria y Construccion S.A. involved independent auditing and verification of all data and procedures on site. The classification of resources used in this report has not been verified by a Qualified Person who is independent of EGL, however it conforms to industry standards for this kind of massive sulphide deposit.

15. MINERAL RESERVE ESTIMATES

Previous mining at Olympias was in the West Orebody above the -220 m level. The proposed future mining is completing the mining of mineral reserves remaining in these areas, the down dip extension to the West Orebody and the fully explored but unexploited East Orebody. There are a total of 13.6 Mt of proven and probable mineral reserves remaining in the Olympias mine which will support a maximum mining rate of approximately 800 ktpa to 850 ktpa. The geotechnical conditions described below influence the choice and layout of mining methods. Historically, these methods chosen for future mining are equal or similar to those that have historically proven to be appropriate for the Olympias orebody. Thus, no risk is anticipated in the mining method.

15.1. UNDERGROUND MINERAL RESERVES

Mineral reserves were then derived from measured and indicated mineral resources by application of economic factors including metal prices, process recoveries and net smelter return to arrive at an economic cut-off grade which was then applied to each stoping block within the model. Due to the sharp geological contact between mineralised rock and waste and the mineralisation grades, no blocks were discarded due to cut-off. The blocks were factorised for anticipated dilution and mining recovery dependent on the mining category of each block.

- Mining Recovery was set at 95%.
- For waste rock dilution, an allowance has been made for discontinuities in the deposit and failure to follow the contact accurately. Additional waste dilution is assumed at 15% and to have zero grade.
- Surface stockpiles of tailings yielding further gold bearing concentrates are directly recoverable and convert from mineral resources to mineral reserves with no dilution or recovery applied.

The proven and probable underground mineral reserves for the Olympias deposit are summarised in Table 15-1:

Table 15-1 Updated Olympias Mineral Reserves

	'000t	Au g/t	Au Moz	Ag g/t	Ag Moz	Pb %	Pb '000t	Zn %	Zn '000t
Proven Underground	8,886	8.7	2.47	128	36.5	4.3	380	5.7	508
Probable Underground	4,686	8.7	1.32	140	21.2	4.7	219	6.2	288
Total underground	13,572	8.7	3.79	132	57.7	4.4	599	5.9	796
Proven Tailings	2,408	3.4	0.27	14	1.1	-	-	-	-
Total	15,980	-	4.06	-	58.8	-	599	-	796

Mineral Reserves are included in Measured and Indicated Mineral Resources.
Figures in the tables may not sum due to rounding.

16. MINING METHODS

16.1. GROUND CONDITIONS

Previous mining has generated a lot of experience with the ground conditions and the rockmass physical and geotechnical characteristics.

The footwall and hanging wall rocks are generally gneiss. The orebody lies within the marble horizon, but the top of the ore may extend to the faulted geological contact with the gneiss. In general, the footwall and orebody rocks can be described as Fair with Poor conditions relating to the presence of Kaolinite. This kaolinite is often present in the ore at the immediate hanging wall and results in adopting modified mining sequences.

Table 16-1 gives the average Uniaxial Compressive Strength (UCS) of the Olympias rock types and Table 16-2 gives the rockmass properties.

Table 16-1 Uniaxial Compressive Strength (UCS) of Olympias Rock Types

Geological Formation	UCS (MPa)
Marble	108
Ore	84
Gneiss	126
Kaolin	1

Table 16-2 Rockmass Properties of Olympias Horizons

	RQD (%)	IRS (MPa)	RMR	Density (t/m^3)
Upper Hanging wall	30	85	45	2.7
Immediate Hanging wall	50	125	42	2.7
Orebody	40	84	45	3.8
Footwall	40	118	45	2.7
Faults	10	15	12	2.4

This data has been input into geotechnical models to determine stope stability and support requirements for the Olympias mining. A range of spans from 5 m to 9 m is possible in the transverse drift stopes depending on ground conditions and support. The span is maintained at 5 m for the purpose of this plan to compute mineral reserves.

16.2. SUPPORT

Table 16-3 below shows the minimum support requirements for the development ends and drifts as determined by geotechnical modelling.

Table 16-3 Support Required for Ore and Waste Headings

	1 bolt/2 m^2	25 mm Shotcrete	50 mm Shotcrete
Ore Drift Roof	100%	12%	12%
Ore Drift Walls	60%	7%	7%
Development Roof	100%	5%	3%
Development Walls	40%	5%	3%

Additionally, fibre reinforced shotcrete is used in the kaolinised areas.

16.3. SURFACE SUBSIDENCE FROM BACKFILL MINING

A geotechnical simulation of the recent backfilled and proposed future backfilled mining zones has been carried out for the Stratoni mine and the results are equally applicable for the backfill mining at Olympias. The backfill prevents caving and collapse into the workings so that the only mining induced deformation is elastic.

The mining simulation gives theoretical maximum lowering of the surface at its final long term subsided position of 4.5 millimetres (mm) based upon elastic deformation. With these levels of movement it was concluded that no damage will be caused to the existing and future surface installations.

16.4. SEISMICITY

The future mining at Olympias is not considered a likely trigger for seismicity due to the relatively small amount of mining and the use of backfill to fill the voids. Shaking from regional seismicity has been experienced in the past without damage being reported from underground.

16.5. MINING OVERVIEW

The ore zones at the Olympias Project are variable in ore geometry and ground conditions. The ore contacts are well defined and are often irregular on the footwall. The high grades associated with these types of ore dictate that a selective mining method will be used. The mining method will be conventional transverse and longitudinal Drift & Fill. A double lift Drift & Fill method (Mini Bench & Fill) in wide orebody areas has been considered but is only applicable to approximately 15% of the reserve and only in very good, stable geotechnical hangingwall conditions. As a result, the mineral reserves have been computed based solely on the conventional Drift & Fill method. A conventional drill and blast and load-haul-dump (LHD) method of mining will be employed in both production and development. The method is flexible allowing headings to change direction with changing ore geometry.

The overall geometry of the Olympias East and West orebodies is shown in Figure 16-1. The gold shaded area is mined out with Sub-level Cave or drift & fill or undercut & fill. The brown and green areas are planned areas of drift & fill.

16.6. RAMPS AND ACCESS CROSSCUTS

An existing ramp has been driven in the footwall from surface at +50 m down to -230 m level. This ramp will be enlarged and resupported to allow access and ventilation. This existing ramp will form the West Ramp from the -110 m junction (with the new Olympias Decline) and will eventually be extended to the base of the orebody at -630 m level. A new Olympias Decline of 1,300 m will be developed from surface in the area north west of the concentrator to intersect the existing ramp at -110 m where a new East Ramp will commence to access the East ore body. This decline is necessary primarily for ventilation purposes but also provides an ore/waste truck haulage route directly to the process plant on surface in the initial years. Access crosscuts to intersect the orebody will be driven from the main West and East ramps.

The 8.5 km Stratoni Decline is planned to the base of the ore at Olympias. This will allow the ore to be trucked to the new Olympias ore concentrator at Stratoni during year 9 with coarse tailings for backfill returning by this decline.

16.7. STOPE DEVELOPMENT

Production will commence after the access crosscut where the ramp reaches the footwall of the orebody, usually midway along its strike length. The crosscut is driven through the orebody to expose the hanging wall. The stope heading is currently designed at 5m x 5m. This may be adjusted to allow for pinching and swelling.

The mining method is expected to be longitudinal or transverse Drift & Fill depending on orebody geometry. If the distance between the hanging wall and the footwall is very variable from narrow to wide, then a mixed method of longitudinal and transverse would be adapted to suit the conditions.

Generally, for footwall to hanging wall thickness of 10 m or less, the stope will be developed for longitudinal drift & fill mining (see Figure 16-2). This involves developing on the footwall contact avoiding exposing poor hanging wall ground conditions. After completion of the footwall drift, depending on the orebody width and ground conditions, the ore on the hanging wall side will be either stripped on the retreat, or the drift will be filled and a second drift on the hanging wall side started.

For a thickness greater than 10 m, the transverse drift & fill method is preferable (see Figure 16-3) whereby a drift is driven along the centre of the orebody from which transverse drifts are mined to the hanging wall and footwall on the retreat from the ends of the orebody. This method of mining from footwall to hanging wall has the advantage of offering increased hanging wall stability by reducing the area of exposure at any one time. Where primary and secondary mining is scheduled, productivity is also increased as a single stoping level will have many more available faces than with the longitudinal method.

Ore is removed from the stopes after blasting using load haul dump machines. It is tipped into the orepass system alongside the main ramp or in the lower areas directly into the dump trucks. A loading bay is developed if logistically necessary. The stoped area is then filled.

16.8. BACKFILL

Conventional cemented hydraulic backfill has been used at Olympias since 1988 when the mining method was changed to Underhand Cut & Fill to limit surface caving. It is currently in use at Stratoni so the process is well understood.

Only the coarse tailings fraction is used for backfill to maximise drainage of water. A mass balance has indicated that all of the coarse tailings will be required for underground backfill at Olympias precluding the need for a large TMF. The fine tailings will be trucked from both the Olympias concentrator and the new concentrator to the TMF at Stratoni. In the final phase of mining the ore is trucked up the Stratoni Decline and processing of ore takes place at Stratoni. The coarse tailings will then be trucked back down the decline to the -210 m level and either used at the backfill plant on this level or pumped using GEHO pumps to the backfill plant on surface at Olympias.

The stope is prepared with suspended fill discharge pipes to the highest points and barricaded at the neck of the development drive with timber round poles, planks and filtration fabric. In some limited areas where previous mining requires Hellas Gold to mine in a downward mining sequence, the floor is covered with reinforcing mesh before filling with backfill of increased cement content. Additionally, ties of 20 mm diameter rebar with plates will help to support the mesh and reinforce the slab. Fill is poured via 130 mm and 150 mm pipes from surface at a rate of approximately 40 m^3 per hour. Tight fill is essential to safe operation in drift and fill mining. The method of achieving tight fill at Olympias is to develop the drifts at a 2% upgrade. Fill pipes with breather pipes are placed at the middle and the furthest end of the stope. The filling starts at the middle pipe until the tails appear in the breather pipe, then filling changes to the end fill pipe. This works well when closely supervised and the 2% gradient is sufficient for tight fill without undue pressure knocking the barricade down.

16.9. UNDERGROUND MINING FLEET

The mining fleet is listed in Table 16-4 Mining and Development Fleet.

Table 16-4 Mining and Development Fleet

Description	Quantity
Advance Jumbos	10
Support Jumbos	8
Charging+Services Plat.	9
LHD	8
Trucks	6
Trucks Loaders	3

16.10. UNDERGROUND MINING PRODUCTION PLAN

Table 16-5 shows the scheduled production tonnes and grade for Olympias mine life. This ore is initially processed through the refurbished Olympias concentrator and subsequently through the new concentrator. Recovery and dilution factors are discussed in the previous Section.

Table 16-5 Mining Schedule for Olympias Tailings and Ore

OLYMPIAS	Unit	Total/Avg	Tailings Phase			Part Year	Olympias Concentrator Phase			
1. PRODUCTION										
			Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8
Orebody		13,572,734								
- Upper West	(t)	581,800	-	-	-	14,489	30,235	50,533	58,022	73,631
- Inter West	(t)	1,492,161	-	-	-	56,803	165,724	115,192	109,804	85,045
- Lower West	(t)	7,372,492	-	-	-	-	65,727	157,587	177,224	176,538
- South Extension	(t)	2,533,573	-	-	-	-	-	-	-	-
- Lower East	(t)	1,013,925	-	-	-	-	26,164	34,340	27,644	27,212
- Upper East	(t)	578,783	-	-	-	10,016	33,467	32,116	25,371	41,417
Total ROM	(t)	13,572,734	-	-	-	81,308	321,317	389,768	398,065	403,843
	(tpd)									
Grade										
Au	(g/t)	8.70	-	-	-	9.80	10.06	9.68	9.53	9.91
Ag	(g/t)	132.35	-	-	-	111.14	128.03	140.41	140.18	121.66
Pb	(%)	4.42	-	-	-	2.48	3.94	4.46	4.53	3.98
Zn	(%)	5.89	-	-	-	3.15	5.15	5.14	4.97	4.86
Tailings	(t)	2,400,000	430,000	720,000	720,000	530,000				
Au grade	(g/t)	3.40	3.40	3.40	3.40	3.40				
Total processed Rom and Talings	(t)		430,000	720,000	720,000	611,308	321,317	389,768	398,065	403,843

OLYMPIAS	Unit	Stratoni New Concentrator Phase								
1. PRODUCTION										
		Year 9	Year 10	Year 11	Year 12	Year 13	Year 14	Year 15	Year 16	Year 17
Orebody										
- Upper West	(t)	77,216	80,146	75,026	51,576	42,582	28,344	-	-	-
- Inter West	(t)	87,308	83,523	86,999	91,529	91,723	94,738	79,484	78,581	74,140
- Lower West	(t)	297,325	292,918	360,486	370,574	369,338	396,548	444,021	443,506	479,084
- South Extension	(t)	142,964	203,505	207,191	226,085	226,161	200,489	207,483	211,917	199,811
- Lower East	(t)	72,780	82,475	70,714	70,306	70,509	70,360	70,872	66,961	71,972
- Upper East	(t)	51,317	49,224	45,858	35,981	43,289	34,289	15,182	17,203	19,594
Total ROM	(t)	728,910	791,791	846,274	846,051	843,602	824,768	817,042	818,168	844,601
	(tpd)	2,893	3,142	3,358	3,357	3,348	3,273	3,242	3,247	3,352
Grade										
Au	(g/t)	8.17	8.80	8.92	8.44	8.09	8.32	7.92	8.33	8.35
Ag	(g/t)	115.82	136.32	131.80	139.56	132.12	127.27	130.20	124.18	129.10
Pb	(%)	3.93	4.50	4.30	4.55	4.42	4.25	4.41	4.18	4.49
Zn	(%)	5.49	5.81	5.33	5.76	5.77	5.79	5.89	6.01	6.24
Tailings	(t)									
Au grade	(g/t)									
Total processed Rom and Talings	(t)	728,910	791,791	846,274	846,051	843,602	824,768	817,042	818,168	844,601

OLYMPIAS	Unit	Stratoni New Concentrator Phase							
1. PRODUCTION									
		Year 18	**Year 19**	**Year 20**	**Year 21**	**Year 22**	**Year 23**	**Year 24**	**Year 25**
Orebody									
- Upper West	(t)	-	-	-	-	-	-	-	-
- Inter West	(t)	33,015	-	-	-	-	-	33,544	125,009
- Lower West	(t)	471,064	509,272	518,568	562,242	425,331	400,089	303,004	152,046
- South Extension	(t)	198,695	158,166	124,777	106,697	85,306	34,326	-	-
- Lower East	(t)	81,148	72,418	71,855	26,195	-	-	-	-
- Upper East	(t)	18,490	17,269	20,000	22,057	-	15,352	22,089	9,202
Total ROM	(t)	**802,412**	**757,125**	**735,200**	**717,191**	**510,637**	**449,767**	**358,637**	**286,257**
	(tpd)	**3,184**	**3,004**	**2,917**	**2,846**				
Grade									
Au	(g/t)	8.59	8.84	9.68	8.40	8.00	8.59	9.56	9.36
Ag	(g/t)	133.93	129.64	145.70	133.90	146.52	130.52	136.34	139.39
Pb	(%)	4.62	4.39	4.88	4.52	4.98	4.39	4.60	4.73
Zn	(%)	6.61	6.46	6.72	6.25	6.61	5.79	6.05	5.73
Tailings	(t)								
Au grade	(g/t)								
Total processed Rom and Talings	(t)	**802,412**	**757,125**	**735,200**	**717,191**	**510,637**	**449,767**	**358,637**	**286,257**

16.11. MINING – TAILINGS PHASE

The existing underground works are rehabilitated and brought up to the standard required to progress the Olympias Project. The main items are to:

- Rehabilitate the existing ramp from the mine surface to the base of the existing shaft, enlarging the cross section where necessary and re-supporting with bolts and shotcrete.
- Develop new Olympias Decline from the owned property north west of the concentrator plant to intersect the new East Ramp and connect to the existing enlarged ramp.
- Completion of the Olympias Decline enables the development of the Upper East Ramp, -250 m Level Haulage and West Ramp and Lower East Ramp. Develop ventilation drifts/raises, ore passes and accesses to ore associated with both East and West Ramps.
- Rehabilitate and install surface facilities as necessary.
- Strip and make safe the current shaft such that it acts efficiently as a main ventilation airway.
- Install new electrical and communications systems.
- Install new pumps and pipe ranges in the shaft and ramps.
- Install new ventilation fans.
- Install new backfill plant on surface.
- Develop underground facilities (workshops, offices, refuelling facilities, etc.).
- Commence Stratoni Decline development from Stratoni.

16.12. MINING – MIXED AND OLYMPIAS CONCENTRATOR PHASES

Mining of ore starts from late Year 4 onwards for a total of just over 4 years. Production rises to a rate of 400ktpa. All ore and waste is trucked out of the Olympias Decline to surface for processing and disposal.

- All major development is completed during this phase including the -250 m Level and -600 m Level Haulages, the West Ramp, Lower East Ramp. The associated infrastructure, ventilation drifts/raises, ore passes and accesses to ore associated with both East and West Ramps are developed to match ore production requirements.
- Ore production is from the Upper East orebody and the West Upper and Intermediate Orebody.
- Development of the Stratoni Decline completes during Year 8.

16.13. MINING – STRATONI CONCENTRATOR PHASE

Ore production rises to 729 ktpa in Year 9 and then fluctuates between 790 ktpa and 846 ktpa between Year 10 and Year 18. Ore production declines towards the end of mine life from 757 ktpa in Year 19 to 286 ktpa in the final Year 25. All ore and waste is trucked out of the Stratoni Decline to surface for processing and disposal.

- The associated infrastructure, the ventilation drifts/raises, ore passes and accesses to ore associated with both East and West Ramps continue to be developed to match ore production requirements.
- Ore production is from all areas of both orebodies with the Upper West exhausting in Year 14. The Intermediate West, excepting some pillars taken in years 24 and 25, exhausts in Year 18. The South Extension exhausts in Year 24 and the Lower East in Year 22. The remaining Upper East and Lower West areas run through to Year 25 although the production drops as much of the production is in pillar extraction.

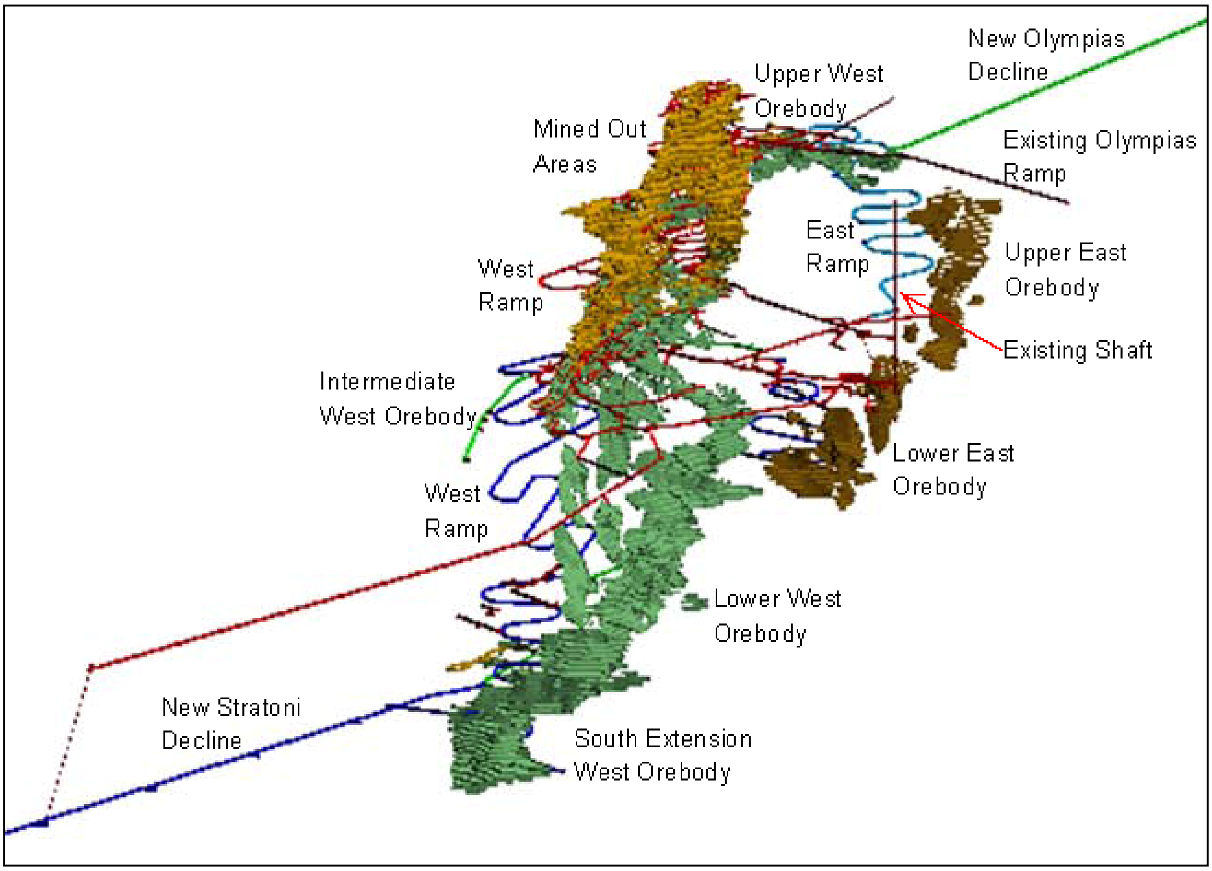


Figure 16-1 General Isometric View of Mining

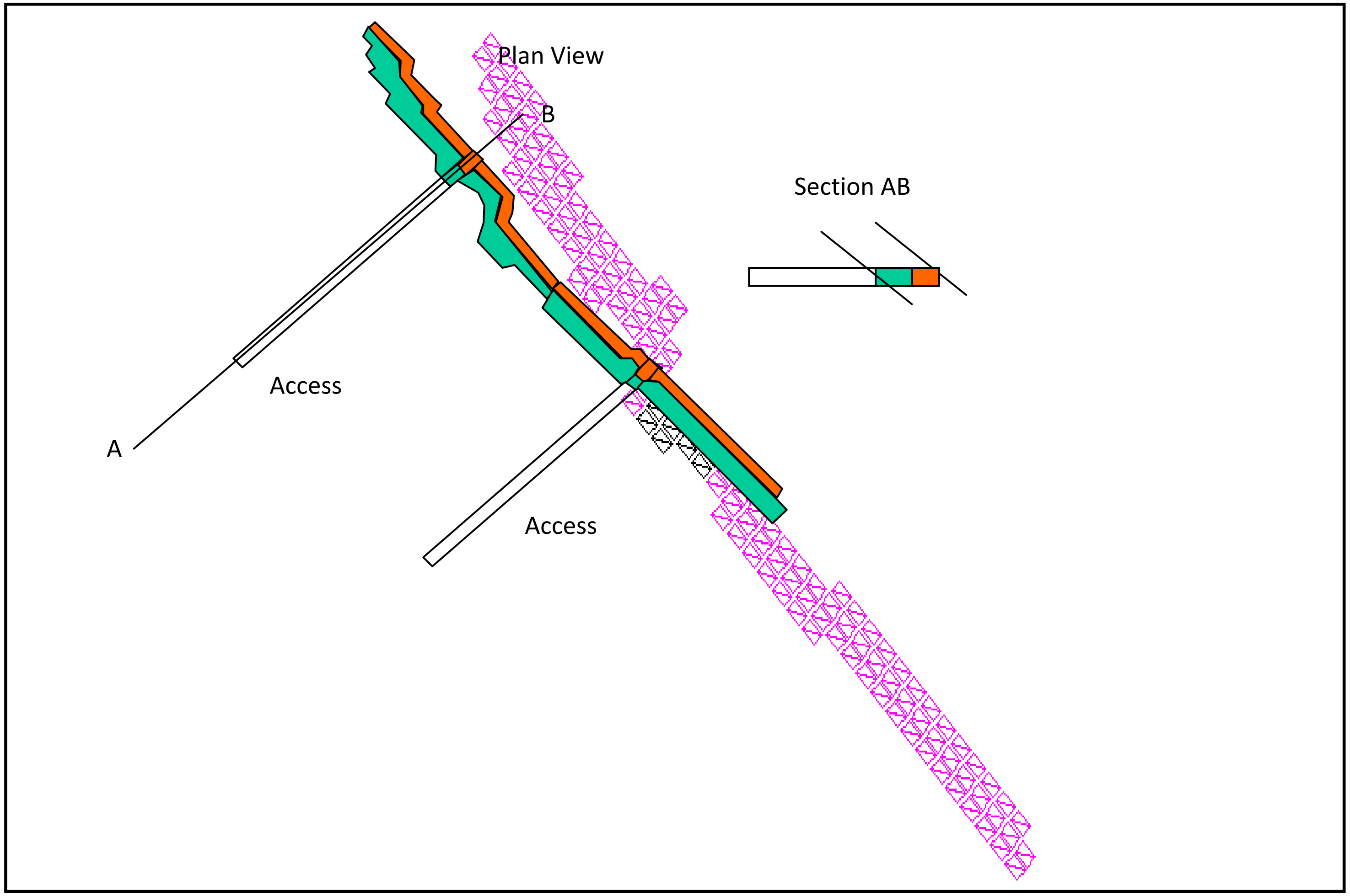


Figure 16-2 Longitudinal Mining to a Narrow Area of the Orebody

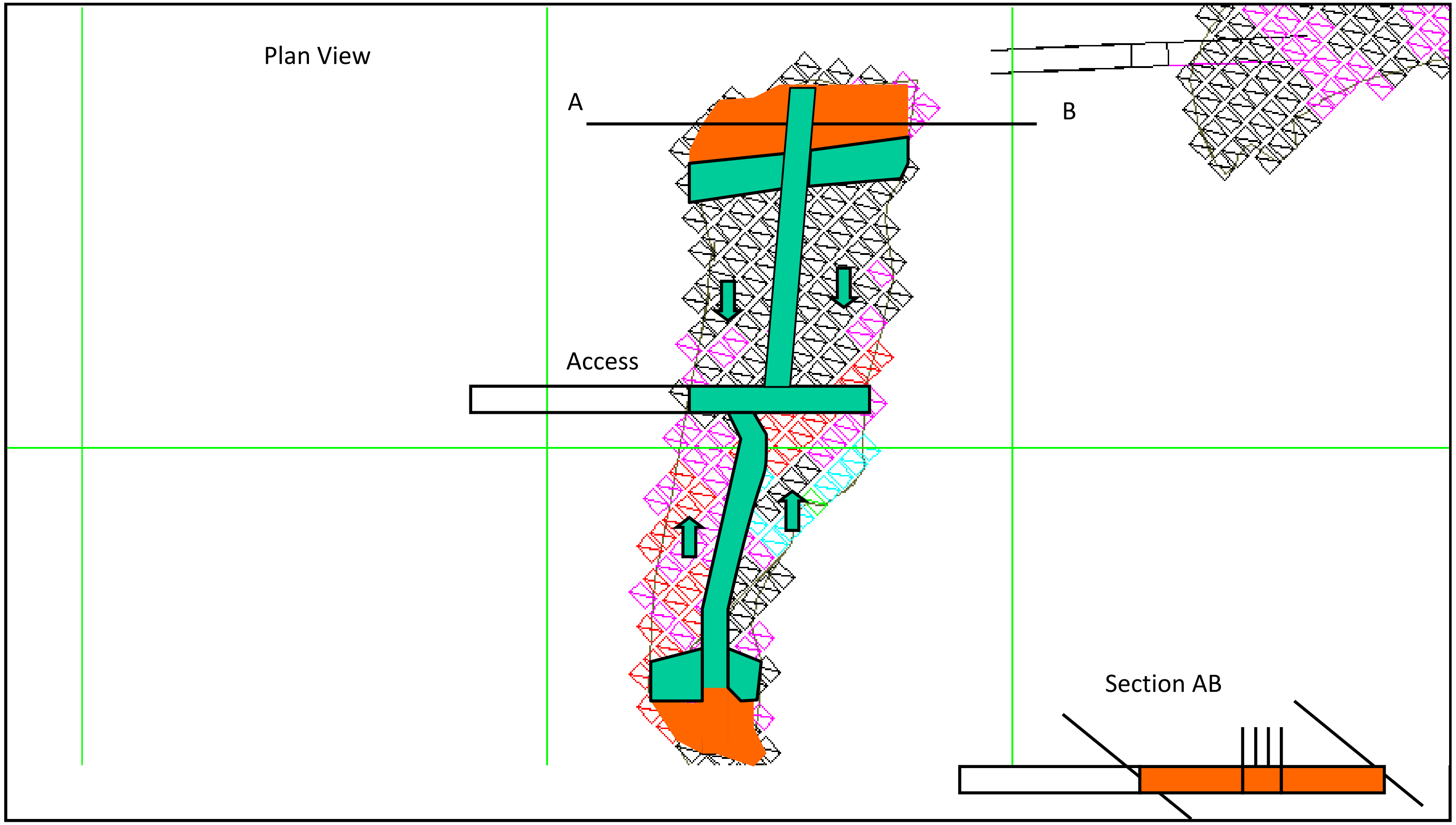


Figure 16-3 Transverse Mining to a Wide Area of the Orebody

16.14. MINE WATER MANAGEMENT

The drainage and pumping system at Olympias is divided into the following two systems:

- Shaft pumping system
- Ramp pumping system

Both current systems employ stage pumping rather than high head single lift. The maximum vertical lifts are about 150 m on the shaft and about 40 m on the ramp system. Both systems will be replaced in the early years of development.

16.14.1. GROUND WATER INFLOW

Water inflow has been predicted to increase to a maximum of 650 m^3/h when mining expands into the eastern orebody and below -210 m level in the western orebody. By Greek law, the main pumping capacity needs to be 1,300 m^3/h and standby pumping capability of 650 m^3/h is also required. This requires additional capacity. New 300 mm pipes will be installed in the shaft coupled to multi-stage centrifugal pumps as the primary pumping system. A new standby facility will also be installed. Allowance has also been made to pump up the ramps to the centralised sump feeding the shaft pumps.

17. RECOVERY METHODS

17.1. INTRODUCTION

The Olympias Project is being developed in phases. Initially the Olympias Project will utilise the rehabilitated existing concentrator plant at Olympias to treat reclaimed existing tailings for 3 to 4 years and will then be supplied by ore mined underground for a further 4 years. A new concentrator is scheduled to be built on a brownfield area at the Stratoni mine site ready for year 9 of the operation to accommodate increased ore production 850,000 dtpa which will be delivered by trucks through a decline tunnel linking the Olympias mine to the new concentrator.

In both phases, the concentrates produced from run of mine ore will be:

- lead/silver concentrate
- zinc concentrate
- gold bearing pyrite / arsenopyrite concentrate

The metal concentrates will either be trucked to Hellas Gold's Stratoni port facilities for bulk sea freight shipment or stuffed into containers and transported to Thessaloniki for export.

It is the intention to construct a gold plant although the process technology used will depend on continuing technical and financial evaluation. When the gold plant is commissioned, which will also be located at Stratoni, the pyrite material will be processed to a copper/gold matte for sale.

17.2. THE EXISTING REHABILITATED OLYMPIAS CONCENTRATOR

The Olympias mine and concentrator were commissioned in 1976 but have not been operated since production stopped in 1995. This was due primarily to the depressed metal prices at the time which made it uneconomic to continue operations.

During historic operation lead concentrates and zinc concentrate was sold and gold bearing pyrite / arsenopyrite concentrate was stockpiled. The stockpile of gold bearing pyrite / arsenopyrite concentrate has since been sold to off-takers by EGL. The historic recovery of gold bearing pyrite / arsenopyrite concentrate was inefficient and a significant quantity reported to the tailings management facility (TMF) adjacent to the mine. Approximately 2.4 Mt grading 3.4 g/t gold was accumulated and these tailings will be reclaimed and directed to the concentrator in the first 3 to 4 years of operation at up to 720,000 dry tonnes per annum (dtpa).

Ore mined from the developed zones of the underground mine will then be fed to the plant at a scheduled rate of 400,000 dtpa for a further 4 years.

Power and water supplies to the existing plant are in place and the infrastructure and access are good.

The plant had been shut down properly and the mills ground out. Complete mechanical and electrical overhaul are required and replacement of missing equipment, primarily flotation cells, pumps, filters, electrical distribution and a new control system. The plant has been audited and an exercise carried out by a Greek engineering contractor called Renewable to identify the missing equipment. This has been completed and a cost estimate compiled. Rehabilitation work to the buildings commenced in mid 2010 and orders have been prepared for the new plant equipment, though not yet placed.

The grinding, flotation and concentrate filtration sections are housed in an enclosed building and the main structural members are reinforced concrete which have been fully refurbished and are structurally sound. The walls have been repaired by sand blasting and applying shotcrete, the windows have been replaced and a new roof mounted.

The original design capacity of the concentrator was ~40 tph of ROM ore, equivalent to approximately 310,000 tpa, although the plant had operated efficiently at higher throughputs on occasion when required. The fully refurbished plant which includes a new process control system will be able to treat 50 tph continuously.

17.3. REPROCESSING EXISTING TAILINGS

The flotation tailings were previously directed to the Tailings Management Facility (TMF) at the Olympias site and are stored in two paddocks with a dividing wall. As stated earlier, these tailings will make up the initial feed to the rehabilitated concentrator for the first 3 years or so of operation which is scheduled to commence in 2012. This feed material will be mechanically reclaimed and re-pulped. The slurry will be pumped to a cyclone and the underflow passed through the ball mill, this is primarily to de-agglomerate the solids prior to flotation. However should it prove necessary to grind the cyclone underflow to maximise metallurgical performance the ball mill will be charged with suitably sized media. The cyclone overflow will be directed to conditioning tanks, reagents added and the conditioned pulp will flow to the flotation section where the gold bearing minerals will be floated in rougher, scavenger and cleaner stages. The high grade gold bearing concentrate will be thickened and filtered ready for despatch to market.

The recovery of gold from the reclaimed tailings is estimated to be about 91% to a concentrate grading around 22 g/t Au, based on previous plant experience and pilot plant and laboratory testwork.

17.4. PROCESSING RUN OF MINE ORE IN THE EXISTING MILL

Once the stored tailings have been exhausted, the flotation circuit will be slightly modified so that it can produce the three concentrates: lead/silver concentrate; zinc concentrate and the gold bearing pyrite / arsenopyrite concentrate.

Ore will be directed from the underground mine to the crushing plant producing a crushed product with a nominal sizing of 80% passing 12 mm and thence to the grinding mills where the solids will be milled to give a sizing in the region of 80% passing 180 microns. The crushed ore will be transferred to the fine ore bin ahead of the rod mill and the secondary ball mill. The overflow from the hydro-cyclones classifier will be directed to the flotation circuit. The flotation section will produce three concentrates, firstly lead/silver, secondly zinc and thirdly the refractory auriferous arsenical pyrite concentrate.

Separation of the minerals into the three concentrates is achieved through a combination of pH control and conventional reagents for the depression and activation of the various mineral species as appropriate. The plant is being refurbished with mechanical flotation cells with a capacity of 3 m^3 units for roughing and scavenging and 1.5 m^3 for cleaning. The concentrates will be directed to their respective thickeners and filters, conveyed to storage ready for despatch to market.

The tailings from the concentrator will be separated into course and fine fractions, the fine fraction, which is about 20% of the total and water treatment plant sludge, will be filtered by a new filter press installed during the plant rehabilitation programme and the fine fraction transported as filter cake to Stratoni for disposal on the existing TMF. In the first years of operation before mining has been established, the course fraction of the residue from the tailings phase will be used by local contractors as aggregate.

In the medium term the coarse tailings will be used for the underground backfill requirement and there is no long term surface disposal requirement for the coarse tailings. The fine tailings will be filtered and transported as filter cake to a new TMF at Kokinolakkos, adjacent to the EGL's Stratoni mine site.

The metallurgical performance of the plant when processing ore will match the previous results and are summarised in Table 17-1.

Table 17-1 Olympias Flotation Recoveries for Run of Mine

Lead Concentrate				Zinc Concentrate		Pyrite/Arsenopyrite Gold Concentrate			
Recovery		Grade		Recovery	Grade	Recovery	Grade		
Pb%*	Ag%*	Pb%	Ag g/t	Zn %	Zn %	Au %	Au g/t	As %	S %
91	+/-83	63	+/-1800	+/-91	51	+/-85	22	9	40

*On the resumption of operations lead and silver recoveries may be below expectation due to oxidation of the near surface ore. An allowance has been made for this in the business plan.

There is minimal risk associated with the concentrator process as the Olympias plant had operated successfully for many years producing concentrates within the set metallurgical parameters. Further, Hellas Gold has operated the Stratoni concentrator plant continuously since 2005 and has a thorough understanding of what is required to successfully operate and manage such plants.

17.5. THE NEW STRATONI CONCENTRATOR

17.5.1. PROCESS

As the Olympias Project develops, a new concentrator plant will be constructed. This will be located at the Stratoni site close to the old Mavres Petres works and will be supplied by trucks through the newly excavated decline from the Olympias mine. The new concentrator is scheduled to come on line six to seven years after the resumption of operations at the Olympias mine.

The mill will be rated to process 850,000 tpa of ore. The ore will be primary crushed on surface before being conveyed to the plant. The concentrator will be of conventional design and will comprise the following unit operations:

- Ore will be transferred from the mine by truck via the 8.5 kilometre Stratoni Decline to the brownfield Stratoni mine site. Primary crushing will be carried out at the new plant area. The ore will be stored on a crushed ore stockpile from where an ore reclaim system and SAG mill feed conveyor will feed the SAG mill;
- A single SAG mill running in combination with two ball mills. A pebble crushing facility is provided for breaking down SAG mill discharge oversize material. The SAG and ball mills discharges are classified in a cluster of hydro-cyclones with the overflow proceeding to the flotation stage and the undersize making up ball mill feed;
- The flotation section is operated in the differential mode. The lead/silver concentrate is floated first, the zinc concentrate second and the refractory gold bearing pyrite concentrate third. The separation of the feed into the three concentrates is achieved with a combination of pH control and reagent addition. The respective rougher concentrates are upgraded to the final product grade by cleaning stages. Provision will be made for the storage, mixing and distribution of milk of lime and reagents;
- The three concentrates will be thickened and filtered. In the case of the lead/silver and zinc concentrates, these will be transferred to the storage and loading facility at the port in Stratoni. The gold bearing pyrite concentrate will be sold (or transferred to the gold plant storage shed ahead of the drying plant at the flash smelting furnace complex);
- The design of the process plant will incorporate features to provide for worker health and safety.

17.6. PLANT INFRASTRUCTURE

It is the intention of EGL / Hellas Gold to utilise as much of the existing infrastructure as possible. Where required, existing buildings will be upgraded. Facilities that are identified as surplus to the Stratoni operations are to be assessed to determine their suitability for the new plant and any upgrades required to render them suitable.

The new concentrator will be housed in a steel frame building. Maintenance to the equipment within the building will be carried out with lifting by Electric Overhead Travelling Cranes. Plant control will be managed through a computer based distributed control system located in a central control room. Local controls will be installed where required to ensure efficient and safe operations.

The plant water balance will be refined during basic and detailed engineering. There is currently excess water from the Stratoni operations at Mavres Petres and Madem Lakkos mines and local catchment ponds. Wherever possible, water will be recycled within the concentrator. The overall water balance will include the potential needs of the gold plant complex. Should the full metallurgical complex be constructed there will be a requirement for water from the Olympias mine which has been allowed for in the mine planning.

There is a power supply from the Greek grid system to the main substations at Olympias and Stratoni.

The plant will include the normal services providing electrical power, process water distribution, fire control, compressed air and the like.

17.6.1. TAILINGS

The tailings from the concentrator will be directed to hydro-cyclones; the coarse fraction will be directed to the surface backfill plant or to the new backfill plant underground at Olympias on the -210 m level. There it will be mixed with cement for placement underground to fill the mined out stopes. When all the mining activities are carried out below the -250 m level, then only the backfill plant on the -210 m level will be used. The fine fraction will be directed to the TMF. It is planned to transport the ore to the new concentrator along the connecting tunnel by truck, the course tailings will then be back hauled to the backfill plants at the Olympias mine.

During periods of excess tailings, when backfill is not required or when the backfill plant is down, all the concentrator tailings will be directed to the relevant part of the new TMF at Kokkinolakkas.

17.6.2. RECOVERIES

The recovery of the lead, silver, zinc and gold to their respective concentrates will be in the range +/- 90% based on previous operating history at Olympias. It is anticipated that with modern equipment and automated process control, the historical recoveries will be exceeded.

Table 17-2 shows the expected typical flotation recoveries and grades for the three concentrates.

Table 17-2 Olympias (Stratoni Concentrator) Run of Mine Flotation Recoveries

Lead Concentrate				Zinc Concentrate		Pyrite/Arsenopyrite Gold Concentrate			
Recovery		Grade		Recovery	Grade	Recovery	Grade		
Pb%	Ag%	Pb%	Ag g/t	Zn %	Zn %	Au %	Au g/t	As %	S %
91	+/-83	63	+/-1800	+/-91	51	+/-85	22	9	40

The lead concentrate may incur minor intermittent penalties for antimony, arsenic and bismuth, and the zinc for iron and arsenic.

17.6.3. TAILINGS TRANSPORT AND IMPOUNDMENT

Tailings disposal and storage is an important part of the Olympias Project. Tailings disposal methods will be aimed at minimising the land take area and water management requirements for the Olympias Project.

The necessary long-term stability tests and Toxicity Characteristic Leaching Procedure will be carried out on the various plant residues as part of the test work programme. The precise location, capacity, design and operational management of the TMF will be decided as the Olympias Project develops but initial studies show that the Upper Kokinolakkos valley is a brown field site and has the right characteristics.

To maintain the water balance, the various plant residues should be dewatered as much as possible within the plant for recycling of process water. The coarse fraction concentrator tailings will be utilised for backfill and will be pumped back to the Olympias mine site where the backfill plant will be located.

17.7. PROCESS PLANT PROJECT IMPLEMENTATION

A detailed construction schedule will be prepared for the process plant outlining the proposed construction schedule and identifying the critical path tasks, together with a detailed capital cost summary matched to the proposed construction schedule outlining the timing of the required capital cost investment. This project is relatively straightforward as it entails well established technology and engineering practice with minimal risk.

17.8. FLASH SMELTING PROCESS OPTION

17.8.1. PROJECT DESCRIPTION

Outotec OY of Finland (Outotec) were contacted to provide an engineering solution to the treatment of the Olympias gold pyrite/arsenopyrite concentrate which will be technically viable, economic and environmentally acceptable. The process was based on Outotec's well known flash smelting technology.

Outotec initially provided in July 2005 a Preliminary Information Package for Treating Pyrite/Arsenopyrite Concentrate which was subsequently advanced into a pre-feasibility study in early 2006. Following on from additional test work and discussions with Hellas Gold the process was further developed from the original concept, the main changes being;

- The co-treatment of Olympias gold bearing pyrite concentrate with copper concentrate to improve gold recovery to the matte phase.
- The replacement of the ambient arsenic stabilisation circuit by incorporating an autoclave to ensure that stable scorodite is formed for stable long term storage.
- The elimination of the Precious Plant so that the final product is a gold bearing copper concentrate derived from the Flash smelter matte.

Outotec carried out mini-pilot scale pyrometallurgical testwork and laboratory scale hydrometallurgical testwork. Reports describing the work were produced. The findings of these reports and the extensive experience of Outotec on flash smelting and metallurgical process plant installations were used by their engineers to arrive at an integrated process to extract the gold and silver in the Olympias concentrate and stabilise the arsenic to scorodite.

The main units of the treatment concept developed by Outotec are:

- Flash smelting and off-gas cooling
- Sulphuric acid plant and off-gas handling
- Matte leaching and gold concentrate production
- Quench and Iron-Arsenic precipitation

The capacity used in the Outotec calculations and estimations was 250,000 t of pyrite/arsenopyrite concentrate in a process plant scheduled to operate for 330 days per annum.

Flash smelting as applied to the treatment of arsenopyrite/pyrite concentrates is a new application of the technology and is still basically in the research and development phase. Outotec have stated that more continuous pilot-scale tests need to be undertaken. Also, due to the extremely high volumes of gas generated in the Flash Smelter, modelling of the quench tower process should be carried out to increase the level of confidence in the process design parameters. Assuming the testwork proves the process is technically viable and provides the required process design criteria, then basic engineering and accurate costing to produce a bankable feasibility study can be undertaken. This will then enable an investment decision to be made and should this be positive, detailed engineering will be completed and project implementation effected.

A schematic of the flash smelting based process is shown in Figure 17-1.

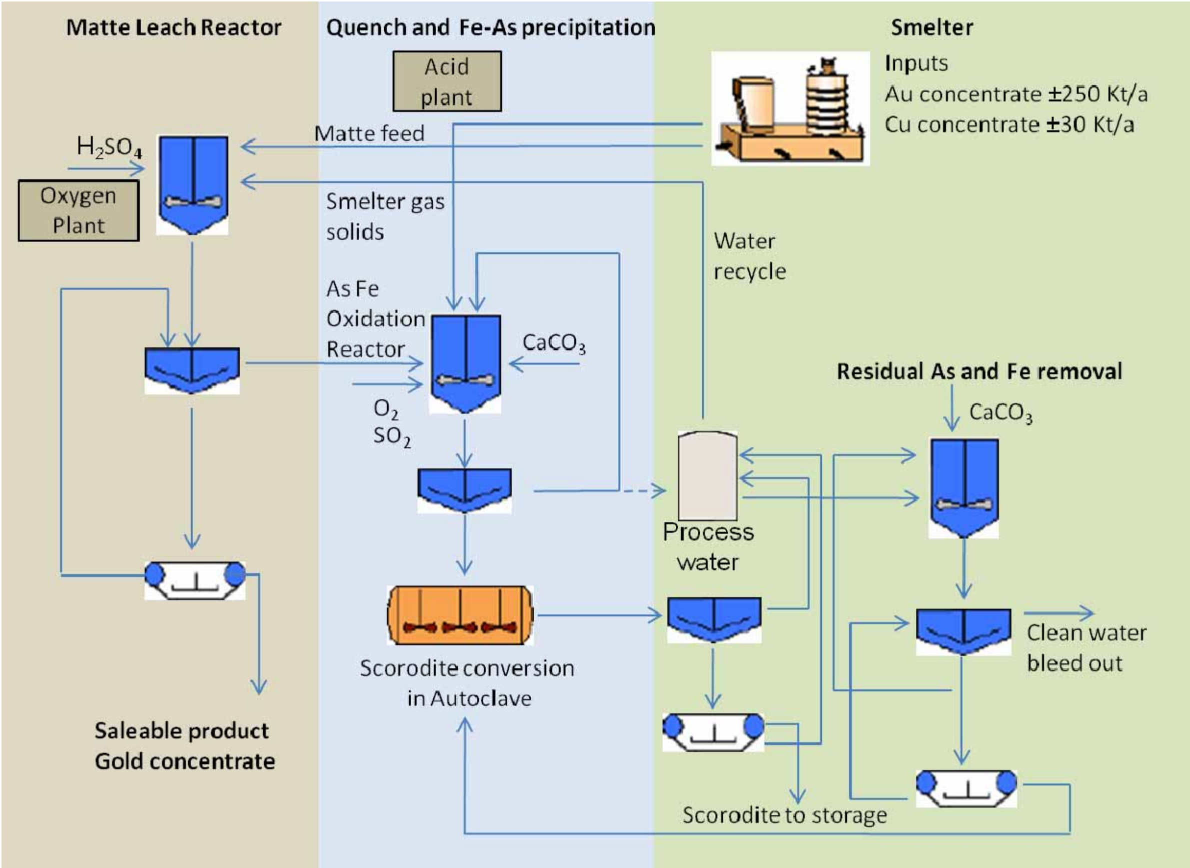


Figure 17-1 Schematic of Flash Smelting Process

The following sections describe the Outotec flash smelting concept as applied to the treatment of Olympias pyrite/arsenopyrite concentrate.

17.8.2. DESCRIPTION OF SMELTER AREA

17.8.2.1. Raw Materials Handling and Drying

Concentrate and Silica Storage – Olympias concentrate, copper concentrate and flux are transported to the smelter plant, unloaded, stored and transported to the day bins and from there the feed mixture is conveyed to the steam dryer.

Drying Operation – In the drying system the filtered concentrate, flux, dust filter cake mixture is dried in contact with the steam tubes by means of indirect steam heating.

Dried Product Handling – From the steam dryer the dried feed mixture is fed directly with a pneumatic conveying system to the dry charge bin from where the dried product is fed into the gravimetric feeding system before the flash smelting furnace.

17.8.2.2. Flash Smelting Furnace Feed System

The operation of the gravimetric feed system is based on continuous weighing of the material in the dosing bin, calculating and controlling the actual feed rate by the screw feeder rotation speed.

17.8.2.3. Flash Smelting Furnace

The flash smelting furnace consists of three main sections: vertical reaction shaft, horizontal settler and vertical uptake shaft.

The feed mixture and the oxygen enriched process air form a rapidly reacting suspension in the reaction shaft. The reactions taking place in the reaction shaft are strongly exothermic.

In the settler part of the furnace, the slag formation reactions are completed and the smelting products settle on the bottom by gravity forming matte and slag layers. Matte is heavier and settles through the slag layer to the furnace bottom.

Matte is periodically tapped through matte tapping holes and matte launders directly to granulation. The granulated matte product, which contains over 90% of the gold, is further treated to recover the gold and silver.

The testwork has shown that the recovery of gold is strongly related to the iron matte to concentrate feed ratio, the higher the ratio the higher the gold extraction to matte. However, the more matte that is produced the greater the complexity and size of the equipment required for the down stream process steps of matte leaching and arsenic stabilisation. The smelter operation has been improved by the co-feeding of copper concentrates to obtain the optimum balance between gold recovery and matte volume. Outotec have specified a gold pyrite:copper concentrate feed ratio of +/- 8.3:1, equating to some 30,000 tonne per year, to achieve a gold extraction to the matte phase of +/- 94%.

The flash smelting furnace slag is tapped directly through slag tapping holes and slag launders to ladles and cast to solid blocks. Slag granulation is also an option though not costed. The slag will either be stored as blocks on a discrete repository or, if granulated, be disposed of with the plant tailings on the tailings management facility. The tailings management facility capital and operating costs have provision for the storage of the slag. As the slag is low in arsenic (approximately 0.1%) and sulphur (2.5%) and these elements will be locked in a glassy matrix, it may be suitable for use as construction material.

17.8.2.4. Gas Cooling and Washing in Quench Tower

The flash smelting furnace off-gas exits through the uptake shaft and is cooled in a quench tower. Approximately 99% of the incoming arsenic is contained in this gas flow.

The off-gas cooling operation entails spraying water into the gas to be cooled. The heat of the off-gas is consumed by evaporating the water and the gas is cooled very rapidly thereby stopping the reactions of gas and dust. Such a large amount of water is used for cooling that the majority of water remains as liquid, which pre-washes the off-gas, binds the arsenic containing dust and flushes the walls of the quench tower.

In the gas cooling and cleaning process, the water becomes acidic and a part of the dust will dissolve into the acidic (pH approx. 1 to 2) wash water. The solids have to be separated from the quench tower circulation and also the content of the dissolved arsenic in the liquid circulation has to be controlled in order to avoid precipitation. Thus a part of the clarifier overflow has to be continuously bled out of the system. The off-gas from the quench tower flows to further cleaning in the gas cleaning section of the sulphuric acid plant.

An area that needs further investigation is how to ensure the large volumes of off-gas due to the high evaporation of arsenic can be effectively handled by the system. Outotec recommended that they carry out simulation modelling to verify the process design.

17.8.2.5. Flash Smelting Furnace Slag Granulation Systems

The matte from the flash smelting furnace, and possibly also the slag, are granulated directly from granulation launders by using a conventional water spray nozzle granulation system.

17.8.2.6. Smelter Fugitive and Ventilation Gas Handling

Fugitive and ventilation gases in the smelter area are collected into the ventilation gas systems from the flash smelting furnace tapping holes and launders. Flash smelters are highly efficient at gas capture and regularly exceed 99.9% in operating plants which is an important consideration when processing Olympias gold concentrate which has a high arsenic content.

17.8.3. IRON MATTE MILLING AND LEACHING AREA

The granulated copper/iron matte is transported from the matte storage to the grinding stage. The matte is wet ground in a ball mill. The ground matte is pumped to a hydro-cyclone where the coarse material is separated and fed back to the wet grinding mill.

The finer material from the cyclone is led to the leaching stage. The ground matte is leached with sulphuric acid in an agitated reactor at ambient pressure, a temperature of 90°C and pH of approximately 1.5 to leach out some of the iron.

The solid phase is directed to solid/liquid separation. The solid underflow is then filtered and the gold containing copper filtrate is the concentrate product that is sold. The iron containing liquid phase is directed to the smelter off-gas quench and iron/arsenic treatment section of the plant.

The expected composition of the concentrate product will be about 20% copper and 175 g/t gold.

Outotec have recommended that more testwork is carried out to establish means of reducing the amount of matte leach residue thereby increasing its gold content.

17.8.4. QUENCH AND FE-AS PRECIPITATION AND EFFLUENT TREATMENT PLANT

17.8.4.1. Arsenic Removal

Arsenic precipitation is carried out in two steps.

In the first step, Arsenic is precipitated as ferric arsenate in an agitated reactor located after the quenching vessel under controlled conditions to achieve an iron to arsenic ratio of 1.25 at a temperature of 90°C and a pH of 1.8. Oxygen gas is added to the reactor to enable oxidation of the iron to Fe^{3+} and the Arsenic to As^{5+} and controlled additions of oxidising SO_2 gas and milk of lime for pH control and neutralisation are also made.

The oxidised product flows to solid/liquid separation where the clear thickener overflow passes back to the Quench tank and the solids are directed to the second stage and fed to an autoclave. Pressure oxidation by means of an autoclave is the only established method which has been proven over many years in industry where crystalline scorodite, ($FeAsO_4$*$2H_2O$) is formed. This is the chemical species that binds the arsenic in a form that is stable for long term storage and which would conform to the EU Mine Waste Directive.

The temperature in the autoclave will be 160°C at a relatively modest pressure and under acidic pH conditions.

The product from the autoclave is cooled and, after solid/liquid separation, the solids are filtered and the scorodite containing solids directed to residue storage.

17.8.4.2. Residual As and Fe Removal

Most of the overflow from the ferric arsenate thickener ahead of the autoclave is recycled as quench water. Any excess and overflow from the scorodite thickener after the autoclave, and filtrate from the scorodite filter, are collected in a tank. A fraction is recycled to the matte leach vessel but most flows to the second arsenic and iron removal section to precipitate the rest of arsenic as amorphous ferric arsenate ($FeAsO_4$). This is carried out in another stirred reactor at ambient pressure, a pH of 4 and the Fe-As ratio maintained as near as possible to 4.

The reactor solids containing the ferric arsenate are sent to solid/liquid separation and the thickener underflow is then filtered. The filtrate is returned to the thickener and the solids directed to the autoclave for conversion to crystalline scorodite as described earlier.

Any extra iron not used in the arsenic reaction is precipitated as goethite/jarosite.

Final neutralization in this section of the process prevents accumulation of metallic impurities. The requirement for fresh water is small because process water leaves the circuit only with filter cake. Final neutralization by means of the thickener overflow bleed also purifies the water discharged to below the impurity levels of environmental requirements.

All the testwork has been carried out on a bench scale and Outotec require that more testwork is carried out in a continuous pilot plant scale to prove up the proposed process design and obtain robust performance data.

17.8.5. SULPHURIC ACID PLANT

The sulphuric acid process consists of the following four principal steps:

Gas cleaning of the sulphur dioxide (SO_2) containing process gas.

Drying of the sulphur dioxide (SO_2) containing process gas.

Conversion of the sulphur dioxide (SO_2) containing process gas to sulphur trioxide (SO_3) gas proceeds according to the chemical reaction: $SO_2 + 1/2\ O_2 <=> SO_3$.

Absorption of the sulphur trioxide (SO_3) gas by combining with water (H_2O) to form a solution of 98.5% sulphuric acid (H_2SO_4) according to the chemical reaction: $SO_3 + H_2O => H_2SO_4$

In this design, the basic configuration of the sulphuric acid plant is the 3+1 double absorption process.

Process gas from the flash smelting furnace is first cooled down and initially cleaned in the quench tower and then led to further cleaning in the gas cleaning section of the sulphuric acid plant.

As has been mentioned previously, one area of concern is the large volumes of gas arising from the smelter due to the vaporisation of the sulphur and arsenic in the concentrate feed. Outotec have proposed that computer modelling is carried out using their in-house developed expert software to increase confidence in the process design and size of the cooling/quench tower.

17.8.5.1. Gas Cleaning Section

The process gas coming from the quench tower has high dust and fume loading. It is further cleaned in a gas washing tower, two scrubbers and in the primary and secondary wet electrostatic precipitators before entering the contact section.

In the quench tower installed upstream, large amounts of water evaporates due to the adiabatic cooling operation. To match the water balance of the downstream sulphuric acid plant, it is necessary to condense the main part of the water vapour from the process gas. Gas cooling and condensing of water vapour takes place in a packed gas cooling tower.

Condensate forms in the downstream gas cleaning equipment (gas cooling tower and wet electrostatic precipitators) and the make-up water that will be added to the system to compensate the required bleed-off flows counter-currently to the gas flow. This dilutes the circulating liquid. Dilution helps to minimize problems which might arise from the precipitation of solids (formation of scaling and build-up).

17.8.5.2. Contact Section

The composition of the cleaned process gas has to be adjusted when entering the contact section to comprise an SO_2 maximum content of 12.0% and a minimum O_2:SO_2 ratio of 1.0 with dilution air. Dilution air is brought into the process from the inlet of the drying tower.

Substantially all of the water vapour is removed from the process gas in the drying tower where the gas flows counter-currently to concentrated sulphuric acid (96%).

In order to initiate the catalytic conversion reaction, the process gas must be heated to the auto-ignition temperature before contacting the catalyst in the contact converter. This is done by recovering heat, generated by the exothermic conversion reaction.

The extent or efficiency of reaction is increased by carrying the reaction out in successive catalyst passes with partial cooling between the passes.

The basic concept of the double absorption process is to further increase the conversion reaction and to reduce tail gas SO_2 emissions from the acid plant by providing a secondary SO_2 to SO_3 conversion and absorption process.

The absorption towers are used to absorb SO_3 from the gas coming from the converter system. The inter-pass absorbing tower system is interconnected with the drying acid system to permit automatic control of drying and absorbing acid concentrations.

All the acid produced in the circulating acid system is removed as 98.5% H_2SO_4 after the final absorbing tower and is pumped through the product acid cooler to the acid storage.

The off-gas flows to the stack after the final absorption tower.

The extra heat evolved in the process is mainly transferred into cooling water.

17.8.6. CONSIDERATIONS FROM TESTWORK IN PORI

Testwork was carried out by Outotec in Pori for process development. Both the pyrite/arsenopyrite smelting process and the hydrometallurgical treatment of iron matte and arsenic precipitation were tested. In the hydrometallurgical tests, raw materials generated from the pyrite/arsenopyrite smelting tests were utilized.

The targets of the smelting test campaign were to verify the technical feasibility of flash smelting for processing pyrite/arsenopyrite concentrate to matte and slag and to examine the distribution of precious metals and arsenic between slag, matte, dust and gas.

The separation of matte and slag was not as complete as in the case of copper flash smelting. This was the main reason for developing the smelting flow sheet by co-feeding copper concentrate with the pyrite/arsenopyrite concentrate.

The matte leaching process should work effectively although further investigations need to be carried out. The formation of scorodite in an autoclave is industry standard best practice for long term stable storage of arsenic. Laboratory test work has been carried out by both Outotec and the National Technical University of Athens (NTUA) on Olympias pyrite/arsenopyrite concentrate and this work indicates that this process step is technically proven.

In general, it must be emphasized that all the matte leaching and arsenic precipitation tests were batch tests. In order to obtain more reliable data for establishing plant process design criteria, continuous hydrometallurgical test runs with necessary recycles must be carried out on a pilot scale.

It is also recommended that further smelting tests be carried out to optimise the proportion of copper to Olympias pyrite/arsenopyrite concentrate so that maximum gold can be recovered to the matte phase while the tonnage of matte produced is minimised.

17.8.7. FOCUS FOR FUTURE WORK

The wet gas cooling of the flash smelt furnace off-gas is larger in scale than other industrial plants known to Outotec. The use of wet gas cooling has been applied at commercial scale but for smaller gas flows than in this case. Also the dust and especially the fume loading of the flash smelting furnace off-gas are very high. A detailed modelling of the quench tower is recommended to ensure proper dust wetting and gas cleaning and to minimize build-ups.

Gold, silver and copper recoveries in the matte need to be verified. The sulphur content of the matte also needs to be optimised. Although difficult to test on a pilot scale the possible generation within the furnace of gold absorbing speiss needs to be tested even if only by means of a suitable computer simulation programme.

The potential of the copper matte acting as a sink for the arsenic also needs to be tested as this could have implications on the design of the arsenic stabilisation section, particularly the autoclave.

The composition of the matte leaching residue, especially its elemental sulphur content, is not clear. The composition used in the process calculations is based on the probable reactions taking place in leaching to a certain extent, so that mass balances are matched. In order to a get clearer picture of the leach residue, bench pilot test runs are recommended.

The stability of the arsenic removal solids from the autoclave, scorodite and associated compounds, needs to be tested. Bench pilot test runs with iron solution from the matte leaching process are required, to produce as authentic precipitates as possible from the arsenic containing quench solution.

The environmental acceptability of the flash smelting furnace slag has to be tested as well. The effect of slag composition (chemical and physical) on the leaching of harmful elements needs to be established even though it should be inert.

17.8.8. CONCLUSIONS ON FLASH SMELTING

Based on the testwork, it can be stated that the chemistry of the proposed process does work and is in accordance with EGL's submitted EIS. However, it must be emphasized that all the copper/iron matte leaching and arsenic precipitation tests were batch tests. In order to obtain more accurate results for plant design, continuous hydrometallurgical test runs with necessary recycles in a bench pilot scale along with additional pyrometallurgical tests will be carried out.

The calculated metallurgical recoveries are the following:

- Gold Recovery 94%
- Silver recovery 87.0%
- Copper Recovery 94%

Once the process design criteria have been determined from the confirmatory testwork programme then a feasibility study and basic engineering will be undertaken to establish more accurate capital and operating costs.

It should be noted that the financial analysis included in this report is made on the basis of sale of gold concentrates using a conservative return of 45% net of transport and processing costs plus the sale of the base metal concentrate streams.

EGL has submitted an EIS which includes a gold plant using the flash smelting route to process the gold bearing pyrite / arsenopyrite concentrates once full ramp up is achieved. It is the intention of the company to investigate the viability of this process route with future testwork and engineering studies. The implementation of a gold plant could be brought forward by stockpiling of gold concentrate or if additional ore streams are produced from deposits currently being explored in the area. The current level of testwork and engineering of flash smelting for this application does not provide capital and operating costs within a sufficiently accurate range to allow inclusion in this evaluation but it is noted that testwork to date has indicated recoveries of more than 90% gold. It is also noted that off-takers for the Olympias gold bearing pyrite / arsenopyrite concentrate in the past included smelters and a recent trial on Olympias gold concentrate by a potential off-taker using copper smelting technology also showed excellent recovery, reflected in terms of 97% plus payability.

18. PROJECT INFRASTRUCTURE

18.1. SURFACE RECEIVING DAM AND WATER TREATMENT PLANT

A small concrete receiving dam at the +80 m level on surface receives all mine water. At present, the water is clear. An open pump station containing two DP pumps transfers the water via a 200 mm surface pipe to the water treatment plant adjacent to the mill. The water treatment plant is of the same design as that operating at Stratoni and appears to be in good condition although not required to operate at present. Water is then transferred via three thickeners (at present unused) to the tailings dam.

18.2. TAILINGS MANAGEMENT

Initially all tailings will be filtered at Olympias and the coarse sold as aggregate. The fine tailings filter cake will be transported to Stratoni and disposed in either the existing TMF or the new Kokinolakkos TMF. The fine tailings filter cake produced by the new Stratoni concentrator will also be disposed of in the Kokinolakkos TMF.

The favoured site for the TMF is by constructing an embankment across the base of the Madem Lakkos valley and lining the upstream side to EU standards. The potential site is shown in light blue in Figure 18-1, down slope of the proposed concentrator and metallurgical plant area. The site has a potential storage capacity well in excess of 6 Mm^3 of tailings. Dry storage reduces the volume requirement and the risk of spills. The proposed TMF site is a brown field site. The TMF would also provide emergency catchment downstream of the Stratoni mine.

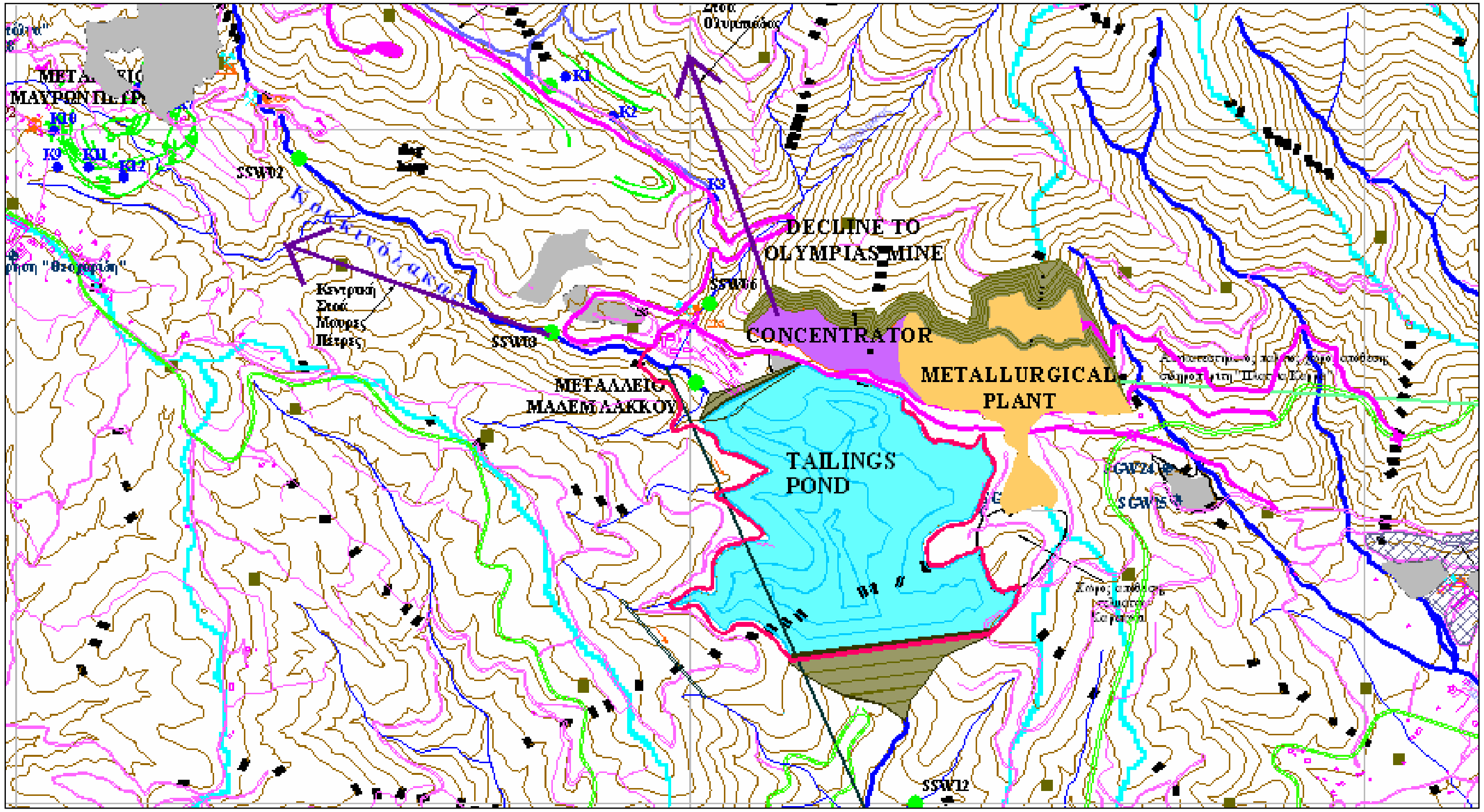


Figure 18-1 Conceptual Layout of Stratoni TMF for Olympias Tailings

19. MARKET STUDIES AND CONTRACTS

Hellas Gold has sold gold concentrates from historic production at Olympias through long term contracts to Sino Gold MRI Trading, Celtic Resources, Euromin, Yantai Non Ferrous Metals and Trafigura for processing in Central Asia and China during the 4 years to 2009, thus proving there is a market for such concentrates.

Based on these historic terms and recent negotiations with off-takers EGL expects to receive the following terms:

Table 19-1 Gold Concentrate Indicative Terms Freight on Board Greece

Payable	90%	
T/C US $:	$162	Per dry metric tonne of concentrate
R/C US $:	$6	per payable gold ounce
Penalties	$1.5	per 0.1% above 0.5% As in conc

Based on these numbers, 45% of the contained gold value net of all shipping and processing costs has been used to calculate revenues. This figure of 45% can be regarded as a minimum in the opinion of the authors.

Hellas Gold has off-take agreements for lead and zinc concentrates from its Stratoni operation to Trafigura and Euromin who trade and or represent European smelting companies. The terms of the contracts for Stratoni were used for the evaluation of Olympias.

The terms used can be summarised as follows:

Table 19-2 Zinc concentrate terms

Base Treatment Charge	USD/t	135
Maximum Zinc Payable	%	84.00%
Minimum Conc Grade Deduction	%	8.00%
TC Price Basis	USD/t	1,750
Escalator 1	USD/t	0.12
TC Escalator 1		2,000
Escalator 2	USD/t	0.15
TC Escalator 2		2,000
De-escalator	USD/t	0.05
TC De-escalator		1,750
Silver Payable	%	70.00%
Minimum Silver Deductible	g/t	93.31
Penalties		
Fe Threshold	%	9.00%
Fe Fee per 1.0%	USD	1.50
Arsenic Penalty		

As Threshold 1	%	0.90%
Fee per 0.10 %	USD	1.50

Table 19-3 Lead Concentrate terms

Base Treatment Charge	USD/t	103.00
Maximum Lead Payable	%	95.00%
Minimum Conc Grade Deduction	%	3.00%
TC Price Basis	USD/t	1,800
Escalator 1	USD/t	0.12
TC Escalator 1		2,300
Escalator 2	USD/t	0.14
TC Escalator 2		2,300
De-escalator	USD/t	0.05
TC De-escalator		1,800
Silver Payable	%	95.00%
Minimum Silver Deductible	g/t	50
Gold Payable	%	95.00%
Minimum Gold deductible	g/t	1.00
Arsenic Penalty		
As Threshold	%	0.80%
Fee per 0.10 %	USD	1.50
Antimony Penalty		
Sb Threshold	%	0.80%
Fee per 0.10 %	USD	1.50

This reports anticipates owners teams will supervise the mine development and the refurbishment of the existing plant at Olympias and that mining and processing will also be owner operated. However, contract mining and mine development are not precluded for the future. Engineering of the underground mine infrastructure will be carried out by an independent engineering firm. The engineering and construction of the new concentrator and flash smelter are likely to be an Engineering, Procurement, Construction and Management style contract (EPCM).

20. ENVIRONMENTAL STUDIES, PERMITTING AND SOCIAL OR COMMUNITY IMPACTS

EGL's 95% owned subsidiary has submitted an EIS which has recently been approved. The following assessments have been made on the Olympias Project's environmental impact.

20.1. LANDSCAPE

Accumulating impact is anticipated only in the Madem Lakkos brown field area where the new Olympias concentrator and tailings disposal facility will be constructed. The remainder of the infrastructure components are distant from each other and therefore there will not be any significant accumulating impact on the morphology of the area under study. Impact is of low significance, of local character and much will be non-permanent and partially reversible. All measures to minimise the anticipated impact will be taken.

The Olympias Project will benefit the Olympias area by allowing the rehabilitation of the Olympias valley after approximately eight years of operation.

20.2. GEOLOGICAL ENVIRONMENT

The ascending drift and fill mining method has been selected for the Olympias Project. The mined areas will be backfilled with material comprising of inert tailings and cement. This prevents surface subsidence and ameliorates underground water quality due to the alkalinity of the backfill.

20.3. GROUND – LAND USE

The impact will be localised to the areas of the disposal facilities but with careful replanting at closure will be minimised. Rehabilitation will commence on the Olympias Valley disposal facilities after approximately 4 years and on the process plant after approximately 9 years. No significant impact is anticipated on the rest of the Olympias Project's areas. After the completion of the operations, the Olympias Project's areas will be rehabilitated according to appropriate and approved land uses.

20.4. WATER RESOURCES

No significant impact is expected either quantitatively or in quality on the water in the immediate mining and processing areas or those areas within the immediate regional water system. The Olympias Project has been designed such that any leakage can be managed and controlled. The overall impacts are actually assessed as moderately positive due to the rehabilitation of the old tailings ponds and permanent restoration of the valley site when the main processing operations move to Stratoni once full ramp up to 850kt is achieved.

20.5. ATMOSPHERIC ENVIRONMENT

Mining activities (mines, surface plants, disposal areas, etc) will not cause any significant impact on the atmospheric environment, since all the necessary precautions will be taken for the minimisation of the anticipated impact which are extensively described in the EIS and therefore all possible impact can be considered as temporary and reversible.

Accumulative impact on the atmospheric environment is anticipated only in the Madem Lakkos area where the proposed waste disposal facility will be situated and the process mill and metallurgy plant will be nearby. The rest of the plants are rather distant from each other and therefore there will not be any significant accumulating impact on the atmospheric environment of the under study area.

As a conclusion it could be said that the Olympias Project's impact on the atmospheric quality of the area will be limited in the direct area of influence and will be mainly related to the local and restricted increase of the dust and gas values. There will be no impact at all on the quality of the atmospheric environment of the nearby populated areas.

20.6. SOUND ENVIRONMENT

According to the operation standards of the new facilities (type of machinery, real operation time, time schedules, noise levels), aggravation of the sound environment is not anticipated in the direct and broader area under study, in all the stages of development of the Olympias Project and under the worst possible conditions including simultaneous presence of surface and linear noise sources.

Accumulative impact on the sound environment is anticipated only in the Madem Lakkos area where the proposed waste disposal facility will be situated and the process mill and metallurgy plant will be nearby. The rest of the plants are rather distant from each other and therefore there won't be any significant accumulating impact on the sound environment of the under study area.

20.7. ECOSYSTEMS – FLORA – FAUNA

All the areas used are outside of but adjoin Natura 2000 (an EU designated nature reserve) however this places no restrictions on activities of EGL providing the terms of the EIS are adhered to.

According to the above, the impact on the ecosystems of the study area is anticipated to be slightly negative but of a local character.

20.8. SOCIAL & FINANCIAL ENVIRONMENT

The positive consequences of the Olympias Project are very important for the Chalkidiki Prefecture and for the National Economy. The general financial and social consequences deriving from the Olympias Project are the following:

- EGL becomes the largest European producer of primary gold and a proponent of modern mining technology and development.
- A significant contribution is made to the National Economy.
- Significant infrastructure is constructed and equipped by local companies.
- Service industries in the local economy expand.
- New jobs are progressively created.

20.9. HISTORICAL – CULTURAL ENVIRONMENT

The area within which the Olympias Project develops does not include any recognised archaeological sites.

20.10. CLOSURE PLAN

General principles of closure and rehabilitation:

- Minimise the negative consequences of closure.
- Maximise the positive benefits of closure.
- Minimise the likelihood that closure goals are not met.
- Maximise the likelihood that opportunities for lasting benefits are captured.
- Integrating closure into the planning, engineering, construction and operational phases.
- Rehabilitation and stabilization of impacted areas as soon as possible.
- Looking out for possibilities to reuse/recycle resources during operation and closure.

Making sure that rehabilitation is in line with goals for safety, health and environment.Surface facilities at the Olympias site will be decommissioned once the final production ramp up is achieved and the stockpile of existing tailings is exhausted. The remaining facilities will be closed and rehabilitated at the end of the mine life.

Voids created from the extraction process will be hydraulically filled with a mixture of tailings and cement. When exploitation of the Mineral Reserves is over, the only pending arrangements for full closure are the removal of mining (mobile mining equipment, fans, etc.) and mechanical (industrial water network, electrical installations, etc.) equipment from the access works, backfilling access works where appropriate and the rehabilitation of the area around the entrances of the main access tunnels.

20.11. ENVIRONMENTAL COSTS AND GUARANTEES

EGL will ensure full compliance with EU legislation embodied in the Mine Waste Directive 2006/21/EC, in particular Article 14, which requires "a financial guarantee or equivalent so that all obligations under the issued permit are discharged, and there are funds readily available at any given time for the rehabilitation of the land affected by the waste facility."

EGL's support will in the first instance take the form of a full and unconditional corporate guarantee of Hellas Gold's reclamation and closure costs and liabilities from EGL.

Further, EGL's corporate guarantee will be fully supported by a surety bond provided by an internationally recognised, AAA-rated insurance company. A surety bond is a guarantee by the insurer to fund the reclamation and closure liabilities of Hellas Gold's mining operations if EGL is unable to fund these obligations. The Greek State would be a named party to the surety bond and this guarantee will be in the amount of €20.8 million to cover the Olympias projects. This is comprised of

- €3,400,000 for the rehabilitation of facilities at the Olympias site
- €8,000,000 for retrenchment of personnel
- €9,400,000 for the rehabilitation of

Environmental monitoring is included in the operating costs based on costs incurred at EGL nearby operations factored to reflect the scale of the Olympias project.

21. CAPITAL AND OPERATING COSTS

The following tables describe the capital and operating costs for the Olympias project.

Capital costs for the mill refurbishment at Olympias and mining equipment are based on current quotes. Capital mine development rates have been estimated by Hellas Gold based on first principals using labour rates, equipment, reagent and power costs from current Hellas Gold operations adjusted for the proposed operation and shift patterns. Capital costs for the proposed new concentrator at Stratoni are based on current databases for mine infrastructure.

Operating costs have been estimated by Hellas Gold based on first principals using labour rates, equipment, reagent and power costs from current Hellas Gold operations and quotes.

The cost estimates have been verified by the authors of this Technical Report, including benchmarking against the Company's and other current European operations and are viewed as reasonable and current.

Table 21-1 Capital Costs

		Total	Initial	Ramp Up	Replacement
Mine					
Mine Equipment / infrastructure	(€)	80,593,674	42,120,829	11,699,191	26,773,654
Mine Development	(€)	113,064,102	33,924,985	40,991,171	38,147,947
Total Mine	(€)	193,657,777	76,045,814	52,690,362	64,921,601
Plant					
Rehab Old Olympias Plant	(€)	11,650,000	11,000,000		650,000
New Plant at Stratoni	(€)	42,682,557	0	38,495,606	4,186,951
TMF	(€)	17,200,000	11,200,000	2,800,000	3,200,000
Total Plant	(€)	71,532,557	22,200,000	41,295,606	8,036,951
Environment					
Rehabilitate old areas (remaining in closure bond)	(€)	11,400,000	3,000,000	2,000,000	6,400,000
Stratoni Plant and TMF Closure	(€)	9,400,000	3,000,000	0	6,400,000
Total Environment	(€)	20,800,000	6,000,000	2,000,000	12,800,000
TOTAL	(€)	285,990,334	104,245,814	95,985,968	85,758,552

Table 21-2 Operating Costs

Mining	**Period / Note**	**Units**	**Rate**
Mining Cost Refurbishment		EUR/t ROM	31.11
Mining Cost Expansion		EUR/t ROM	26.12
Stratoni Decline Trucking		EUR/t ROM	5.00
Olympias Adit Trucking		EUR/t ROM	3.50
Geho operating cost		EUR/t ROM	0.13
Senior Management & Tech Services Operations		EUR/t ROM	3.80
Backfill Cement		EUR/t ROM	1.86
Electricity Fixed during Refurbishment	To Q4 2015	EUR/year	300,000
Electricity Expansion		EUR/t ROM	2.30
Water pumping (electricity and spares)	Tailings	EUR/yr	250,000
Water pumping (electricity and spares)	400ktpa	EUR/yr	500,000
Water pumping (electricity and spares)	850ktpa	EUR/yr	850,000
Technical Services	(Until 2016)	EUR/yr	8.00%
Processing			
Concentrator Cost			
Mill charge 400ktpa		EUR/t ROM	14.00
Mill charge 850ktpa		EUR/t ROM	10.55
Filter press		EUR/t ROM	0.52

Gold Plant Processing Cost		EUR/t	
On expansion	(AsPy+As Conc)	EUR/t	64.11
Tailings Reclaim			
Reclamation by dragline	(Tailing ROM)	EUR/t	2.00
Flotation cost (no milling)	(Tailing ROM)	EUR/t	8.24
Filter press	(Tailing ROM)	EUR/t	0.45
Truck coarse and fines to Stratoni and compact	(Tailing ROM)	EUR/t	0.65
Total			
Pyrite transport cost to smelter	(Tailing Conc)	USD/dmt	60.00
Environmental			
	Refurbishment	EUR/yr	200,000
	Expansion	EUR/yr	474,000

It should be noted that because fixed costs remain constant, irrespective of throughput, there is an economy of scale effect on mining costs therefore different rates are applied for above and below 450ktpa production levels.

22. FINANCIAL ANALYSIS

The following tables describe the economic parameters used for the evaluation of mineral reserves at the Olympias deposit.

It should be noted that the financial analysis included in this report is made on the basis of sale of gold concentrates using a conservative return of 45% net of transport and processing costs plus the sale of the base metal concentrate streams. It is the intention of EGL to develop and implement the flash smelting route, as described in this report and in accordance with the EIS submitted by EGL, and recently approved by the Greek government in order to process the gold concentrates once full ramp-up is achieved in year 9. This could be brought forward by stockpiling gold concentrate or if additional streams are produced from deposits currently being explored in the area. The current level of testwork and engineering of flash smelting for this application does not provide capital and operating costs within a sufficiently accurate range to allow inclusion in this evaluation but it is noted that testwork to date has indicated recoveries of more than 90% gold. It is also noted that off-takers in the past include smelters and a recent trial on Olympias gold concentrate by a potential off-taker using copper smelting technology also showed excellent recovery, reflected in terms of 97% plus playability.

Table 22-1 Metal Prices

Gold Price ($/oz)	($)	$1,000
Silver Price ($/oz)	($)	$15.00
Lead Price ($/t)	($)	$1,500
Zinc Price ($/t)	($)	$1,500

The following table summarises the key dollar capital assumptions and cash costs for the project:

Table 22-2 Key Parameters of Cash Flow

	Units	Life of Mine	Average
Olympias			
ROM production	kt	**13,573**	**543**
ROM production Au grade	g/t	**8.70**	**8.70**
ROM production Ag grade	g/t	**132.35**	**132.35**
ROM production Pb grade	%	**4.42**	**4.42**
ROM production Zn grade	%	**5.89**	**5.89**
Au Contained in Concentrate	k oz	**3,629**	**145**
Ag Contained in Concentrate	k oz	**53,313**	**2,133**
Pb Contained in Concentrate	kt	**542**	**22**
Zn Contained in Concentrate	kt	**727**	**29**
Operating Costs	USD m	**1,005.3**	**40.2**
Capital Costs	USD m	**388.8**	**15.6**
Net Revenue (1)	USD m	**3,614.2**	**144.6**
Undiscounted Operating Income	USD m	**2,608.9**	**104.4**
Discounted cash flow @5%	USD m	**1,040.4**	**41.6**

No off take agreements have been signed by or EGL / Hellas Gold and potential concentrate off takers at the time of preparation of this report.

The cash flow model gives a post tax internal rate of return of greater than 30% and therefore meets the company's criteria for a viable Olympias Project. Payback is achieved in year 6 of the operation but is a flawed measure of the returns on the project due to the phased development of the project. Returns are expected to be considerably improved with the implementation of gold processing, currently scheduled in year 9 but which could be brought forward if gold concentrate is stockpiled or alternative streams are produced as a result of exploration in the area which is currently underway.

Taxes and Royalties

Under the terms of the existing mining licences, royalty is not payable for Olympias and taxes in Greece are currently 25%, reducing to 20% by 2014. Depreciation in Greece is applicable at the rate of 15% per annum.

Sensitivity Analysis

A sensitivity analysis was carried out to model potential fluctuations of key input parameters from the base case cash flow model.

The following parameters were evaluated over a range of a 10% increase to a 10% reduction to observe the impact on the Project's NPV:

- Commodity prices;
- Grade of payable commodities
- Capital expenditure;
- Operating expenditure;

- Processing plant recoveries evaluated over a range of a 4% increase to a 4% decrease;

The Project economics are most sensitive to gold grade, and operating cost. Processing Plant recoveries do not significantly affect economics due to fluctuations within the ranges evaluated

23. ADJACENT PROPERTIES

Not Applicable

24. OTHER RELEVANT DATA AND INFORMATION

Not Applicable

25. INTERPRETATION AND CONCLUSIONS

With the estimates of mineral resources and reserves of the Olympias deposit detailed in this report, the author concludes that there are sufficient mineral reserves currently defined at the Olympias operation in order to sustain an approximate 25 year mine life and as such has met its objectives.

Mine life could be extended by in-fill drilling of the inferred mineral resources. Furthermore the planned decline from the Olympias orebody to the Stratoni mine site passes through a corridor of ground which is highly prospective as indicated by the abundance of marbles, suitable structure to have acted as mineralising fluid conduits and historic drill holes which, though they were not assayed, did encounter massive sulphides.

The mineral resources are based on an extensive programme of diamond drilling. The programme of QAQC was well run and confirmed that there were no significant biases in the data. Drill spacing is sufficient to allow a high level of confidence in the geological interpretation. The resource block interpolation has been the subject of several audits and has been found to be robust and the kriging profiles correct. The mineral resource and reserve estimate can be viewed as current and meets CIM and JORC standards. The clean geological contact between high grade sulphide ore and waste rock ensures that the mineral resources convert well to mineral reserves with the minimum loss of material.

The mining methods proposed are similar to those employed by EGL at the nearby Stratoni operation and therefore the parameters used for both the technical and economic evaluation of mineral reserves are well known and have little risk. The reserve offers a high economic return at conservative metal prices and meets the company criteria for development.

The phased approach proposed by EGL has been endorsed by the Greek State in the approval of a preliminary environmental impact study in 2009.

Studies to date indicate that there are no environmental risks foreseen and that the Olympias Project will be a major employer in the region. The phased approach allows for the early rehabilitation of the Olympias Valley after only 8 years of the Olympias Project, after which the surface infrastructure will be concentrated at the brown field site of the Stratoni Valley.

In line with EU directives, and to ensure that they remain appropriate to the operations, EIS approvals in Greece are refreshed every five years to reflect prevailing conditions such as new mineral resources, metal prices, employment levels, etc. Accordingly, this presents an opportunity, at that time, for EGL to re-assess the extraction approach, so as to ensure that in the context of the then prevailing conditions, the best available techniques are applied for the remainder of the mine life.

25.1. RISKS

The following are factors that may affect the validity of Mineral Resources and Mineral Reserves:

Foreign Country Risk

If there were any change in the economic, legal or political framework in Greece, or other circumstances arising, which materially reduce or suspend the EGL's operations, the results of the proposed Olympias operation and financial condition will be materially negatively affected.

Technical Risks

Mineral Resource and Mineral Reserve figures presented herein are based upon estimates made by EGL personnel and independent consultants. These estimates are imprecise and depend upon geological interpretation and statistical inferences drawn from drilling and sampling analyses, which may prove to be inaccurate, and may require adjustments or downward revisions based upon further development or exploration work. There can be no assurance that these estimates will be accurate, Mineral Reserves, Mineral Resources or other mineralisation figures will be accurate, or that this mineralisation could be mined or processed profitably.

Capital and Operating Cost Risks

EGL's forecasts of costs are based on a set of assumptions current as at the date of completion of this Technical Report. The realised operating and capital costs achieved on the Olympias Project may differ substantially from the forecasts owing to factors outside the control of EGL, including currency fluctuations, supply and demand factors for the equipment and supplies, global commodity prices, transport and logistics costs and competition for human resources. Though EGL incorporates a level of contingency in its assumptions, these may not be adequate depending on market conditions.

Mineral and Commodity Prices

The Olympias Project's profitability and long-term viability depend, in some part, upon the market price of gold and copper. The market price of gold and copper is volatile and is impacted by numerous factors beyond EGL's control, including: expectations with respect to the rate of inflation, the relative strength of the U.S. dollar and certain other currencies, interest rates, global or regional political or economic conditions, supply and demand for jewellery and industrial products containing metals, costs of substitutes, changes in global or regional investment or consumption patterns, and sales by central banks and other holders, speculators and producers of gold and copper in response to any of the above factors.

EGL's long term financial performance is dependent upon the market price of gold and other metals.

Currency Fluctuations

Gold and other metals are sold throughout the world principally in U.S. dollars. Further, the capital markets in which the Company expects to have access to for financing (debt and equity), are predominantly denominated in United States dollars. The Olympias Project's capital and operating costs are incurred principally in Euros. EGL does not currently use any derivative products to manage or mitigate any foreign exchange exposure. As a result, any significant and sustained appreciation of the Euro or other currencies against the U.S. dollar may materially increase the Company's costs and reduce revenues.

Financing Risks

Development of the Olympias Project by EGL will be dependent upon its ability to obtain financing through joint ventures, equity or debt financing or other means, and although EGL has been successful in the past in obtaining financing through the sale of equity securities and agreeing terms with banks, there can be no assurance that EGL will be able to obtain adequate financing in the future or that the terms of such financing will be favourable. Failure to cover capital expenditure or obtain additional financing could result in delay or indefinite postponement of development of the Olympias Project.

26. RECOMMENDATIONS

The Olympias Project is sufficiently robust to progress to the basic engineering and implementation phase.

It is recommended that additional drilling is carried out within the inferred mineral resource and further along strike to the south and down plunge where the deposit is open in order to extend the mine life of the Olympias Project.

The new Stratoni Decline planned for the last phase which will run from Stratoni to Olympias offers a good opportunity to explore along the plunge of the deposit and drilling should be conducted together with the use of down-the-hole geophysical methods.

27. REFERENCES

Papadakis A, On the Age of Granitic Intrusion, Chalkidiki (Greece, Annales Geol Pays Hellenic Vol 23 1971 pp 297-300

Kalogeropoulos S, Kilias S, Bitzios D, Nicolaou M, Both R, Genesis of the Olympias Carbonate Hosted Pb-Zn Deposit, Eastern Chalkidiki Peninsula, Northern Greece. Economic Geology Vol 84 1989 pp 1210-1234

Kalogeropoulos S, Theodoroudis A, K/Ar and Rb/Sr of the Minerals Biotite, Muscovite and Amphibolite from Rocks of the Servo-Macedonian Massif, N Greece, Unpublished report IGME Athens Greece, 1988

Kalogeropoulos S, Kilias S, Bitzios D, Nicolaou M, Both R, Genesis of the Olympias Carbonate Hosted Pb-Zn Deposit, Eastern Chalkidiki Peninsula, Northern Greece. Economic Geology Vol 84 1989 pp 1210-1234

Kilias A, Falalakis G, Mountrakis D, Cretaceous-Tertiary Structures and Kinematics of the Serbo-Macedonian Metamorphic Rocks and Their Relation to the Exhumation of the Hellenic Hinterland (Macedonia Greece), International Journal of Earth Sciences 88 1999 pp 513-531

TVX Hellas SA Olympias Geological Resource Estimation for Feasibility Study, May 1999

Behre Dolbear. A Review of the Data and Methodology Used in a Resource Estimate, Olympias Project, Stavros, Chalkidiki, Greece. May 1999

Kvaerner Metals, Olympias Project Feasibility Study, September 1999

Himmerkus F, Reischmann T, and Kostopoulos D, Geophysical Research Abstracts Permo-Carboniferous and Upper Jurassic Basement ages in the Kerdilion Unit, eastern Serbo-Macedonian Massif, Northern Greece, Vol 8 2006 05758

An Investigation of The Recovery of Lead, Zinc, Gold & Silver from Kasandra, Greece ore samples submitted by TVX Gold Inc. Progress Report No. 3, Project L.R. 4899, Lakefield Research Limited, March 7, 1996.

A Laboratory Investigation of The Recovery of Lead, Zinc and Arsenopyrite/Pyrite from the PEC and ROM 2001-2003 samples of Olympias ore submitted by TVX Hellas S.A. Project LR5566 –Progress Report No. 5, Lakefield Research, December 21, 2000.

A Laboratory Investigation of The Recovery of Lead, Zinc and Gold from Intermediate West Samples submitted by TVX Hellas S.A. Project LR5566 –Progress Report No. 9, Lakefield Research, January 8, 2001.

A Laboratory Investigation of De-Leading of PEC Pilot Plant Arsenopyrite/Pyrite Tailings from samples submitted by TVX Hellas S.A. Project LR5566 –Progress Report No. 10, Lakefield Research, October 31, 2000.

A Laboratory and Pilot Plant Investigation of The Recovery of Lead, Zinc and Arsenopyrite/Pyrite/Gold from a Sample of Olympias ore submitted by TVX Hellas S.A. Project LR5566 –Progress Report No. 1, Lakefield Research, June 1, 2000.

A Pilot Plant Investigation of The Grinding and Washing of Pyrite Concentrates from Olympias Gold Project submitted by TVX Hellas S.A. Project LR5566 –Progress Report No. 2, Lakefield Research, June 5, 2000.

An (Pilot Plant) Investigation of The Recovery of Gold from Reclaimed Tailings Samples submitted by TVX Hellas S. A. Project L.R. 5566 – Progress Report No.3, Lakefield Research, May 31, 2000.

A Pilot Plant Investigation of The Recovery of Lead, Zinc and Arsenopyrite/Pyrite from the PEC sample of Olympias ore submitted by TVX Hellas S.A. Project LR5566 –Progress Report No. 4, Lakefield Research, June 6, 2000.

A Laboratory Investigation of the Recovery of Lead and Zinc and the effect of Desliming from the 2001-2003 & High Clay Samples of Olympias Ore submitted by TVX Hellas S.A. Project LR5566 – Progress Report No.6, Lakefield Research, June 5, 2000.

A Laboratory Investigation of Arsenopyrite-Pyrite Separation from AsPy-Py Rougher Concentrates Generated During Pilot Plant Operations submitted by TVX Hellas S.A. Project LR5566 –Progress Report No.8, Lakefield Research, July 14, 2000.

An Investigation of Pilot Scale Regrinding and Washing of Arsenopyrite/Pyrite Flotation Concentrate Generated from the Post East Composite Ore submitted by TVX Hellas S.A. Project LR5566 –Progress Report No.7, Lakefield Research, June 1, 2000.

Environmental Impact Assessment of the Mining-Metallurgical Facilities of Company Hellas Gold in Halkidiki by ENVECO S.A. for Hellas Gold S.A., 2010.

28. CERTIFICATE OF QUALIFICATIONS

Patrick Forward

I, Patrick William Forward, BSc, FIMMM, as an author of this report entitled “Technical Report on the Olympias Project”, prepared for European Goldfields Limited and dated 14 July 2011, do hereby certify that:

1. I am a graduate of the Imperial College of Science and Technology, London and hold a B.Sc. honours degree Mining Geology (1989).

2. I am presently employed as General Manager, Exploration of European Goldfields (Services) Limited of 11 Berkeley Street, Level 3, London, England W1J 8DS. My residential address is of 11 Kirkley Road, London, SW19 3AZ

3. I have been employed in my profession since graduation and with European Goldfields (Services) Limited since October 2004.

4. I have fifteen years’ experience in all aspects of precious and base metal exploration.

5. I am a Fellow of Institute of Materials, Minerals and Mining (Membership 454049) and a Member of the Australasian Institute of Mining and Metallurgy (Membership 225134) and a “qualified person” for the purposes of Canadian National Instrument 43-101 (the “Instrument”).

6. I am responsible for the contents of sections 1 to 12, 14, part of 18, 19 to 27 of the report (the “Report”) dated 14 July 2011, prepared for European Goldfields Limited (the “Issuer”) entitled “Technical Report on the Olympias Project”.

7. The information contained in the Report was obtained from regular visits to the properties that are subject of the Report between November 2004 and February 2011, discussions and data reviews with Hellas Gold SA personnel and detailed discussions with other consultants to European Goldfields Limited. My most recent visit to site was 28th of February 2011 for a duration of five days.

8. There have been no limitations imposed upon my access to persons, information, data or documents that I consider relevant to the subject matter of this report.

9. As of the date hereof, to the best of my knowledge, information and belief, the Report contains all scientific and technical information that is required to be disclosed to make the Report not misleading.

10. I am not independent of the Issuer applying the tests set out in section 1.5 of the Instrument as I am an employee of European Goldfields (Services) Limited, an affiliated entity of the Issuer.

11. I have not had any prior involvement with the properties that are subject of the Report.

12. I have read the Instrument and Form 43-101 F1, and the Report has been prepared in compliance with the Instrument and Form 43-101 F1.

DATED at London, England, this 14th day of July, 2011.

Mr P. W. Forward

EUROPEAN GOLDFIELDS

CERTIFICATE OF AUTHOR

I, **Neil Oswald Liddell,** MIMMM, as an author of this report entitled "Technical Report on the Olympias Project", prepared for European Goldfields Limited and dated 14 July 2011, do hereby certify that:

1. I am Senior Mining Engineer at European Goldfields (Services) Limited of 11 Berkeley Street, Level 3, London, UK, W1J 8DS. My residential address is 50 Chestnut Lane, Park Farm, Ashford, Kent TN23 3LR, UK.
2. I graduated with a B.Sc. Mining Engineering from Leeds University, Leeds, Yorkshire, UK in 1974.
3. I am a Member of the Institute of Materials, Minerals and Mining and a Chartered Engineer.
4. I have practiced my profession for over 35 years since my graduation from university.
5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that I am a "qualified person" for the purposes of NI 43-101.
6. I am responsible for the preparation of Section 15,16 and part of 18 of the technical report titled "Technical Report on the Olympias Project" and dated 14 July, 2011 (the "Technical Report") relating to the Olympias property. I have visited the Olympias property on several occasions between 2007 and 2011 for an approximate total of over 25 days with my most rescent visit being 6th of July 2011 for a duration of three days.
7. I have had no prior involvement with the property that is the subject of the Technical Report. I am not aware of any limitations imposed upon my access to persons, information, data or documents that I consider relevant to the subject matter of the Technical Report.
8. As of the date hereof and to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.
9. I am not independent of European Goldfields Limited and Hellas Gold pursuant to section 1.5 of NI 43-101.
10. I have read NI 43-101 and Form 43-101F1, and the Technical Report has been prepared in compliance with that instrument and form.

Dated this 14th day of July, 2011.

Neil O Liddell

Antony Francis

I, Antony Francis, B.Sc, FIMMM, as an author of this report entitled "Technical Report on the Olympias Project", prepared for European Goldfields Limited and dated 14 July 2011, do hereby certify that:

1. I am Senior Metallurgist at European Goldfields (Services) Limited of Level 3, 11 Berkeley Street, London, UK, W1J 8DS. My residential address is 8, Coulter Road, Kingsnorth, Ashford, Kent, TN23 3JQ, UK.

2. I graduated with a B.Sc. Hons, (Eng) Met degree from the Royal School of Mines, Imperial College of Science, Technology & Medicine, London University in 1971.

3. I am a Fellow of the Institute of Materials, Minerals and Mining.

4. I have practiced my profession for a total of 38 years since my graduation from university.

5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify that I am a "qualified person" for the purposes of NI 43-101.

6. I am responsible for the preparation of Sections 13 and 17 of the technical report entitled "Technical Report on the Olympias Project" and dated 14 July 2011 (the "Technical Report") relating to the Olympias property. I have visited the Olympias property on regular occasions during 2005, 2006, 2007, 2008, 2009, 2010 and 2011 for an approximate total of 40 days with the most recent visit being from the 6th of July 2011 for a duration of three days.

7. I have had no prior involvement with the property that is the subject of the Technical Report. I am not aware of any limitations imposed upon my access to persons, information, data or documents that I consider relevant to the subject matter of the Technical Report.

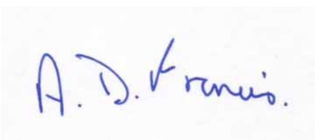
8. As at the date hereof and to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the Technical Report not misleading.

9. I am not independent of European Goldfields Limited and Hellas Gold SA pursuant to section 1.5 of NI 43-101.

10. I have read NI 43-101 and Form 43-101F1, and the Technical Report has been prepared in compliance with that instrument and form.

11. I own securities of European Goldfields Limited in the form of shares, and as such I have an indirect interest in the Olympias property.

Dated at London, England, this 14th day of July 2011.



Antony Francis

Appendix 1. Summary of Mineralised One Metre Composites from the Olympias Deposit

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23627.66	-18167	-178.41	96001	23.9	41.5	1.17	6.51
23628.54	-18167.4	-178.41	96001	21.9	113.75	3.53	7.16
23630.29	-18168.4	-178.41	96001	20.34	229	6.21	5.4
23629.42	-18167.9	-178.41	96001	20.12	207.5	6.05	6.6
23646.97	-18177.5	-178.41	96001	12.8	106	6.86	13.8
23647.84	-18178	-178.41	96001	11.7	57.4	2.56	6.06
23646.09	-18177	-178.41	96001	8.95	106.25	5.66	7.18
23639.07	-18173.2	-178.41	96001	8.01	23.4	0.74	9.29
23639.95	-18173.7	-178.41	96001	7.5	98.2	2.43	9.9
23640.82	-18174.2	-178.41	96001	6.99	173	4.13	10.5
23636.44	-18171.8	-178.41	96001	6.51	10.1	0.35	4.6
23637.31	-18172.2	-178.41	96001	6.51	10.1	0.35	4.6
23648.72	-18178.5	-178.41	96001	6.33	32.2	1.48	3.29
23641.7	-18174.6	-178.41	96001	5.1	106.5	4.45	0.57
23642.58	-18175.1	-178.41	96001	5.1	106.5	4.45	0.57
23643.46	-18175.6	-178.41	96001	5.1	106.5	4.45	0.57
23644.33	-18176.1	-178.41	96001	5.1	106.5	4.45	0.57
23645.21	-18176.6	-178.41	96001	5.1	106.5	4.45	0.57
23626.51	-18166.7	-172.19	96003	25.71	83.3	2.9	2.04
23630.3	-18168.9	-168.1	96003	22.41	172	9.65	12.8
23627.14	-18167.1	-171.51	96003	20.66	63.25	2.13	1.47
23629.67	-18168.5	-168.78	96003	19	107.6	5.5	6.84
23627.77	-18167.4	-170.83	96003	15.6	43.2	1.35	0.89
23628.4	-18167.8	-170.14	96003	15.6	43.2	1.35	0.89
23629.03	-18168.2	-169.46	96003	15.6	43.2	1.35	0.89
23630.93	-18169.3	-167.42	96003	15.3	282	9.26	4.96
23631.56	-18169.6	-166.73	96003	15.3	282	9.26	4.96
23624.61	-18165.2	-174.17	96005	33.3	103	4.08	2.27
23624.61	-18165.2	-173.17	96005	33.3	103	4.08	2.27
23624.61	-18165.2	-172.17	96005	10.1	32.3	1.27	0.8
23624.61	-18165.2	-175.17	96005	1.1	5	0.18	0.25
23636.25	-18138	-178.1	96006	33.75	56.5	8.42	0.75
23637.25	-18138	-178.1	96006	28.83	32.9	3.5	1.18
23635.25	-18138	-178.1	96006	24.26	55.4	8.47	2.4
23647.25	-18137.9	-178.1	96006	22.63	236.8	6.42	7.46
23638.25	-18138	-178.1	96006	21.77	29.3	3.36	1.47
23639.25	-18138	-178.1	96006	21.77	29.3	3.36	1.47
23648.25	-18137.9	-178.1	96006	15.21	156.75	4.61	5.07
23634.25	-18138	-178.1	96006	10.2	27.15	2.06	2.4
23649.25	-18137.9	-178.1	96006	7.23	18.4	1.04	2.75
23650	-18137.9	-178.1	96006	7.23	18.4	1.04	2.75

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23645.25	-18137.9	-178.1	96006	5.05	25.83	1.17	4.29
23646.25	-18137.9	-178.1	96006	4.33	49.8	0.55	1.49
23633.25	-18138.1	-178.1	96006	3.48	20	0.38	0.6
23657.75	-18137.8	-178.1	96006	1.59	5	0.15	0.08
23658.75	-18137.8	-178.1	96006	1.59	5	0.15	0.08
23636.26	-18140.7	-173.76	96008	13.14	18.1	0.79	1.98
23638.25	-18141.8	-171.79	96008	13.14	40.9	5.53	0.88
23636.92	-18141.1	-173.11	96008	12.87	39.28	2.58	2.6
23633.6	-18139.3	-176.39	96008	10.88	48.54	3.33	10.85
23637.59	-18141.5	-172.45	96008	10.83	67.92	6.18	2.53
23634.26	-18139.7	-175.73	96008	8.94	37.64	4.34	7.35
23632.93	-18139	-177.04	96008	6.75	39.9	3.52	7.22
23639.98	-18142.7	-170.09	96008	6.54	41.6	3.07	3.21
23638.92	-18142.2	-171.14	96008	5.76	34.98	2.36	2.4
23639.58	-18142.5	-170.48	96008	5.75	39.17	2.62	3.08
23635.59	-18140.4	-174.42	96008	1.71	6.8	0.25	0.21
23634.93	-18140	-175.07	96008	1.38	9	0.35	0.24
23632.05	-18138.4	-171.9	96010	21.3	6	0.09	0.07
23632.05	-18138.4	-170.9	96010	20.76	23.4	0.34	0.71
23632.05	-18138.4	-172.9	96010	14.65	13.04	0.54	0.7
23632.05	-18138.4	-173.9	96010	9.62	13.12	0.4	3.1
23632.05	-18138.4	-174.9	96010	5.92	12.6	0.44	2.37
23632.05	-18138.4	-166.9	96010	5.61	17.3	0.75	1.17
23632.05	-18138.4	-165.9	96010	5.61	17.3	0.75	1.17
23632.05	-18138.4	-175.9	96010	4.94	13	0.58	0.89
23632.05	-18138.4	-167.9	96010	3.12	15.32	0.86	1.09
23632.05	-18138.4	-168.9	96010	1.21	11.6	0.51	2.94
23632.05	-18138.4	-169.9	96010	1.05	10	0.23	4.22
23796.23	-18644.9	-188.78	96011	10.8	92	2.5	23
23795.55	-18645.2	-188.78	96011	10.8	92	2.5	23
23797.14	-18644.5	-188.78	96011	10.08	74.7	2.99	16.5
23796.33	-18629	-188.76	96012	5.8	377	16.3	15.7
23799.96	-18627.4	-188.76	96012	2.86	641	25.7	14.8
23624.67	-18097.3	-177.84	96013	14.35	9.5	0.71	0.6
23627.66	-18097.3	-178.11	96013	2.76	12.3	0.22	0.61
23626.67	-18097.3	-178.02	96013	2.35	10.84	0.2	0.52
23621.68	-18097.3	-177.58	96013	1.24	5	0.09	0.09
23784.6	-18599	-184.77	96027	14.2	149	5.79	15.1
23784.6	-18599	-186.52	96027	9.3	187	7.55	8.01
23784.6	-18599	-185.52	96027	7.53	174	6.23	10.7
23770.55	-18576.3	-186.12	96031	7.43	74.6	3.02	9.1
23770.55	-18576.3	-174.42	96031	4.8	270	12.5	11.4
23770.55	-18576.3	-173.42	96031	4.8	270	12.5	11.4

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23770.55	-18576.3	-172.52	96031	4.8	270	12.5	11.4
23770.55	-18576.3	-185.12	96031	2.24	105	2.29	1.89
23770.55	-18576.3	-184.12	96031	2.24	105	2.29	1.89
23738.16	-18535.2	-176.03	96039	8.66	393	14.6	9.02
23738.16	-18535.2	-178.53	96039	7	545	15.2	14.2
23738.16	-18535.2	-175.03	96039	6.8	268	8.78	7.18
23738.16	-18535.2	-177.68	96039	4.09	660	23	9.36
23708.41	-18468.9	-189.85	96041	3.61	140	5.38	1.53
23708.86	-18468.6	-189.85	96041	3.61	140	5.38	1.53
23692.54	-18447.9	-190.02	96047	9	136	5.81	7.95
23698.81	-18438.8	-190.02	96047	6.08	79.9	3.44	16.5
23699.38	-18438	-190.02	96047	4.86	114.95	4.89	23.8
23695.96	-18442.9	-190.02	96047	2.02	137	4.87	1.76
23712.81	-18494.9	-179.17	96049	11.3	404	11	9.61
23712.81	-18494.9	-176.17	96049	10.7	306	9.57	5.32
23712.81	-18494.9	-178.42	96049	8.11	317	12.6	6.33
23712.81	-18494.9	-172.17	96049	7.74	574	11.8	3.73
23712.81	-18494.9	-186.17	96049	6.99	220	9.28	13
23712.81	-18494.9	-171.17	96049	6.81	783	18.7	3.64
23712.81	-18494.9	-174.17	96049	5.95	207	4.64	6.8
23712.81	-18494.9	-184.17	96049	4.47	236	7.74	4.74
23683.5	-18286.8	-204.74	96053	24.8	90	0.83	4.72
23684.43	-18286.5	-204.67	96053	22.7	137.5	6.26	5.23
23665.88	-18293.8	-206.07	96053	17	44	1.62	2
23666.81	-18293.4	-206	96053	17	44	1.62	2
23660.32	-18296	-206.49	96053	16.4	85	3.04	4.9
23661.24	-18295.6	-206.42	96053	15.76	65.22	2.18	7.38
23662.17	-18295.3	-206.35	96053	15	42	1.16	10.3
23682.58	-18287.2	-204.81	96053	14.3	74	2.07	2.1
23667.64	-18293.1	-205.93	96053	10.55	218.5	8.98	3.83
23663.1	-18294.9	-206.28	96053	7.65	21	0.57	4.1
23664.03	-18294.5	-206.21	96053	7.65	21	0.57	4.1
23676.83	-18289.5	-205.24	96053	4.42	9	0.16	0.6
23674.04	-18290.6	-205.45	96053	2.08	19	0.34	0.49
23675.9	-18289.8	-205.31	96053	1.76	4.8	0.09	0.4
23674.97	-18290.2	-205.38	96053	1.64	14.2	0.26	0.44
23869.74	-18675.2	-211.01	96055	10.77	292	9.6	5.82
23870.27	-18674.6	-211.63	96055	10.77	292	9.6	5.82
23870.8	-18674	-212.24	96055	10.5	326	11.6	8.64
23871.33	-18673.4	-212.86	96055	10.5	326	11.6	8.64
23871.86	-18672.9	-213.47	96055	9.44	343.5	12.35	9.92
23872.39	-18672.3	-214.09	96055	8.37	361	13.1	11.2
23872.92	-18671.7	-214.71	96055	8.37	361	13.1	11.2

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23868.68	-18676.4	-209.78	96055	6.96	552	17.6	7.48
23869.21	-18675.8	-210.4	96055	6.96	552	17.6	7.48
23661.86	-18295.2	-197.79	96056	3.63	40	0.94	0.77
23662.47	-18295	-197.02	96056	3.63	40	0.94	0.77
23865.17	-18679.5	-208.74	96058	5.82	584	11.7	22.8
23865.17	-18679.5	-207.99	96058	4.21	327	9.61	20.4
23801.06	-18586.4	-208.07	96066	3.48	220	10.79	25
23799.96	-18586.9	-206.01	96067	9.79	44	2.22	4.5
23803.97	-18585.3	-201.84	96067	1.41	9	0.22	0.48
23806.27	-18584.2	-215.43	96068	2.91	4.1	0.08	0.4
23765.67	-18524.8	-212.11	96072	11.97	200	8.09	6.54
23765.67	-18524.8	-213.11	96072	11.97	200	8.09	6.54
23793.84	-18590.3	-207.68	96073	4.91	194.25	4.43	3.16
23798.56	-18575.3	-207.88	96074	1.91	6.9	0.14	0.31
23799.48	-18574.9	-207.88	96074	1.91	6.9	0.14	0.31
23815.63	-18568.3	-229.52	96076	17.01	30.5	0.91	1.43
23816.3	-18568.1	-230.21	96076	17.01	30.5	0.91	1.43
23799.36	-18575.1	-212.5	96076	2.8	18	0.61	1.35
23799.86	-18574.9	-213.02	96076	2.8	18	0.61	1.35
23801.02	-18574.4	-214.24	96076	2.32	16.4	0.55	1.26
23801.69	-18574.1	-214.93	96076	2.32	16.4	0.55	1.26
23798.03	-18575.7	-211.11	96076	2.07	17.7	0.6	1.1
23798.7	-18575.4	-211.81	96076	2.07	17.7	0.6	1.1
23774.83	-18539	-208.52	96077	2.45	41.9	1.62	1.5
23775.69	-18538.5	-208.52	96077	2.45	41.9	1.62	1.5
23776.54	-18538	-208.52	96077	2.45	41.9	1.62	1.5
23794.42	-18577.3	-217.54	96079	11.28	84.3	3.21	0.94
23794.42	-18577.3	-218.54	96079	11.28	84.3	3.21	0.94
23776.73	-18536.3	-213.24	96080	9.33	245	8.97	2.21
23775.68	-18537.4	-211.95	96080	7.83	165	5.38	7.52
23776.2	-18536.8	-212.6	96080	7.83	165	5.38	7.52
23774.64	-18538.5	-210.66	96080	5.96	141	5.47	14.3
23773.59	-18539.6	-209.36	96080	3.22	199	7.87	8.04
23774.11	-18539	-210.01	96080	3.22	199	7.87	8.04
23700.99	-18444	-208.68	96085	9.42	87.9	3.77	0.17
23701.98	-18443.9	-208.68	96085	7.29	48.3	1.99	10.02
23722.61	-18459	-208.73	96086	20.95	21.8	0.05	0.56
23721.45	-18460	-208.73	96086	9.44	47.95	1.6	1.34
23720.67	-18460.6	-208.73	96086	5.34	428	15.6	8.98
23722.03	-18459.5	-208.73	96086	4.99	38.5	1.24	0.52
23719.12	-18461.8	-208.73	96086	4.98	229	8.66	10.2
23719.9	-18461.2	-208.73	96086	4.46	252.4	9.82	9.77
23730.97	-18450.1	-229.86	96087	10.68	158.1	5.36	7.54

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23727.33	-18453.5	-225.26	96087	8.68	294	9.57	3.21
23728.95	-18452	-227.3	96087	8.32	96.9	3.66	11.9
23730.56	-18450.5	-229.35	96087	7.93	23.66	1.72	0.78
23727.87	-18453	-225.94	96087	7.2	114	3.79	17.9
23728.41	-18452.5	-226.62	96087	7.18	130	4.52	12.7
23729.49	-18451.5	-227.98	96087	3.5	34.88	1.3	4.03
23730.03	-18451	-228.67	96087	2.9	7.88	0.27	0.59
23726.8	-18454	-224.57	96087	1.44	62.5	2.64	0.1
23726.26	-18454.5	-223.89	96087	1.37	48.1	2.06	0.04
23714.23	-18465.4	-209.86	96088	5.18	302	11.8	0.22
23718.36	-18463.5	-203.91	96089	65.62	22	0.73	3.35
23718.86	-18463.3	-203.4	96089	54.65	7.7	0.1	0.07
23717.69	-18463.8	-204.6	96089	37.1	140	5.17	4.24
23719.36	-18463.1	-202.89	96089	21.74	4.6	0.17	0.05
23733.68	-18485.5	-208.59	96092	22.9	51.4	1.88	1.99
23734.4	-18485.3	-208.59	96092	3.32	6	0.21	0.79
23720.52	-18489.1	-208.32	96095	2.33	66.3	3.14	9.1
23676.15	-18317.5	-207.05	96098	35.18	121	3.09	6.11
23672.74	-18319.6	-207.05	96098	27.22	253	6.05	8.29
23675.3	-18318	-207.05	96098	25.3	66.4	1.93	6.47
23671.89	-18320.1	-207.05	96098	21.81	10.8	0.28	0.6
23674.45	-18318.5	-207.05	96098	21.05	52.7	1.36	3.82
23677.86	-18316.4	-207.05	96098	20.02	39	1.22	1.92
23677.01	-18317	-207.05	96098	17.76	148	3.7	8.22
23673.59	-18319.1	-207.05	96098	16.94	107	2.96	0.83
23681.27	-18314.4	-207.05	96098	8.44	189.13	4	1.62
23671.03	-18320.6	-207.05	96098	7.37	0.9	0.69	0.39
23670.18	-18321.1	-207.05	96098	7.11	68.95	2.17	3.37
23679.57	-18315.4	-207.05	96098	6.87	17.62	0.66	0.39
23669.33	-18321.7	-207.05	96098	4.74	100.9	2.62	4.18
23680.42	-18314.9	-207.05	96098	2.13	23.5	0.9	0.17
23672.34	-18318.9	-219.19	96100	21.36	586.5	14.52	3.38
23673.25	-18318.2	-220.83	96100	18.34	576	16.5	6.7
23672.79	-18318.6	-220.01	96100	18.17	771.5	20.35	2.55
23673.7	-18317.9	-221.65	96100	17.32	327.44	9.09	9.54
23671.88	-18319.3	-218.37	96100	15.57	204.55	5.84	2.6
23669.16	-18321.4	-213.45	96100	11.4	133	5.59	3.27
23669.61	-18321	-214.27	96100	11.4	133	5.59	3.27
23686.73	-18307.8	-245.16	96100	9.2	67.36	3.47	3.91
23693.54	-18302.5	-257.44	96100	6.51	129.25	9.15	7.55
23693.08	-18302.9	-256.62	96100	6.3	108.75	6.6	4.44
23686.27	-18308.1	-244.34	96100	5.94	46.1	2.34	2.55
23679.47	-18313.4	-232.05	96100	5.08	12.48	0.3	1.12

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23693.88	-18302.3	-258.06	96100	4.94	117	11	14.8
23679.92	-18313	-232.87	96100	4.58	10.14	0.34	0.38
23671.43	-18319.6	-217.55	96100	3.37	38.55	1.2	0.7
23692.63	-18303.2	-255.8	96100	3.16	39.25	3.02	4.41
23681.74	-18311.6	-236.15	96100	2.2	2.4	0.11	0.3
23687.18	-18307.4	-245.97	96100	2.03	3.92	0.09	0.62
23678.1	-18314.4	-229.59	96100	1.88	30.94	0.24	0.62
23682.19	-18311.3	-236.96	96100	1.88	16.7	0.36	1.25
23687.64	-18307.1	-246.79	96100	1.88	4.58	0.13	0.71
23682.64	-18310.9	-237.78	96100	1.64	5.7	0.06	1.19
23676.74	-18315.5	-227.13	96100	1.61	16.3	0.32	0.75
23685.82	-18308.5	-243.52	96100	1.36	12.4	0.43	0.83
23690.81	-18304.6	-252.53	96100	1.3	1.9	0.1	0.39
23670.98	-18320	-216.73	96100	1.29	11	0.26	0.57
23684	-18309.9	-240.24	96100	1.25	2.7	0.14	0.37
23678.56	-18314.1	-230.41	96100	1.19	94.18	0.21	0.27
23683.1	-18310.6	-238.6	96100	1.18	7.5	0.18	0.54
23679.01	-18313.7	-231.23	96100	1.14	3.22	0.08	0.31
23689.91	-18305.3	-250.89	96100	1.11	2.6	0.07	0.31
23665.23	-18324.5	-217.55	96102	10.7	178	6.06	5.24
23665.23	-18324.5	-220.3	96102	1.57	31.5	0.97	0.14
23665.23	-18324.5	-221.3	96102	1.3	24	0.83	0.09
23674.66	-18317.7	-196.69	96104	22.2	22.8	0.73	0.22
23674.03	-18318.1	-197.33	96104	3.06	7.6	0.26	0.41
23665.23	-18324.5	-200.05	96106	17	51	1.69	3.18
23690.1	-18351.9	-207.59	96108	2.95	407	12	0.24
23691.02	-18351.5	-207.59	96108	2.95	407	12	0.24
23696.58	-18349.3	-207.59	96108	2.35	57.48	1.89	0.52
23685.46	-18353.8	-207.59	96108	2.16	2.7	0.02	0
23695.66	-18349.6	-207.59	96108	1.67	32.52	1.12	1.77
23688.24	-18352.6	-207.59	96108	1.57	13.86	0.33	0.28
23676.05	-18385.5	-207.86	96114	1.69	15.1	0.45	0.35
23675.19	-18386	-207.86	96114	1.36	9.6	0.25	0.96
23676.92	-18385	-207.86	96114	1.21	10.9	0.36	0.65
23800.31	-18593.7	-192.22	96117	22.35	221	8.37	3.78
23800.31	-18593.7	-191.67	96117	22.35	221	8.37	3.78
23784.69	-18562.6	-197.8	96119	11.77	93.3	2.23	3.67
23785.13	-18562	-197.8	96119	8.76	65.7	2.13	8.73
23691.86	-18386.2	-216.62	96120	3.42	25.3	0.73	0.04
23693.43	-18384.7	-218.74	96120	1.83	9.2	0.23	0
23769.26	-18555.6	-191.83	96121	15.28	89.5	3.04	1.08
23769.26	-18555.6	-192.83	96121	9.06	179	6.77	1.82
23769.26	-18555.6	-186.18	96121	3.52	398	9.93	2.58

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23769.26	-18555.6	-183.53	96121	2.02	374	11.7	4.96
23769.26	-18555.6	-188.83	96121	1.68	25.8	0.89	3.19
23774.89	-18581.1	-196.6	96123	5.66	161.94	3.61	14.66
23775.6	-18580.3	-196.6	96123	2.08	89.36	1.49	3.46
23780.38	-18575	-191.62	96125	16.05	36	1.46	4.06
23780.38	-18575	-193.62	96125	13.56	25.9	1.11	4.32
23673.53	-18402.8	-207.96	96126	7.16	127.5	5.86	14.6
23672.78	-18403.4	-207.96	96126	6.65	127	5.11	10.6
23675.02	-18401.4	-207.96	96126	6.51	286	9.59	10.6
23674.28	-18402.1	-207.96	96126	6.03	137	5.13	10.1
23675.77	-18400.8	-207.96	96126	5.39	60.4	2.05	4.14
23672.03	-18404.1	-207.96	96126	3.53	101.78	2.25	0.27
23676.52	-18400.1	-207.96	96126	2.45	41.8	1.45	3.19
23681.76	-18395.5	-207.96	96126	1.83	15.5	0.34	0.72
23682.51	-18394.8	-207.96	96126	1.59	35	0.99	1.52
23680.26	-18396.8	-207.96	96126	1.45	84.1	2.74	1.27
23691.37	-18420.2	-208.17	96128	6.58	75.2	2.77	9.51
23690.43	-18420.5	-208.17	96128	6.14	30.5	1.45	3.05
23707.01	-18411.9	-228.7	96130	15.3	81.2	4.41	2.19
23705.12	-18412.8	-226.57	96130	9.5	170.5	5.91	10.3
23706.38	-18412.2	-227.99	96130	7.04	47.4	1.9	1.93
23693.19	-18419	-213.14	96130	6.86	20.6	2.84	3.11
23705.75	-18412.5	-227.28	96130	6.68	45.6	1.12	1.09
23698.84	-18416.1	-219.5	96130	6.25	266	9.3	6.41
23699.47	-18415.8	-220.21	96130	5.76	219	8.04	13.5
23707.63	-18411.5	-229.4	96130	5.35	23	2.02	1.89
23698.22	-18416.4	-218.8	96130	4.58	47.7	1.82	6.74
23700.1	-18415.4	-220.92	96130	4.29	352	8.97	7.51
23695.7	-18417.7	-215.97	96130	3.41	85.5	3.18	3.75
23697.59	-18416.8	-218.09	96130	3.29	53.3	2.19	4.1
23693.82	-18418.7	-213.85	96130	2.56	11.35	0.34	1.89
23695.08	-18418.1	-215.26	96130	2.52	55.55	2.31	4.1
23703.24	-18413.8	-224.45	96130	2.25	325	3.64	1.57
23694.45	-18418.4	-214.55	96130	2.14	20.95	0.96	3.91
23696.96	-18417.1	-217.38	96130	2.02	98.6	3.77	4.47
23709.52	-18410.6	-231.52	96130	1.84	11.95	0.48	1.14
23710.77	-18409.9	-232.94	96130	1.8	10	0.23	0.42
23703.87	-18413.5	-225.16	96130	1.12	59.4	1.63	1.27
23745.03	-18507.7	-200.74	96133	18.86	53.6	2.26	1.3
23742.48	-18509.2	-200.74	96133	9.33	36.6	1.35	1.47
23747.37	-18506.2	-200.74	96133	7.17	18.3	0.44	0.05
23739.08	-18511.3	-200.74	96133	6.11	162.5	6.7	6.49
23736.4	-18513	-188.76	96134	8.44	336	11.99	5.41

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23736.4	-18513	-189.76	96134	8.15	194	7.58	6.24
23736.4	-18513	-193.76	96134	4.01	59	2.04	1.76
23736.4	-18513	-195.76	96134	1.71	148	5.07	4.99
23688.52	-18421.5	-217.75	96135	21.1	126.5	4.02	3.41
23688.52	-18421.5	-215	96135	19.9	32.7	1.45	2.52
23688.52	-18421.5	-217	96135	12.35	82.25	2.72	3.3
23688.52	-18421.5	-216	96135	11.76	35.35	1.43	2.85
23688.52	-18421.5	-218.5	96135	4.31	21.8	0.74	0.88
23692.11	-18420.2	-204.73	96137	37.5	76.7	2.95	2.82
23689.95	-18421	-206.66	96137	23.9	30.6	1.08	1.35
23676.35	-18431.6	-208.36	96138	9.57	336	12.1	1.35
23677.05	-18431.1	-208.36	96138	8.73	384.5	13.5	6.44
23681	-18428.4	-208.36	96138	7.74	283	10.3	4.71
23677.87	-18430.5	-208.36	96138	6.15	330	10.5	5.56
23679.52	-18429.4	-208.36	96138	4.98	213	8.06	15.1
23682.44	-18427.4	-208.36	96138	4.92	49.6	1.88	22.1
23681.66	-18427.9	-208.36	96138	4.78	177.84	6.55	2.91
23680.34	-18428.8	-208.36	96138	4.47	188	6.2	12.3
23678.7	-18430	-208.36	96138	4.17	170	6.38	17.6
23684.05	-18426.3	-208.36	96138	3.27	648	23.6	13.6
23683.22	-18426.9	-208.36	96138	2.79	82.9	3.25	28.6
23684.87	-18425.7	-208.36	96138	2.31	98.1	3.75	28.2
23713.96	-18462.6	-201.2	96139	72.42	128	5.01	3.03
23712.49	-18464	-201.2	96139	56.17	23.6	0.93	1.23
23713.23	-18463.3	-201.2	96139	30.15	44	1.69	0.99
23715.33	-18461.4	-201.2	96139	22.7	7.14	0.21	0.07
23714.7	-18462	-201.2	96139	7.59	6.5	0.3	0.25
23702.3	-18449.3	-199.5	96140	61.79	126.26	4.44	1.88
23703.15	-18448.8	-199.5	96140	32.47	87.3	3.33	2.57
23704	-18448.3	-199.5	96140	14.98	384.5	16.4	1.81
23708	-18445.8	-199.5	96140	12.55	325	11.2	0.65
23691.41	-18443.6	-199.34	96143	8.74	420	16.5	4.06
23690.76	-18444	-199.34	96143	8.74	420	16.5	4.06
23700.07	-18226.1	-214.01	96144	9.38	9.95	0.86	0.96
23700.6	-18225.2	-214.01	96144	8.73	10.85	1.34	0.65
23699.53	-18226.9	-214.01	96144	6.6	6	0.22	0.71
23699	-18227.8	-214.01	96144	4.49	3.85	0.19	0.61
23697.94	-18229.5	-214.01	96144	3.48	2.7	0.1	0.57
23698.47	-18228.6	-214.01	96144	2.25	3.1	0.17	0.61
23697.41	-18230.3	-214.01	96144	2.12	1.25	0.05	0.39
23687.97	-18418.6	-199.02	96145	12.3	96.3	3.17	4.61
23672.34	-18430.5	-199.07	96146	6.24	364.86	13.41	11.57
23671.54	-18431.1	-199.07	96146	6.11	318	11.26	9.01

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23676.36	-18427.5	-199.07	96146	6	409.75	15.8	5.93
23679.57	-18425.1	-199.07	96146	5.79	188.78	7.6	16.32
23680.37	-18424.5	-199.07	96146	5.42	103.07	3.81	21.06
23673.95	-18429.3	-199.07	96146	5.21	281.08	7.43	13.01
23681.18	-18424	-199.07	96146	4.92	300	11.1	5.12
23678.77	-18425.7	-199.07	96146	4.57	181.5	7.07	13.45
23673.14	-18429.9	-199.07	96146	4.17	118.04	4.7	8.73
23677.16	-18426.9	-199.07	96146	4.12	203.25	9.19	3.31
23670.73	-18431.7	-199.07	96146	3.57	132.95	4.71	2.74
23675.55	-18428.1	-199.07	96146	3.51	260.2	8.84	3.87
23677.96	-18426.3	-199.07	96146	3.24	127	4.95	7.03
23670.13	-18432.1	-199.07	96146	1.54	49.9	2.21	0.37
23677.82	-18386.8	-204.38	96147	36.89	341	7.01	3.4
23676.23	-18388	-204.38	96147	8.82	37.8	0.89	7.51
23677.02	-18387.4	-204.38	96147	7.27	17.1	0.34	4
23680.2	-18384.9	-204.38	96147	1.9	84.9	2.07	8.6
23683.15	-18382.7	-204.38	96147	1.73	1	0.1	0.04
23683.94	-18382.1	-204.38	96147	1.15	2.28	0.1	0.2
23688.35	-18242.2	-242.54	96148	8.19	116	2.76	4.11
23688.08	-18242.7	-241.72	96148	7.51	113.2	2.65	3.85
23679.42	-18258.9	-215.51	96148	5.89	105	3.74	5.9
23689.43	-18240.2	-245.82	96148	1.73	5.35	0.17	1.41
23689.98	-18239.2	-247.46	96148	1.7	2.2	0.07	0.32
23690.25	-18238.6	-248.28	96148	1.62	3.05	0.09	0.59
23689.71	-18239.7	-246.64	96148	1.25	3.75	0.13	1.08
23670.26	-18398.3	-194.17	96151	24.93	146.65	5.35	0.9
23662.4	-18402.6	-194.17	96151	10.7	-999	-999	-999
23663.24	-18402.1	-194.17	96151	9.35	231	8.38	18.4
23664.12	-18401.6	-194.17	96151	6.43	187.5	6.05	14.5
23682.6	-18253.4	-207.36	96152	20.1	185	8.82	6.86
23682.21	-18254.1	-207.97	96152	12.7	283	6.4	8.36
23682.99	-18252.7	-206.74	96152	1.71	38	1.29	1.13
23683.38	-18252	-206.13	96152	1.27	3.1	0.14	0.36
23684.16	-18250.7	-204.9	96152	1.22	3.6	0.29	0.31
23661.12	-18288.2	-214.32	96153	36.2	35.4	4.59	0.9
23665.54	-18281.5	-214.32	96153	5.26	3.3	0.11	0.2
23664.99	-18282.3	-214.32	96153	1.24	1.5	0.05	0.17
23678.61	-18260.1	-221.09	96154	6.87	35.68	1.99	2.39
23678.61	-18260.1	-220.09	96154	4.57	23.88	1.28	1.55
23678.61	-18260.1	-221.89	96154	1.72	10	0.47	0.6
23678.61	-18260.1	-215.39	96154	1.21	30	1.41	2.5
23663.68	-18362.9	-194.2	96155	26.7	34.5	2.09	2.82
23664.49	-18362.3	-194.2	96155	9.03	90.3	2.55	10.6

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23678.34	-18352.4	-194.2	96155	1.57	7.5	0.15	0.11
23679.16	-18351.9	-194.2	96155	1.08	5.1	0.09	0.09
23678.61	-18260.1	-205.61	96156	27.1	234	0.18	1.19
23678.61	-18260.1	-193.61	96156	26.3	70.4	3.09	3.59
23678.61	-18260.1	-191.76	96156	21.4	74.1	2.15	1.7
23678.61	-18260.1	-194.61	96156	9.18	234	7.17	7.76
23678.61	-18260.1	-195.61	96156	8.25	306	9.27	8.28
23678.61	-18260.1	-204.61	96156	8.16	40.4	0.91	1.4
23678.61	-18260.1	-203.61	96156	3.23	13.6	0.47	1.18
23678.61	-18260.1	-198.61	96156	3.19	20.4	0.48	0.55
23678.61	-18260.1	-200.61	96156	3.16	38.7	1.11	0.8
23678.61	-18260.1	-209.61	96156	3.14	6.6	0.51	1.04
23678.61	-18260.1	-197.61	96156	2.83	36	1.08	2.14
23678.61	-18260.1	-207.61	96156	2.57	39.5	0.9	2.73
23678.61	-18260.1	-196.61	96156	2.48	316	8.13	13.2
23678.61	-18260.1	-206.61	96156	2.13	17.4	0.39	1.36
23678.61	-18260.1	-202.61	96156	1.91	6.7	0.18	0.43
23678.61	-18260.1	-208.61	96156	1.79	13.5	0.34	0.77
23678.61	-18260.1	-201.61	96156	1.69	114	3.51	2.12
23678.61	-18260.1	-199.61	96156	1.49	30	0.82	0.23
23667.55	-18313.3	-214.56	96157	13.4	85.5	2.9	0.53
23675.02	-18305.2	-214.56	96157	12.68	17.7	0.66	0.88
23674.34	-18306	-214.56	96157	11.24	19.6	0.72	1.43
23668.23	-18312.6	-214.56	96157	10.7	92.9	3.49	2.36
23677.06	-18303	-214.56	96157	10	116	3.34	3.93
23677.74	-18302.3	-214.56	96157	7.26	15.9	0.42	2.69
23678.42	-18301.6	-214.56	96157	6.78	5.4	0.1	0.21
23673.66	-18306.7	-214.56	96157	6.61	20.7	0.62	2.72
23679.78	-18300.1	-214.56	96157	6.46	115	3.53	2.58
23679.1	-18300.8	-214.56	96157	5.62	11	0.29	0.61
23671.62	-18308.9	-214.56	96157	5.52	16.1	0.46	1.65
23670.26	-18310.4	-214.56	96157	4.3	7.5	0.47	0.55
23672.98	-18307.4	-214.56	96157	4.25	15	0.44	2.22
23680.46	-18299.4	-214.56	96157	4.05	89.5	2.5	1.99
23672.3	-18308.2	-214.56	96157	3.77	10.65	0.29	1.07
23660.11	-18366.2	-194.22	96158	15.9	36.3	4.76	6.64
23684.76	-18294.5	-214.59	96159	19.35	156.9	4.97	7.03
23685.51	-18293.8	-214.59	96159	17.01	102	3.26	6.66
23687.02	-18292.5	-214.59	96159	14.8	123.5	2.83	2.38
23687.78	-18291.9	-214.59	96159	11.6	22.1	0.6	3.92
23689.29	-18290.5	-214.59	96159	2.47	5.5	0.26	0.46
23688.53	-18291.2	-214.59	96159	2.37	5.2	0.48	0.04
23683.87	-18295.2	-216.2	96160	14.4	81.5	2.6	7.84

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23685.84	-18293.1	-220.3	96160	13.92	18	0.42	0.86
23686.63	-18292.3	-221.93	96160	12.5	20.2	0.85	6.97
23689.39	-18289.4	-227.67	96160	11.9	41.8	1.52	0.31
23687.42	-18291.4	-223.57	96160	11	40	2.02	8.9
23684.26	-18294.8	-217.02	96160	10.8	48.92	1.78	5.45
23687.02	-18291.9	-222.75	96160	10.8	10.4	0.28	4.68
23688.21	-18290.6	-225.21	96160	10.6	58.5	0.97	5.66
23687.81	-18291	-224.39	96160	9.57	88	2.83	3
23693.34	-18285.2	-235.86	96160	9.1	55.2	2.04	1.98
23689	-18289.8	-226.85	96160	8.63	30.5	0.97	0.27
23685.45	-18293.5	-219.48	96160	8.46	7.3	0.11	1.94
23692.94	-18285.6	-235.04	96160	7.23	359	9.39	4.04
23688.6	-18290.2	-226.03	96160	7.05	24.7	0.58	0.26
23685.05	-18293.9	-218.66	96160	6.38	19.6	0.51	0.35
23686.24	-18292.7	-221.11	96160	5.97	7.4	0.26	1.63
23691.37	-18287.3	-231.76	96160	4.29	13.1	0.38	0.3
23689.79	-18288.9	-228.49	96160	4.27	9.7	0.4	0.17
23693.73	-18284.8	-236.68	96160	3.81	15.9	0.79	0.69
23690.97	-18287.7	-230.94	96160	1.91	104	3.12	0.09
23694.13	-18284.4	-237.5	96160	1.38	7.5	0.31	0.21
23692.55	-18286	-234.22	96160	1.26	11.1	0.4	1.19
23691.76	-18286.9	-232.58	96160	1.23	5.3	0.14	0.5
23694.52	-18283.9	-238.32	96160	1.11	1.6	0.03	0.08
23649.79	-18228.4	-191.1	96162	19.82	82.1	9.54	9.37
23650.79	-18228.3	-191.1	96162	19.61	62.5	5.11	9.03
23662.72	-18227.1	-191.1	96162	17.14	184	7.94	5.42
23654.77	-18227.9	-191.1	96162	13.65	50.8	3.68	3.91
23663.72	-18227	-191.1	96162	13.3	949	23.9	3.5
23657.75	-18227.6	-191.1	96162	12.5	32.5	1.5	1.93
23656.76	-18227.7	-191.1	96162	11.1	61.5	2.22	4.4
23655.76	-18227.8	-191.1	96162	9.75	19.7	1.22	2.16
23652.78	-18228.1	-191.1	96162	9.58	80.3	2.98	3.7
23653.77	-18228	-191.1	96162	8.62	44.5	1.87	8.34
23658.75	-18227.5	-191.1	96162	8.62	84.2	4.35	7.53
23651.78	-18228.2	-191.1	96162	6.17	49.2	2.77	9.1
23649.05	-18228.5	-191.1	96162	4.96	150	3.85	6.63
23648.3	-18228.6	-191.1	96162	2.58	75.35	1.93	3.34
23659.74	-18227.4	-191.1	96162	1.51	23.1	0.85	1.92
23664.71	-18226.9	-191.1	96162	1.37	52.4	1.56	0.67
23646.87	-18228.7	-208.47	96163	1.1	13.8	0.51	0.14
23690.36	-18292.4	-205	96164	25.78	87.32	3.98	2.64
23690.99	-18292.1	-204.29	96164	24.17	193.4	6.71	4.91
23689.72	-18292.7	-205.7	96164	21.19	112.6	5.14	6.41

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23691.63	-18291.8	-203.58	96164	18.07	211.5	6.83	8.57
23691.98	-18291.6	-203.19	96164	14.6	132	4.36	9.47
23688.44	-18293.3	-207.12	96164	11.41	194.58	5.94	5.95
23683.98	-18295.4	-212.07	96164	8.19	68.3	2.36	3.97
23687.81	-18293.6	-207.82	96164	5.76	137.06	4.19	3.32
23687.17	-18293.9	-208.53	96164	4.48	130.77	3.97	2.76
23684.62	-18295.1	-211.36	96164	3.28	20.06	0.88	2.83
23685.25	-18294.8	-210.65	96164	1.2	13.45	0.38	0.91
23682.81	-18296.3	-226.36	96165	22.63	9.2	0.4	0.69
23682.81	-18296.3	-218.36	96165	11.25	9	0.18	1.3
23682.81	-18296.3	-221.36	96165	10.29	30.5	1.28	1.6
23682.81	-18296.3	-217.36	96165	9.33	39.2	1.39	2.61
23682.81	-18296.3	-227.36	96165	8.92	-999	-999	-999
23682.81	-18296.3	-222.36	96165	5.21	4.1	0.08	0.12
23682.81	-18296.3	-216.36	96165	4.94	11	0.29	1.18
23682.81	-18296.3	-225.36	96165	4.51	3.9	0.07	0.24
23682.81	-18296.3	-220.36	96165	4.49	29.8	2.34	1.63
23682.81	-18296.3	-228.36	96165	3.39	2.7	0.18	0.46
23682.81	-18296.3	-223.36	96165	1.51	1.6	0.05	0.08
23682.81	-18296.3	-224.36	96165	1.2	1.3	0.03	0.06
23682.81	-18296.3	-203.11	96166	15.24	72.9	2.2	2.87
23682.81	-18296.3	-203.76	96166	12.89	132.45	3.47	4.01
23682.81	-18296.3	-210.76	96166	7.79	22.95	1.12	3.42
23682.81	-18296.3	-211.76	96166	6.36	64.8	2.28	2.84
23682.81	-18296.3	-204.76	96166	4.52	63.27	1.61	2.21
23682.81	-18296.3	-208.76	96166	2.49	21.2	0.6	1.42
23682.81	-18296.3	-206.76	96166	1.27	4.75	0.27	0.65
23626.55	-18230.8	-181.84	96167	19	94.2	6.31	10
23626.55	-18230.8	-180.84	96167	17	222	6.9	3.1
23626.55	-18230.8	-183.84	96167	4.52	31.2	1.6	2.21
23626.55	-18230.8	-182.84	96167	1.11	15.6	0.49	0.25
23684.15	-18328.3	-215.43	96168	36	150.5	5.54	2.88
23683.4	-18329	-215.43	96168	36	150.5	5.54	2.88
23682.65	-18329.7	-215.43	96168	30	113	3.8	0.59
23672.91	-18338.3	-215.43	96168	23.4	16.2	0.51	2.22
23670.67	-18340.3	-215.43	96168	21.2	205.35	5.73	4.73
23672.17	-18338.9	-215.43	96168	20.5	67.5	2.64	5.36
23684.9	-18327.7	-215.43	96168	20.4	346	11.1	4.7
23671.42	-18339.6	-215.43	96168	18.6	253	6.54	16
23675.16	-18336.3	-215.43	96168	17.8	66.3	1.73	10.8
23685.65	-18327	-215.43	96168	17.4	574	17.6	0.82
23669.92	-18340.9	-215.43	96168	16.1	220.25	6.93	1.85
23681.9	-18330.3	-215.43	96168	15.8	331	11	1.54

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23669.21	-18341.5	-215.43	96168	12.42	114.5	2.93	1.94
23681.15	-18331	-215.43	96168	11.73	471.5	14.7	6.32
23678.91	-18333	-215.43	96168	11.7	147.5	4.79	7.68
23679.65	-18332.3	-215.43	96168	11.22	170.92	5.57	8.12
23674.41	-18336.9	-215.43	96168	10.8	31.5	1.1	5.84
23680.4	-18331.6	-215.43	96168	8.24	450	13.93	10.7
23673.66	-18337.6	-215.43	96168	7.13	14.3	0.33	0.86
23666.25	-18344.2	-215.43	96168	1.32	10.8	0.17	0.63
23710.36	-18301.2	-247.88	96172	43.4	101	2.94	2.1
23712.1	-18299.3	-250.94	96172	35.2	29.7	0.58	1.73
23711.66	-18299.8	-250.18	96172	33.6	15	0.51	2.83
23710.79	-18300.7	-248.64	96172	33.5	31.2	1.54	0.47
23711.23	-18300.3	-249.41	96172	26.1	22.8	1.39	1.14
23712.54	-18298.9	-251.71	96172	19	126	4.63	15.8
23703.83	-18308.3	-236.39	96172	11.4	227	4.96	22.7
23708.18	-18303.6	-244.05	96172	10.7	13.4	1.49	4.24
23709.05	-18302.6	-245.58	96172	10.4	11.4	0.75	3.42
23702.52	-18309.7	-234.09	96172	9.45	316	8.69	22.8
23694.47	-18318.5	-219.92	96172	9.44	179.5	6.03	8.49
23703.39	-18308.8	-235.62	96172	9.34	399	7.89	29
23707.31	-18304.5	-242.52	96172	9.25	20	0.35	8.02
23712.97	-18298.4	-252.47	96172	7.42	182	6.46	3.32
23702.96	-18309.3	-234.86	96172	7.08	188	5.71	14.1
23706.01	-18305.9	-240.22	96172	7	23.5	0.96	8.52
23705.57	-18306.4	-239.45	96172	6.95	23.6	1.85	15.1
23709.92	-18301.7	-247.11	96172	6.82	9	1.46	0.71
23706.88	-18305	-241.75	96172	6.62	10.5	0.48	2.3
23706.44	-18305.5	-240.98	96172	6.16	17.2	1.1	5.65
23695.78	-18317.1	-222.22	96172	6.02	460	11.7	14.5
23702.09	-18310.2	-233.32	96172	5.89	-999	1.22	1.15
23707.75	-18304.1	-243.28	96172	5.82	8.4	0.15	2.15
23708.62	-18303.1	-244.81	96172	4.79	12.5	0.44	1.51
23695.34	-18317.5	-221.45	96172	4.59	350	11.3	13.8
23714.28	-18297	-254.77	96172	4.39	11.7	0.51	1.68
23709.49	-18302.2	-246.35	96172	4.15	4.8	0.14	0.29
23713.41	-18297.9	-253.24	96172	3.5	35.4	2.09	2.92
23705.13	-18306.9	-238.69	96172	3.38	24.43	1.48	5.07
23716.02	-18295.1	-257.84	96172	3.08	1.8	0.05	0.21
23704.7	-18307.4	-237.92	96172	2.82	78.65	2.11	5.85
23713.84	-18297.4	-254.01	96172	2.59	21	1.65	1.32
23714.71	-18296.5	-255.54	96172	2.4	8.1	0.16	0.37
23716.45	-18294.6	-258.6	96172	2.31	2.7	0.12	0.48
23701.22	-18311.1	-231.79	96172	2.02	3.9	0.15	0.37

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23716.89	-18294.1	-259.37	96172	1.54	3.6	0.18	0.75
23704.26	-18307.8	-237.15	96172	1.16	5.6	0.19	0.35
23715.15	-18296	-256.3	96172	1.05	3.6	0.12	0.36
23694.9	-18318	-220.68	96172	1.01	85.84	2.46	2.97
23696.19	-18318.6	-215.35	96174	6.94	433	13.5	14.28
23693.57	-18320.1	-215.35	96174	5.41	400	11	10.9
23691.31	-18321.4	-221.76	96176	8.85	400	13.2	7.41
23691.31	-18321.4	-221.01	96176	4.7	206	6.84	4.14
23693.23	-18320.3	-213.58	96177	6.3	130	5.1	7.32
23695.68	-18349.5	-215.63	96179	16.68	37.8	1.16	3.13
23694.69	-18349.4	-215.63	96179	16.59	15.9	0.56	6.63
23693.7	-18349.3	-215.63	96179	13.14	45.7	1.54	3.7
23698.41	-18349.9	-215.63	96179	11.16	166	4.24	14.4
23697.66	-18349.8	-215.63	96179	9.96	37.8	1.21	13.7
23692.71	-18349.1	-215.63	96179	5.13	60	1.93	8.07
23690.73	-18348.8	-215.63	96179	3.24	196	6.32	12.1
23691.72	-18349	-215.63	96179	2.79	174	5.69	4.79
23640.18	-18264.8	-191.16	96181	2.39	-999	-999	-999
23649.14	-18264	-191.16	96181	2.18	86.3	4.2	1.76
23648.14	-18264.1	-191.16	96181	1.37	63.45	2.24	1.03
23646.15	-18264.2	-191.16	96181	1.25	2.95	0.09	0.06
23647.15	-18264.2	-191.16	96181	1.14	3.7	0.07	0.05
23650.13	-18263.9	-191.16	96181	1.11	25.8	2.01	0.99
23687.27	-18348.8	-212.56	96183	5.52	19.8	0.62	0.16
23694.75	-18350.1	-208.67	96184	3.65	58.8	2.13	1.06
23694	-18349.9	-209.31	96184	2.71	30.96	1.12	1.01
23695.5	-18350.2	-208.03	96184	1.23	43.62	1.45	0.72
23659.17	-18229	-214.24	96186	18.35	747	19	4.99
23658.84	-18228	-214.24	96186	17.45	571.5	14.31	6.8
23659.49	-18229.9	-214.24	96186	12.08	552.5	13.69	5.39
23663.7	-18242.2	-214.24	96186	9.76	14.1	0.86	2.3
23658.52	-18227.1	-214.24	96186	8.93	179.05	4.47	5.02
23663.38	-18241.3	-214.24	96186	4.26	7.5	0.47	1.2
23659.82	-18230.8	-214.24	96186	3.42	209.8	4.91	2.66
23661.44	-18235.6	-214.24	96186	3.02	12.45	0.46	1.58
23662.73	-18239.4	-214.24	96186	2.84	-999	-999	-999
23661.11	-18234.6	-214.24	96186	2.06	10.5	0.38	1.47
23661.76	-18236.5	-214.24	96186	1.64	5.4	0.19	0.7
23664.35	-18244.1	-214.24	96186	1.41	0.9	0	0.01
23660.79	-18233.7	-214.24	96186	1.28	4.35	0.08	0.83
23657.22	-18223.3	-214.24	96186	1.23	9.9	0.14	0.33
23666.29	-18249.8	-214.24	96186	1.19	3.6	0.08	0.43
23651.07	-18205.3	-214.24	96186	1.13	1.8	0.03	0.03

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23656.52	-18200.5	-194.76	96188	20.95	43.75	1.62	0.94
23652.56	-18201	-194.76	96188	20.2	18.6	1.33	0.75
23657.51	-18200.4	-194.76	96188	18.6	79.5	1.32	0.07
23655.53	-18200.6	-194.76	96188	16.8	24.75	1.69	2.12
23653.55	-18200.9	-194.76	96188	15.5	25.5	1.36	0.66
23654.54	-18200.8	-194.76	96188	15.3	19.5	1.17	2.43
23658.25	-18200.2	-194.76	96188	13.6	101.5	1.61	0.08
23660.98	-18199.9	-194.76	96188	4.62	8.7	0.44	1.14
23659	-18200.1	-194.76	96188	3.51	9.9	0.48	0.15
23668.9	-18198.8	-194.76	96188	2.32	16.8	0.34	0.41
23664.94	-18199.3	-194.76	96188	1.93	2.1	0.12	0.56
23693.66	-18195.3	-194.76	96188	1.67	3	0.02	0.06
23694.4	-18195.2	-194.76	96188	1.67	3	0.02	0.06
23650.58	-18201.3	-194.76	96188	1.07	0.6	0.01	0.01
23661.97	-18199.7	-194.76	96188	1.04	6.9	0.31	0.75
23674.07	-18224.5	-214.21	96189	23.3	204.25	5.44	6.68
23684.29	-18159.3	-214.21	96189	21.6	6.9	0.44	0.87
23673.91	-18225.5	-214.21	96189	15.1	317.25	6.82	2.77
23674.22	-18223.5	-214.21	96189	14.65	194.65	5.26	5.85
23684.14	-18160.3	-214.21	96189	12.09	419.45	0.61	0.71
23675.31	-18216.6	-214.21	96189	8.49	20.85	0.55	4.77
23683.98	-18161.3	-214.21	96189	8.48	560	1.33	2.22
23683.83	-18162.2	-214.21	96189	7.91	147.15	0.99	2.13
23683.52	-18164.2	-214.21	96189	7.59	30.3	0.94	1.5
23678.25	-18197.8	-214.21	96189	7.32	4.8	0.18	0.54
23683.36	-18165.2	-214.21	96189	7.2	58.2	1.2	2.38
23678.1	-18198.8	-214.21	96189	6.24	4.5	0.16	0.43
23675.15	-18217.6	-214.21	96189	5.49	17.25	0.44	4.47
23673.76	-18226.5	-214.21	96189	5.45	299.85	6.38	0.89
23683.67	-18163.2	-214.21	96189	3.76	7.05	0.1	0.37
23675.46	-18215.6	-214.21	96189	3.64	5.7	0.19	0.63
23683.21	-18166.2	-214.21	96189	3.63	41.7	0.46	1.16
23674.69	-18220.5	-214.21	96189	2.92	14.55	0.99	1.38
23674.53	-18221.5	-214.21	96189	2.57	9.75	0.52	1.34
23678.41	-18196.8	-214.21	96189	2.23	5.4	0.1	0.45
23674.38	-18222.5	-214.21	96189	1.96	13.2	0.52	1.83
23678.87	-18193.9	-214.21	96189	1.94	5.25	0.09	0.24
23678.72	-18194.8	-214.21	96189	1.77	5.7	0.12	0.39
23674.84	-18219.5	-214.21	96189	1.54	12.9	0.8	1.3
23683.05	-18167.2	-214.21	96189	1.53	18.3	0.48	0.14
23680.57	-18183	-214.21	96189	1.37	7.2	0.17	0.32
23682.28	-18172.1	-214.21	96189	1.24	3.75	0.16	0.01
23680.11	-18186	-214.21	96189	1.2	3.9	0.08	0.34

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23682.12	-18173.1	-214.21	96189	1.15	3.75	0.16	0.02
23680.42	-18184	-214.21	96189	1.14	8.85	0.16	0.34
23675	-18218.6	-214.21	96189	1.05	5.4	0.15	0.67
23633.14	-18203.8	-204.47	96191	2.02	3.1	0.16	0.58
23633.14	-18203.8	-205.47	96191	1.8	3.2	0.12	0.29
23710.03	-18432.7	-222.29	96194	22.53	67.9	2.12	2.12
23710.03	-18432.7	-224.29	96194	13.35	74.9	2.47	1.42
23710.03	-18432.7	-221.29	96194	8.19	48.9	4.66	4.57
23710.03	-18432.7	-223.29	96194	6.94	34.19	1.21	2.93
23710.03	-18432.7	-228.79	96194	6.66	17	0.57	0.92
23710.03	-18432.7	-218.29	96194	5.98	14.12	0.48	0.87
23710.03	-18432.7	-220.29	96194	4.53	67.5	2.89	2.34
23710.03	-18432.7	-227.79	96194	2.49	58.8	1.89	1.97
23710.03	-18432.7	-229.79	96194	1.53	2.7	0.11	0.1
23704.66	-18436.3	-216.52	96196	12.4	130	4.79	6.33
23697.9	-18438.1	-216.52	96196	9.62	154.5	5.62	11.9
23700.8	-18437.3	-216.52	96196	7.54	212.5	7.81	9.48
23701.76	-18437.1	-216.52	96196	6.53	230.5	8.64	12.82
23696.26	-18438.6	-216.52	96196	6.34	134	5.3	20.3
23699.83	-18437.6	-216.52	96196	6.24	187.75	6.74	10.69
23703.69	-18436.5	-216.52	96196	5.14	375	14.1	19.3
23698.87	-18437.9	-216.52	96196	1.33	30.66	0.98	2.5
23713.67	-18430.2	-219.29	96198	1.11	48.8	1.87	4.14
23728.47	-18451.8	-216.78	96199	17.6	171	5.67	3.03
23729.41	-18451.5	-216.78	96199	10.7	150	5.2	0.05
23730.36	-18451.2	-216.78	96199	10.21	178	6.28	0.05
23726.71	-18452.4	-216.78	96199	1.52	18	0.67	0.76
23728.03	-18454.6	-214.09	97001	3.77	2.1	0.01	0.01
23714.57	-18400.6	-233.33	97004	49.9	147.5	4.27	2.24
23715.17	-18400.2	-234.04	97004	16.73	55.58	1.7	0.67
23719.91	-18397.1	-239.69	97004	15.1	53.2	1.55	3
23720.5	-18396.7	-240.4	97004	9.62	62.8	2.52	1.18
23721.1	-18396.4	-241.11	97004	5.59	181.5	5.69	19
23725.84	-18393.3	-246.76	97004	5.21	399	10	8.75
23718.72	-18397.9	-238.28	97004	3.42	6.9	0.23	0.08
23724.65	-18394	-245.35	97004	3.37	306	6.52	12.2
23728.21	-18391.7	-249.59	97004	2.58	102.5	1.78	3.86
23726.43	-18392.9	-247.47	97004	2.51	106	3.46	0.62
23727.03	-18392.5	-248.18	97004	2.51	106	3.46	0.62
23723.47	-18394.8	-243.94	97004	2.5	154	5.35	18
23729.1	-18391.2	-250.65	97004	1.36	9	0.26	0.78
23721.69	-18396	-241.82	97004	1.04	10.1	0.5	4.07
23700.17	-18410.2	-218.18	97005	11.5	-999	-999	-999

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23700.17	-18410.2	-219.18	97005	6.35	182.5	6.74	6.33
23700.17	-18410.2	-224.18	97005	4.18	16.5	0.65	0.86
23700.17	-18410.2	-220.18	97005	3.7	88.5	2.74	2.3
23700.17	-18410.2	-222.18	97005	1.19	4.5	0.19	0.34
23698.55	-18411.6	-216.48	97008	7.08	37.9	1.41	2
23690.65	-18417.2	-216.48	97008	7.05	202	7.11	6.18
23689.83	-18417.8	-216.48	97008	6.43	228.4	7.98	10.84
23696.11	-18413.4	-216.48	97008	3.57	14.9	0.52	0.81
23692.85	-18415.7	-216.48	97008	3.15	66.7	2.72	3.45
23693.66	-18415.1	-216.48	97008	2.9	304.85	5.66	6.11
23689.1	-18418.3	-216.48	97008	2.64	186	6.77	15.2
23692.03	-18416.2	-216.48	97008	2.55	12.8	0.53	0.86
23696.92	-18412.8	-216.48	97008	2.25	120	3.99	7.61
23697.74	-18412.2	-216.48	97008	2.22	17.6	0.69	1.14
23694.48	-18414.5	-216.48	97008	1.74	183.13	3.4	3.67
23704.22	-18372.7	-216.59	97009	6.21	158	5.23	15.5
23699.92	-18376.3	-216.59	97009	6.12	7.5	0.3	1.17
23705.76	-18371.4	-216.59	97009	5.25	353.5	12.2	14.7
23706.53	-18370.8	-216.59	97009	4.89	129.7	4.02	5.39
23704.99	-18372.1	-216.59	97009	3.93	219	7.28	12.8
23710.52	-18367.4	-216.59	97009	3.12	37.52	1.18	0.95
23703.46	-18373.3	-216.59	97009	2.31	208	7.44	10.3
23713.59	-18364.9	-216.59	97009	2.25	33.2	1.05	0.82
23711.29	-18366.8	-216.59	97009	1.95	20.4	0.64	0.93
23701.92	-18374.6	-216.59	97009	1.8	42.3	1.88	2.09
23702.69	-18374	-216.59	97009	1.05	22.2	0.75	0.83
23696.78	-18378.3	-233.84	97010	24.12	71	1.35	6.84
23696.25	-18378.7	-233.14	97010	14.55	24.7	0.75	9.63
23690.95	-18383.4	-226.07	97010	6.84	2.2	0.07	0.13
23691.48	-18382.9	-226.77	97010	2.31	2.4	0.07	0.16
23692.54	-18382	-228.19	97010	1.71	3.7	0.05	0.21
23695.72	-18379.2	-232.43	97010	1.2	38.4	1.39	9.86
23693.07	-18381.5	-228.89	97010	1.11	3.3	0.11	0.67
23675.5	-18170.7	-194.78	97014	14	60.3	1.38	0.47
23674.5	-18170.6	-194.78	97014	7.43	99.88	0.92	1.43
23680.49	-18171	-194.78	97014	7.26	6.8	0.27	0.16
23679.49	-18171	-194.78	97014	4.23	138.5	2.1	0.29
23676.5	-18170.8	-194.78	97014	3.39	8.1	0.53	0.44
23677.5	-18170.8	-194.78	97014	3.01	6.3	0.09	2.26
23678.49	-18170.9	-194.78	97014	3.01	27	0.35	0.09
23654.55	-18169.2	-194.78	97014	2.47	31.8	0.23	0.47
23648.57	-18168.8	-194.78	97014	2.32	5.7	0.1	0.02
23664.53	-18169.9	-194.78	97014	2.23	3.7	0.03	0.01

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23653.55	-18169.2	-194.78	97014	1.09	4	0.07	0.17
23641.42	-18168.5	-203.4	97015	3.16	6.3	0.03	0.11
23641.42	-18168.5	-202.4	97015	1.19	2.4	0.05	0.12
23640.77	-18157.4	-194.35	97016	12.8	46.8	0.5	2.9
23640.35	-18156.8	-194.35	97016	12.8	46.8	0.5	2.9
23641.33	-18158.3	-194.35	97016	1.92	5.9	0.06	0.55
23641.89	-18159.1	-194.35	97016	1.54	8.9	0.19	0.63
23643.08	-18160.9	-200.6	97017	37.1	43.2	0.28	4.02
23643.08	-18160.9	-207.6	97017	19.6	3.9	0.05	0.11
23643.08	-18160.9	-199.6	97017	7.79	5.7	0.65	0.3
23643.08	-18160.9	-202.6	97017	7.77	4.2	0.06	0.54
23643.08	-18160.9	-203.6	97017	5.67	6.3	0.06	0.67
23643.08	-18160.9	-198.6	97017	5.65	2.3	0.07	0.44
23643.08	-18160.9	-197.6	97017	3.81	1.4	0.05	0.18
23643.08	-18160.9	-208.6	97017	3.36	7.8	0.11	0.57
23643.08	-18160.9	-201.6	97017	2.8	2.7	0.05	0.6
23643.08	-18160.9	-196.85	97017	2.65	3	0.03	0.1
23643.08	-18160.9	-209.6	97017	1.98	2.4	0.04	0.14
23643.08	-18160.9	-210.6	97017	1.34	2.1	0.03	0.08
23643.08	-18160.9	-206.6	97017	1.23	1.5	0.04	0.47
23646.7	-18153.8	-212.62	97019	24.2	60.9	4.65	4.64
23646.7	-18153.8	-210.62	97019	19.3	69	5.03	9.2
23646.7	-18153.8	-208.62	97019	19.2	39.6	3.5	8.19
23646.7	-18153.8	-211.62	97019	18.8	45.3	3.96	10.6
23646.7	-18153.8	-209.62	97019	10.9	45.6	2.11	4.13
23646.7	-18153.8	-206.12	97019	5.99	7.5	0.07	0.24
23646.7	-18153.8	-196.12	97019	4.33	-999	0.95	0.93
23646.7	-18153.8	-197.12	97019	4.33	-999	0.95	0.93
23646.7	-18153.8	-205.12	97019	2.84	3.6	0.04	0.12
23646.7	-18153.8	-202.12	97019	2.79	3.3	0.06	0.14
23646.7	-18153.8	-203.12	97019	2.52	2.4	0.06	0.13
23646.7	-18153.8	-204.12	97019	1.5	2.4	0.05	0.18
23646.7	-18153.8	-201.12	97019	1.27	4.8	0.04	0.09
23646.7	-18153.8	-207.12	97019	1.06	2.4	0.07	0.18
23674.67	-18394.4	-193.92	97020	17	58.2	2.02	4.9
23676.74	-18395	-193.94	97021	9.66	62.7	1.89	15.2
23678.27	-18394.4	-193.94	97021	1.82	0.2	0.03	0.04
23621.8	-18299	-182.16	97023	18.63	54	1.58	5.11
23623.71	-18299.6	-182.16	97023	17.3	32.08	0.66	15.22
23627.53	-18300.8	-182.16	97023	16.44	26.35	0.77	7.26
23622.75	-18299.3	-182.16	97023	15.75	71.5	1.89	13.8
23624.66	-18299.9	-182.16	97023	15.52	17.7	0.4	9.42
23628.48	-18301.1	-182.16	97023	14.13	51.95	1.43	8.56

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23626.57	-18300.5	-182.16	97023	12.96	7.95	0.22	1.87
23625.62	-18300.2	-182.16	97023	12.82	8.55	0.25	3.03
23620.84	-18298.7	-182.16	97023	11.61	153	3.78	14
23629.44	-18301.4	-182.16	97023	6.12	39.05	1.12	1.88
23630.39	-18301.7	-182.16	97023	4.64	9.32	0.37	0.1
23631.35	-18302	-182.16	97023	3.87	163	4.26	10.4
23631.92	-18302.2	-182.16	97023	3.87	163	4.26	10.4
23617.98	-18297.9	-182.16	97023	3.69	17.8	0.66	4.38
23633.45	-18302.7	-182.16	97023	1.86	14	0.71	1.2
23634.4	-18303	-182.16	97023	1.86	14	0.71	1.2
23647.01	-18219.4	-179.8	97024	37.2	69.6	2.54	5.55
23646.35	-18220.1	-179.8	97024	35.6	17.1	0.54	2.06
23644.36	-18222.3	-179.8	97024	34	15.6	0.4	6.72
23652.32	-18213.4	-179.8	97024	25.4	198.5	6.7	6.5
23647.67	-18218.6	-179.8	97024	24.4	165.5	6.84	0.79
23643.69	-18223.1	-179.8	97024	23.9	38.1	1.11	11.6
23648.34	-18217.9	-179.8	97024	23	55.9	1.84	4.5
23649.66	-18216.4	-179.8	97024	21	216	5.54	9.18
23641.71	-18225.3	-179.8	97024	18.9	17.7	0.46	13.3
23645.02	-18221.6	-179.8	97024	17.01	13.75	0.41	0.71
23649	-18217.1	-179.8	97024	15	314	8.21	3.45
23652.98	-18212.6	-179.8	97024	13.1	261	7.78	11.1
23643.03	-18223.8	-179.8	97024	12.2	227	7.16	22.8
23651.65	-18214.1	-179.8	97024	12.1	542	16.2	6.55
23642.37	-18224.6	-179.8	97024	11.5	195	5.96	16.7
23637.06	-18230.6	-179.8	97024	11.3	123	4.12	8.77
23639.05	-18228.3	-179.8	97024	11.3	493	9.67	9.27
23640.38	-18226.8	-179.8	97024	10.9	385	11.8	14.4
23650.99	-18214.9	-179.8	97024	10.7	607	17.2	14.6
23650.33	-18215.6	-179.8	97024	10.4	371	11.2	6.22
23641.04	-18226.1	-179.8	97024	8.11	246	3.75	23.4
23639.72	-18227.6	-179.8	97024	7.63	807	24.9	5.13
23637.73	-18229.8	-179.8	97024	5.53	300	9.65	2.11
23645.68	-18220.9	-179.8	97024	5.19	103.05	2.61	4.45
23638.39	-18229.1	-179.8	97024	5.03	255	7.4	3.02
23636.47	-18231.3	-179.8	97024	2.02	1.7	0.06	0.04
23638.72	-18241.7	-179.77	97025	12.3	693.5	20.7	4.81
23634.78	-18242.4	-179.77	97025	12	610	16.6	12.5
23640.69	-18241.4	-179.77	97025	9.68	834	23.8	2.77
23639.7	-18241.6	-179.77	97025	8.93	1120.5	31.9	3.95
23637.73	-18241.9	-179.77	97025	6.82	221.4	7.14	2.12
23641.67	-18241.2	-179.77	97025	6.63	228.2	7.03	1.77
23636.75	-18242.1	-179.77	97025	4.66	182.9	4.94	3.07

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23625.23	-18244.7	-175.31	97026	15.69	129	4.32	8.1
23625.23	-18244.7	-171.31	97026	1.59	79.9	2.57	1.58
23626.3	-18274	-181.21	97027	4.32	18.8	0.52	0.07
23627.15	-18274.5	-181.21	97027	2.72	12.05	0.33	0.05
23623.75	-18272.4	-181.21	97027	2.07	30.3	1.08	0.33
23622.9	-18271.8	-181.21	97027	1.2	12.3	0.31	0.54
23731.93	-18522.4	-179.17	97030	8.78	478	17.6	6.75
23732.62	-18523.1	-179.17	97030	7.95	218	5.89	16.4
23773.8	-18565.6	-179.17	97030	7.12	315.4	12.56	19.76
23733.32	-18523.8	-179.17	97030	6.01	283	5.6	4.84
23734.02	-18524.5	-179.17	97030	6.01	795	26.4	1.52
23730.54	-18520.9	-179.17	97030	5.99	465.05	16.95	8.23
23734.71	-18525.2	-179.17	97030	4.05	767	24.3	3.79
23775.19	-18567.1	-179.17	97030	3.62	-999	13.21	18.15
23735.41	-18526	-179.17	97030	3.04	990	33.7	9.39
23735.82	-18526.4	-179.17	97030	3.04	990	33.7	9.39
23731.23	-18521.6	-179.17	97030	1.81	150.5	2.11	9.33
23776.58	-18568.5	-179.17	97030	1.65	299.6	13.5	12.02
23775.89	-18567.8	-179.17	97030	1.4	245	11.4	12.3
23778.67	-18570.6	-179.17	97030	1.36	154	7.46	8.69
23780.76	-18572.8	-179.17	97030	1.33	92.58	4.3	5.19
23777.28	-18569.2	-179.17	97030	1.03	307	13.93	19.5
23734.11	-18527.1	-179.17	97031	10.9	515	10.84	12.56
23733.56	-18526.2	-179.17	97031	10.83	410.88	15.94	9.16
23734.66	-18527.9	-179.17	97031	10.8	987	8.43	9.65
23735.21	-18528.7	-179.17	97031	10.02	887	10.19	7.35
23733.01	-18525.4	-179.17	97031	8.56	348.15	15.11	15.68
23737.96	-18532.9	-179.17	97031	8.26	331	10.14	19.17
23735.76	-18529.6	-179.17	97031	7.05	370	10.01	21.3
23740.11	-18536.2	-179.17	97031	6.97	-999	14.88	17.5
23739.06	-18534.6	-179.17	97031	6.65	-999	12.02	21.9
23732.46	-18524.6	-179.17	97031	6.62	486	11.6	7.48
23736.31	-18530.4	-179.17	97031	6.59	334.86	7.4	26
23736.86	-18531.2	-179.17	97031	5.96	298	7.5	28.2
23738.51	-18533.7	-179.17	97031	5.88	-999	10.51	22.52
23739.61	-18535.4	-179.17	97031	5.46	-999	30.95	14.6
23731.36	-18522.9	-179.17	97031	5.4	240	2.28	13.1
23737.41	-18532.1	-179.17	97031	5.32	354	11.2	25.6
23730.26	-18521.2	-179.17	97031	3.2	136	4.51	28.1
23730.81	-18522	-179.17	97031	2.38	77.4	3.03	31.9
23731.91	-18523.7	-179.17	97031	2.06	113	4.06	13.7
23730.12	-18522.5	-179.16	97032	14.16	208	6.82	1.94
23730.43	-18523.4	-179.16	97032	8.61	229	6.3	10.5

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23730.74	-18524.4	-179.16	97032	6	178	6.28	6.89
23731.05	-18525.3	-179.16	97032	5.76	669.5	14.8	0.88
23731.36	-18526.3	-179.16	97032	5.16	821	27.3	0.97
23731.67	-18527.2	-179.16	97032	4.74	908.5	29	0.41
23731.23	-18520.5	-179.17	97033	9.72	590.5	20	7.37
23732.07	-18520.9	-179.17	97033	4.23	565.5	20.9	19.8
23715.6	-18494.6	-179.92	97034	8.14	640	11.3	5.49
23712.62	-18497	-179.92	97034	4.45	235	6.31	19.9
23701.44	-18475.3	-179.46	97035	1.91	44.1	1.86	5.28
23708.99	-18465.4	-179.56	97037	6.33	137	4.64	6.46
23709.68	-18464.7	-179.56	97037	6.33	137	4.64	6.46
23690.16	-18454.4	-182.87	97039	8.73	173	4.83	11.5
23692.42	-18452.4	-182.87	97039	5.85	127	4.27	14.7
23691.67	-18453.1	-182.87	97039	5.85	127	4.27	14.7
23689.41	-18455.1	-182.87	97039	5.43	97.63	2.95	7.04
23662.44	-18387.6	-185.23	97042	16.07	105.64	3.64	2.77
23661.88	-18388.1	-185.23	97042	1.71	3.1	0.14	0.22
23649.72	-18372.1	-184.62	97043	7.86	186	5.92	12.1
23650.57	-18371.6	-184.62	97043	6.58	297	9.37	15.76
23653.95	-18369.5	-184.62	97043	6.33	393	11.6	15.7
23653.1	-18370	-184.62	97043	6.15	162	5	11.7
23654.8	-18368.9	-184.62	97043	3.96	415.5	12.3	21.7
23652.26	-18370.5	-184.62	97043	3.69	522	13.7	8.9
23651.41	-18371.1	-184.62	97043	3.39	574.5	18	24.9
23657.33	-18367.3	-184.62	97043	2.19	291	9.18	16.4
23656.49	-18367.9	-184.62	97043	2.1	269	8.38	8.82
23655.64	-18368.4	-184.62	97043	1.74	17.5	0.73	1.81
23648.87	-18372.7	-184.62	97043	1.2	41.4	1.6	3.02
23649.24	-18162.4	-176.16	97046	6.15	34.8	2.74	0.44
23649.24	-18162.4	-174.16	97046	3.72	63.2	1.92	0.46
23649.24	-18162.4	-164.16	97046	2.49	29.9	0.49	2.46
23649.24	-18162.4	-163.16	97046	2.46	91.7	1.68	11.5
23649.24	-18162.4	-173.16	97046	2.4	72.3	2.56	1.54
23649.24	-18162.4	-159.16	97046	1.92	30.1	0.98	1.53
23649.24	-18162.4	-179.16	97046	1.17	10	0.39	0.33
23657.43	-18221.3	-186.4	97047	14	250	5.69	3.04
23658.35	-18221.7	-186.4	97047	13	204	6.31	9.18
23656.51	-18220.9	-186.4	97047	10.7	332	11.2	4.83
23659.26	-18222.1	-186.4	97047	10.4	365	10.9	13.7
23653.15	-18194.1	-186.39	97049	27	80.1	4.32	0.4
23665.18	-18210.1	-186.39	97049	24	96.6	2.32	0.53
23664.58	-18209.3	-186.39	97049	18.9	287	6.44	5.86
23654.96	-18196.5	-186.39	97049	17.28	12.5	0.66	1.7

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23647.14	-18186.1	-186.39	97049	17.1	23.85	1.01	4.09
23646.53	-18185.3	-186.39	97049	17.05	27.45	1.54	4.84
23645.33	-18183.7	-186.39	97049	15.45	51.15	2.7	4.3
23645.93	-18184.5	-186.39	97049	13.9	30.75	1.78	4.68
23653.75	-18194.9	-186.39	97049	13	102	2.25	4.65
23644.73	-18182.9	-186.39	97049	12.23	48.51	2.52	2.1
23649.54	-18189.3	-186.39	97049	10.67	33.45	1.39	0.46
23647.74	-18186.9	-186.39	97049	10.43	12.15	0.25	1
23655.56	-18197.3	-186.39	97049	9.72	64.2	2.75	3.63
23650.14	-18190.1	-186.39	97049	9.65	37.2	1.65	0.82
23663.98	-18208.5	-186.39	97049	8.68	132.5	3.28	4.42
23662.17	-18206.1	-186.39	97049	8.14	904	24.9	2.88
23661.57	-18205.3	-186.39	97049	7.27	11.1	0.7	1.24
23648.34	-18187.7	-186.39	97049	6.63	10.5	0.17	0.09
23663.38	-18207.7	-186.39	97049	6.63	142.5	4.98	5.72
23648.94	-18188.5	-186.39	97049	5.92	14.4	0.41	0.09
23654.35	-18195.7	-186.39	97049	4.72	28.8	1.48	5.34
23656.16	-18198.1	-186.39	97049	4.65	27.8	0.34	0.66
23662.78	-18206.9	-186.39	97049	4.55	34.8	1.9	1.99
23650.75	-18190.9	-186.39	97049	4.5	25.8	1.19	0.85
23651.35	-18191.7	-186.39	97049	3.96	37.2	0.67	0.22
23658.57	-18201.3	-186.39	97049	3.28	18.6	0.71	10.5
23644.13	-18182.1	-186.39	97049	3.07	15.3	0.78	0.75
23657.36	-18199.7	-186.39	97049	2.44	4.5	0.17	0.49
23659.17	-18202.1	-186.39	97049	1.33	2.4	0.16	0.53
23668.83	-18256.4	-186.3	97050	26.6	21.6	0.69	3.12
23646.83	-18256.7	-186.3	97050	26.3	366	11.8	5.08
23665.83	-18256.5	-186.3	97050	20.3	10.2	0.23	7.41
23670.83	-18256.4	-186.3	97050	20.2	166	4.82	9.12
23667.83	-18256.4	-186.3	97050	17.4	129	3.84	10.1
23672.63	-18256.4	-186.3	97050	15.3	136	4.02	5.5
23671.83	-18256.4	-186.3	97050	14.5	273	8.21	11.2
23664.83	-18256.5	-186.3	97050	14.4	102	3.03	15.1
23669.83	-18256.4	-186.3	97050	14.2	163.5	4.67	5.36
23647.83	-18256.7	-186.3	97050	11.8	356	10.3	5.1
23661.83	-18256.5	-186.3	97050	9.87	404	12.6	4.75
23663.83	-18256.5	-186.3	97050	8.84	283	9.51	20.8
23666.83	-18256.4	-186.3	97050	8.71	250	7.61	14.4
23645.83	-18256.7	-186.3	97050	7.9	110.85	3.57	1.57
23648.83	-18256.7	-186.3	97050	7.14	73.8	2.28	19.4
23652.83	-18256.6	-186.3	97050	6.06	113.5	4.16	1.26
23644.83	-18256.7	-186.3	97050	5.93	8.15	0.2	0.28
23650.83	-18256.6	-186.3	97050	5.55	409	13	4.78

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23662.83	-18256.5	-186.3	97050	5.16	113.5	4.02	4.44
23659.83	-18256.5	-186.3	97050	4.91	359	12	4.86
23643.83	-18256.7	-186.3	97050	4.85	225	5.42	3.12
23649.83	-18256.6	-186.3	97050	4.82	156	3.34	23.1
23641.83	-18256.7	-186.3	97050	4.76	227	6.04	2.7
23640.83	-18256.8	-186.3	97050	2.14	62.8	2.07	3.27
23642.83	-18256.7	-186.3	97050	1.07	283	6.87	14.6
23633.38	-18227	-186.41	97051	25.12	113.46	5.21	2.64
23634.36	-18226.8	-186.41	97051	21	118.71	5.52	2.77
23636.32	-18226.4	-186.41	97051	8.29	115.26	3.13	2.85
23637.3	-18226.2	-186.41	97051	7.31	70.08	1.63	2.14
23628.49	-18228	-186.41	97051	7.15	43.5	2.3	2.69
23629.47	-18227.8	-186.41	97051	5.74	29.58	1.56	1.95
23635.34	-18226.6	-186.41	97051	5.66	60.02	1.77	1.28
23630.44	-18227.6	-186.41	97051	3.86	17.22	0.59	1.89
23631.42	-18227.4	-186.41	97051	2.53	18.08	0.49	2.08
23657.47	-18222	-186.41	97051	1.72	21.3	1.03	0.12
23614.13	-18246.5	-167.69	97052	22.65	50.5	1.46	1.42
23616.06	-18246	-167.69	97052	17.19	34.8	0.86	5.96
23621.69	-18244.4	-167.69	97052	16.1	9.9	0.26	2.73
23619.91	-18244.9	-167.69	97052	13.11	28.4	0.8	1.18
23618.94	-18245.2	-167.69	97052	12.42	23.8	0.62	10
23613.17	-18246.8	-167.69	97052	12.03	70	1.96	2.42
23608.36	-18248.1	-167.69	97052	11.64	9.2	0.22	0.18
23615.09	-18246.2	-167.69	97052	10.95	91.1	2.7	4.05
23617.98	-18245.4	-167.69	97052	10.83	13	0.3	8.61
23609.32	-18247.9	-167.69	97052	10.7	35.1	0.84	3.49
23620.87	-18244.6	-167.69	97052	8.58	38.7	0.94	4.69
23611.24	-18247.3	-167.69	97052	8.34	83.1	2.48	7.97
23610.28	-18247.6	-167.69	97052	8.1	18	0.46	2.48
23612.21	-18247.1	-167.69	97052	4.94	46.2	1.13	14.5
23617.02	-18245.7	-167.69	97052	3.45	11	0.28	0.36
23622.85	-18233.8	-167.71	97053	17.19	62.1	1.78	13.6
23612.39	-18241	-167.71	97053	16.8	34.4	0.85	18.1
23622.15	-18234.3	-167.71	97053	14.27	18.35	0.55	15.68
23611.77	-18241.4	-167.71	97053	11.46	57.15	1.59	24.25
23619.59	-18236	-167.71	97053	10.08	180.5	4.18	9.28
23609.3	-18243.1	-167.71	97053	9.84	29.65	0.73	2.31
23610.13	-18242.5	-167.71	97053	9.75	42.5	1.21	6.63
23620.42	-18235.4	-167.71	97053	6.54	105.6	2.86	8.23
23610.95	-18242	-167.71	97053	6.53	59	1.76	19.98
23613.01	-18240.6	-167.71	97053	6.51	85.1	1.96	24
23618.77	-18236.6	-167.71	97053	6.51	105.55	1.62	2.08

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23621.69	-18234.6	-167.71	97053	6.51	3.7	0.09	4.3
23613.83	-18240	-167.71	97053	5.64	104	1.35	11.3
23621.24	-18234.9	-167.71	97053	5.1	8.45	0.22	2.63
23608.48	-18243.7	-167.71	97053	4.89	7.45	0.14	0.54
23616.3	-18238.3	-167.71	97053	4.59	59.45	0.92	1.53
23617.12	-18237.7	-167.71	97053	4.05	49.8	0.4	0.83
23615.48	-18238.9	-167.71	97053	3.11	58.35	1.04	6.99
23617.95	-18237.1	-167.71	97053	2.91	49.75	0.22	1.13
23607.66	-18244.2	-167.71	97053	2.67	2.5	0.05	0.16
23614.65	-18239.4	-167.71	97053	1.93	16.64	0.32	3.7
23609.55	-18258.8	-167.92	97054	5.85	2	0.02	0.1
23610.3	-18258.8	-167.92	97054	5.85	2	0.02	0.1
23614.05	-18258.9	-167.92	97054	2.43	6.6	0.24	1.52
23617.14	-18270.9	-168.36	97055	3.24	43.9	1.61	3.46
23619.14	-18270.8	-168.26	97055	1.8	26.9	0.63	1
23618.14	-18270.9	-168.31	97055	1.19	9.79	0.31	0.69
23617.87	-18282.1	-168.4	97056	2.06	4.25	0.14	0.31
23618.87	-18282.2	-168.4	97056	1.53	9.65	0.41	0.63
23644.04	-18344.6	-168.04	97059	6.06	174	5.27	6.65
23644.58	-18342.9	-168.04	97059	5.43	442	15	19.4
23644.34	-18343.6	-168.04	97059	3.81	357	11.1	22
23643.74	-18345.5	-168.04	97059	2.49	422	13.4	13
23646.33	-18337.3	-168.04	97059	1.29	7.4	0.19	1.32
23636.12	-18059.2	-162.92	97062	29.23	109.3	4.13	10.53
23630.19	-18062.9	-162.92	97062	27.38	320.3	10.13	2.21
23631.04	-18062.4	-162.92	97062	21.58	342.4	9.26	2.82
23631.88	-18061.8	-162.92	97062	21.5	169	13.1	7.29
23627.65	-18064.5	-162.92	97062	19.66	505.1	3.6	2.6
23635.27	-18059.7	-162.92	97062	17.16	41.6	2.92	5.88
23626.8	-18065	-162.92	97062	17.1	473.5	2.03	3.1
23632.73	-18061.3	-162.92	97062	15.5	283	6.95	0.73
23633.58	-18060.8	-162.92	97062	13.32	242.93	5.96	0.71
23629.34	-18063.4	-162.92	97062	9.73	1019.9	8.44	1.8
23636.9	-18058.7	-162.92	97062	9.01	111	3.12	7.32
23628.5	-18064	-162.92	97062	5.45	466.7	6.28	0.76
23616.93	-18071.2	-162.92	97062	3.65	164	1.01	1.32
23617.78	-18070.7	-162.92	97062	3.01	10.8	0.13	0.45
23634.43	-18060.2	-162.92	97062	3	17.97	0.7	1.26
23616.08	-18071.7	-162.92	97062	2.28	132	0.66	1
23622.86	-18067.5	-162.92	97062	1.03	8.4	0.16	0.26
23617.24	-18071.1	-159.65	97063	1.95	17.8	0.29	0.69
23616.48	-18071.4	-160.19	97063	1.38	51.5	0.25	2.34
23623.94	-18060.2	-154	97065	23.13	55.8	3.52	1.51

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23623.4	-18060.9	-154.44	97065	19.47	12.3	0.68	0.88
23624.48	-18059.5	-153.55	97065	16.23	30.2	1.55	6.26
23621.77	-18063	-155.77	97065	6.9	23.1	1.84	2.83
23622.85	-18061.6	-154.88	97065	3.42	1.7	0.08	0.06
23615.25	-18071.6	-161.09	97065	2.64	390	1.29	1.13
23622.31	-18062.3	-155.33	97065	1.52	5.82	0.48	0.66
23615.79	-18070.9	-160.65	97065	1.51	216.9	0.74	0.75
23621.23	-18063.7	-156.21	97065	1.32	3.3	0.28	0.2
23625.03	-18058.8	-153.11	97065	1.11	0.4	0.03	0.03
23627.2	-18055.9	-151.34	97065	1.02	3	0.26	0.46
23615.01	-18076.5	-162.94	97066	14.61	33	0.18	7.72
23614.62	-18075.6	-162.94	97066	14.28	27	1.35	0.36
23620.13	-18088.5	-162.94	97066	12.84	102	1.1	9.65
23619.73	-18087.5	-162.94	97066	11.9	89.85	1.43	8.14
23615.8	-18078.4	-162.94	97066	11.4	52.8	0.09	3.35
23619.34	-18086.6	-162.94	97066	8.4	56.45	1.11	5.47
23615.4	-18077.4	-162.94	97066	8.04	39.8	0.13	14.1
23616.19	-18079.3	-162.94	97066	6.87	126.22	0.26	5.78
23618.95	-18085.7	-162.94	97066	5.32	35.2	0.88	3.13
23618.55	-18084.8	-162.94	97066	5.09	37.6	0.85	1.28
23618.16	-18083.9	-162.94	97066	2.76	21.3	0.24	0.31
23616.98	-18081.1	-162.94	97066	1.65	9.65	0.12	0.03
23617.37	-18082	-162.94	97066	1.65	14.05	0.13	0.04
23575.35	-18148.3	-149.2	97068	11.07	298	3.17	4.09
23581.71	-18151.2	-149.2	97068	8.76	67.8	2.31	7.3
23579.89	-18150.4	-149.2	97068	8.46	132	4.58	7.61
23582.62	-18151.6	-149.2	97068	8.01	112	2.39	7.96
23580.8	-18150.8	-149.2	97068	6.24	162	4.38	12.1
23576.26	-18148.7	-149.2	97068	5.7	117	4.48	12.1
23577.17	-18149.1	-149.2	97068	5.64	175	4.76	4.92
23578.07	-18149.6	-149.2	97068	3.93	141	2.93	2.8
23573.53	-18147.5	-149.2	97068	3.09	70.4	0.78	0.76
23578.98	-18150	-149.2	97068	2.88	35.4	1.48	2.72
23583.52	-18152.1	-149.2	97068	1.98	1.3	0.07	0.19
23572.62	-18147	-149.2	97068	1.65	17.8	0.59	0.64
23557.66	-18139.9	-126.66	97069	35.7	215.55	3.15	11.07
23557.28	-18139.7	-125.75	97069	32.31	162.08	3.39	10.3
23558.04	-18140.1	-127.57	97069	24.1	200.85	2.93	4.7
23559.56	-18140.8	-131.19	97069	12.28	74.85	2.56	0.75
23559.94	-18141	-132.1	97069	11.06	72.1	2.35	0.64
23558.42	-18140.3	-128.47	97069	6.46	40.5	1.43	0.99
23558.8	-18140.4	-129.38	97069	3.21	35.7	1.09	1.13
23556.91	-18139.5	-124.85	97069	2.4	-999	-999	-999

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23559.18	-18140.6	-130.29	97069	1.93	12.9	0.43	0.99
23564.88	-18143.4	-143.89	97069	1.75	0.2	0.01	0.01
23567.17	-18145	-144.01	97070	8.47	-999	-999	-999
23567.17	-18145	-145.01	97070	7.82	-999	-999	-999
23567.17	-18145	-146.51	97070	4.36	-999	-999	-999
23567.17	-18145	-142.01	97070	2.25	-999	-999	-999
23682.01	-18285.5	-206.78	97071	28.41	156	9.21	9.43
23665.22	-18293.2	-206.78	97071	23.13	491	15	7.4
23663.81	-18293.8	-206.78	97071	19.02	7.4	0.41	4.42
23681.1	-18285.9	-206.78	97071	18.63	249	9.48	4.1
23682.92	-18285.1	-206.78	97071	16.08	167	5.56	4.12
23664.72	-18293.4	-206.78	97071	14.83	247.24	7.61	4.46
23659.26	-18295.9	-206.78	97071	14.13	47.9	1.76	5.94
23658.35	-18296.3	-206.78	97071	13.77	29.2	1.16	4.5
23683.83	-18284.7	-206.78	97071	12.93	116	3.46	10.1
23657.44	-18296.7	-206.78	97071	11.67	14.8	0.67	6.24
23661.08	-18295	-206.78	97071	10.13	42.35	3.42	11.15
23660.17	-18295.5	-206.78	97071	9.78	55	3.91	9.71
23684.75	-18284.3	-206.78	97071	8.83	39.02	0.84	5.01
23661.99	-18294.6	-206.78	97071	7.29	18.15	0.56	6.24
23662.9	-18294.2	-206.78	97071	5.05	11.4	0.35	1.49
23673.91	-18289.2	-206.78	97071	2.21	15.34	0.67	0.68
23673	-18289.6	-206.78	97071	1.95	7.16	0.19	0.87
23668.45	-18291.7	-206.78	97071	1.89	16.4	0.35	1.18
23672.09	-18290	-206.78	97071	1.82	9.18	0.29	0.94
23674.82	-18288.8	-206.78	97071	1.81	11.48	0.49	0.88
23675.73	-18288.4	-206.78	97071	1.72	5.78	0.19	0.65
23665.72	-18292.9	-206.78	97071	1.43	8.06	0.29	0.42
23676.64	-18288	-206.78	97071	1.21	6.64	0.19	0.4
23671.18	-18290.5	-206.78	97071	1.17	5.04	0.18	0.22
23667.54	-18292.1	-206.78	97071	1.14	3.7	0.1	0.38
23666.63	-18292.5	-206.78	97071	1.07	4.1	0.11	0.36
23676.38	-18331.8	-207.53	97072	52.24	27.45	1.09	1.15
23677.36	-18331.6	-207.53	97072	48.27	66.65	2.44	2.02
23678.33	-18331.3	-207.53	97072	31.62	102.95	4.87	4.05
23679.3	-18331.1	-207.53	97072	30.45	93.25	6.21	5.8
23684.17	-18330	-207.53	97072	25.83	10.2	0.23	2
23675.41	-18332	-207.53	97072	24.92	37.8	1.2	1.08
23684.86	-18329.8	-207.53	97072	24.6	17.5	0.25	2.38
23683.2	-18330.2	-207.53	97072	21.75	23.31	0.19	3.22
23674.43	-18332.2	-207.53	97072	7.47	35	0.55	0.92
23680.28	-18330.9	-207.53	97072	6.68	21.68	1.53	1.4
23498.16	-17807.7	-47.83	97073	3.81	3.7	0.07	0.47

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23498.16	-17807.7	-49.58	97073	3.81	4.6	0.13	1.04
23498.16	-17807.7	-46.83	97073	3	3.85	0.06	0.49
23498.16	-17807.7	-31.83	97073	2.49	4.1	0.05	0.1
23498.16	-17807.7	-42.83	97073	2.19	4.5	0.24	0.34
23498.16	-17807.7	-43.83	97073	2.19	4.5	0.24	0.34
23498.16	-17807.7	-45.83	97073	2.13	4	0.08	0.46
23498.16	-17807.7	-44.83	97073	1.83	4	0.15	0.2
23498.16	-17807.7	-26.83	97073	1.77	6.8	0.09	0.22
23498.16	-17807.7	-32.83	97073	1.11	4.1	0.06	0.07
23498.16	-17807.7	-33.83	97073	1.02	4.55	0.08	0.08
23497.54	-17817.6	-40.38	97074	6.09	31.1	0.53	0.52
23497.59	-17816.8	-38.54	97074	6.03	16.4	0.77	0.54
23497.51	-17818	-41.3	97074	5.07	9	0.11	0.2
23497.64	-17816	-36.71	97074	4.95	15.2	0.71	0.26
23497.49	-17818.3	-41.99	97074	4.95	2.9	0.09	0.23
23497.61	-17816.4	-37.63	97074	3.6	3.8	0.13	0.05
23497.66	-17815.7	-36.02	97074	3.33	6.7	0.14	0.43
23497.48	-17818.6	-42.68	97074	2.85	3.1	0.1	0.61
23497.67	-17815.4	-35.33	97074	2.56	7.18	0.1	0.21
23497.4	-17819.7	-45.43	97074	1.92	4.6	0.06	0.62
23497.39	-17820	-45.94	97074	1.92	4.6	0.06	0.62
23497.7	-17815	-34.41	97074	1.5	6.55	0.05	0.09
23497.43	-17819.4	-44.51	97074	1.26	4.4	0.03	0.63
23497.72	-17814.6	-33.49	97074	1.11	6.85	0.04	0.12
23497.75	-17814.2	-32.58	97074	1.06	6.99	0.03	0.1
23495.39	-17842.9	-39.97	97075	26.37	192	5.55	4
23495.33	-17843.7	-40.51	97075	16.11	203	4.62	10.6
23495.46	-17842	-39.43	97075	14.73	218	6.24	3.29
23495.71	-17838.7	-37.26	97075	11.97	118.5	2.38	5.83
23495.58	-17840.4	-38.34	97075	11.85	23.8	0.64	2.3
23495.26	-17844.6	-41.05	97075	11.69	180.92	3.66	5.61
23495.21	-17845.2	-41.46	97075	10.8	176.5	3.47	4.61
23495.52	-17841.2	-38.88	97075	10.05	181	4.1	7.59
23495.84	-17837	-36.18	97075	9.39	99.1	1.48	1.49
23495.78	-17837.9	-36.72	97075	9.06	80.8	0.66	2.48
23496.55	-17827.8	-30.21	97075	8.31	4.7	0.03	0.13
23495.65	-17839.5	-37.8	97075	8.01	32	0.21	0.89
23496.74	-17825.3	-28.59	97075	7.14	15.5	0.14	0.38
23496.62	-17827	-29.67	97075	5.37	5.6	0.07	0.17
23496.68	-17826.1	-29.13	97075	5.28	6	0.03	0.11
23496.49	-17828.6	-30.76	97075	5.13	7.4	0.03	0.07
23496.81	-17824.4	-28.05	97075	4.56	27.5	0.29	0.6
23495.91	-17836.2	-35.63	97075	4.56	48.1	0.66	1.49

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23495.97	-17835.3	-35.09	97075	3.39	7.8	0.09	0.07
23496.42	-17829.5	-31.3	97075	2.57	3.8	0.02	0.04
23496.04	-17834.5	-34.55	97075	2.54	10.6	0.06	0.08
23497.04	-17821.5	-26.15	97075	1.92	17.2	0.19	0.62
23495.17	-17845.8	-41.86	97075	1.89	13.3	0.14	0.27
23494.97	-17848.3	-43.49	97075	1.71	8.3	0.32	0.9
23497.23	-17819	-24.53	97075	1.53	5.7	0.06	0.08
23496.86	-17823.8	-27.64	97075	1.47	3.3	0.06	0.18
23496.91	-17823.2	-27.23	97075	1.37	9.95	0.09	0.24
23496.97	-17822.4	-26.69	97075	1.26	16.6	0.13	0.3
23497.1	-17820.7	-25.61	97075	1.23	10.2	0.16	0.41
23494.91	-17849.2	-44.03	97075	1.11	3.5	0.11	0.59
23492.69	-17798.8	-38.7	97076	23.24	134.2	3.66	1.5
23492.47	-17798.4	-39.6	97076	13.79	77.14	2.37	0.35
23492.04	-17797.7	-41.41	97076	13.17	83.3	2.25	1
23492.25	-17798	-40.51	97076	7.17	34.7	0.83	0.47
23497.58	-17780.7	-37.13	97077	31.77	65.7	2.4	4.82
23497.68	-17793.7	-27.74	97077	29.91	118	4	3.91
23497.49	-17769	-45.63	97077	28.98	344	0.79	1.92
23497.6	-17783.1	-35.37	97077	28.29	205	6.54	5.44
23497.59	-17781.5	-36.54	97077	28.26	89.4	2.86	4.38
23497.65	-17789.6	-30.67	97077	27.69	194	1.97	2.28
23497.59	-17782.3	-35.95	97077	26.76	80.3	2.74	2.62
23497.65	-17790.4	-30.09	97077	21.91	238.29	1.58	1.76
23497.48	-17766.5	-47.39	97077	17.43	182	1.91	4.13
23497.67	-17792.8	-28.33	97077	15.69	40.1	1.46	0.43
23497.66	-17792	-28.91	97077	12.63	33	1.15	0.83
23497.58	-17780.1	-37.57	97077	8.79	10.9	0.42	0.59
23497.66	-17791.2	-29.5	97077	7.47	349	0.61	0.47
23497.55	-17776.2	-40.35	97077	6.21	4.1	0.23	0.56
23497.54	-17775.4	-40.94	97077	5.31	32.9	0.33	1.59
23497.54	-17774.6	-41.53	97077	5.16	18.6	0.44	1.04
23497.51	-17771.4	-43.87	97077	4.89	10.9	0.21	0.31
23497.57	-17779.5	-38.01	97077	4.71	4.7	0.21	0.2
23497.53	-17773.8	-42.11	97077	4.59	7.9	0.25	0.25
23497.5	-17769.8	-45.05	97077	3.36	10.5	1	3.01
23497.52	-17773	-42.7	97077	3	2.3	0.04	0.17
23497.49	-17768.1	-46.22	97077	2.46	2.9	0.03	0.16
23497.6	-17783.9	-34.78	97077	2.31	36.8	0.15	0.28
23497.48	-17767.3	-46.81	97077	2.25	7.1	0.23	0.23
23497.56	-17777.9	-39.18	97077	2.07	2.1	0.07	0.18
23497.57	-17778.7	-38.59	97077	1.77	15.8	0.14	0.17
23497.52	-17772.2	-43.29	97077	1.29	5.5	0.13	0.25

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23497.62	-17785.6	-33.61	97077	1.2	24.8	0.12	0.38
23497.55	-17777.1	-39.77	97077	1.11	6.1	0.31	0.81
23488.61	-17825.3	-23.63	97078	8.73	38.4	0.12	0.66
23484.95	-17832.1	-25.97	97078	6.09	4.65	0	0.06
23480.82	-17839.6	-28.61	97078	5.47	24.05	0.22	0.88
23484.49	-17832.9	-26.27	97078	5.03	5.5	0.01	0.05
23478.53	-17843.8	-30.08	97078	4.83	6.95	0.25	0.51
23485.4	-17831.2	-25.68	97078	4.74	6.8	0.01	0.09
23482.66	-17836.3	-27.44	97078	4.64	7.85	0.08	0.16
23480.36	-17840.5	-28.91	97078	4.61	15.95	0.06	0.25
23478.99	-17843	-29.79	97078	4.56	8.25	0.25	0.51
23485.86	-17830.4	-25.39	97078	4.49	11.55	0.05	0.08
23486.32	-17829.5	-25.09	97078	4.43	11.2	0.07	0.09
23474.87	-17850.5	-32.42	97078	4.41	44	1.12	2.37
23481.28	-17838.8	-28.32	97078	4.34	35.6	0.44	0.97
23489.07	-17824.5	-23.34	97078	4.29	7.4	0.08	0.2
23483.57	-17834.6	-26.85	97078	4.28	7	0	0.05
23482.2	-17837.1	-27.73	97078	4.09	10.4	0.15	0.37
23487.7	-17827	-24.21	97078	3.99	6.9	0.05	0.2
23475.32	-17849.7	-32.13	97078	3.69	33.09	0.84	1.88
23487.24	-17827.9	-24.51	97078	3.57	37.2	0.09	0.17
23477.61	-17845.5	-30.67	97078	3.29	6.7	0.33	0.5
23490.9	-17821.2	-22.16	97078	3.24	8.65	0.4	0.79
23471.66	-17856.4	-34.48	97078	2.91	3.1	0.1	0.1
23490.45	-17822	-22.46	97078	2.89	7.1	0.47	1.17
23478.07	-17844.6	-30.37	97078	2.85	2.8	0.09	0.2
23477.16	-17846.3	-30.96	97078	2.76	7.05	0.3	0.5
23486.78	-17828.7	-24.8	97078	2.22	7.7	0.03	0.15
23489.99	-17822.8	-22.75	97078	2.15	11.65	0.21	1.05
23472.12	-17855.6	-34.18	97078	2.13	3.9	0.08	0.12
23471.2	-17857.2	-34.77	97078	1.98	1.9	0.03	0.16
23475.78	-17848.8	-31.84	97078	1.89	5.8	0.15	0.67
23474.41	-17851.4	-32.72	97078	1.29	4	0.13	0.38
23488.15	-17826.2	-23.92	97078	1.23	8	0.07	0.33
23482.9	-17835.7	-37.69	97079	4.89	16.05	0.64	0.88
23485.83	-17830.3	-33.79	97079	4.87	15	0.16	0.11
23483.3	-17835	-37.15	97079	4.26	13.75	0.48	0.52
23486.13	-17829.8	-33.39	97079	4.07	10.8	0.12	0.12
23492.19	-17818.7	-25.32	97079	3.67	11.8	0.13	0.57
23484.01	-17833.7	-36.21	97079	3.6	6.7	0.02	0.04
23484.72	-17832.4	-35.27	97079	3.33	6.7	0.05	0.06
23486.54	-17829	-32.85	97079	3.31	5.45	0.07	0.12
23491.79	-17819.4	-25.86	97079	3.12	8.6	0.09	0.37

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23492.9	-17817.4	-24.38	97079	2.74	6.9	0.24	0.25
23486.94	-17828.3	-32.32	97079	2.71	8.45	0.08	0.13
23485.12	-17831.6	-34.74	97079	2.61	15.6	0.16	0.23
23483.71	-17834.2	-36.62	97079	2.26	5.2	0.09	0.45
23478.65	-17843.5	-43.34	97079	2.13	5	0.04	0.19
23480.07	-17840.9	-41.46	97079	2.06	4.6	0.14	0.26
23479.46	-17842	-42.26	97079	1.99	5.8	0.12	0.27
23487.34	-17827.6	-31.78	97079	1.88	7.95	0.04	0.09
23482.49	-17836.4	-38.23	97079	1.86	5.85	0.23	0.73
23485.53	-17830.9	-34.2	97079	1.82	8.3	0.02	0.05
23478.25	-17844.2	-43.88	97079	1.82	3.6	0.02	0.07
23479.76	-17841.4	-41.86	97079	1.71	4.7	0.1	0.24
23493.21	-17816.8	-23.98	97079	1.63	4.95	0.16	0.29
23487.75	-17826.8	-31.24	97079	1.52	4.5	0	0.04
23479.06	-17842.7	-42.8	97079	1.41	5.2	0.13	1.17
23484.31	-17833.1	-35.81	97079	1.37	4.6	0	0.04
23480.47	-17840.1	-40.92	97079	1.36	3.2	0.13	0.17
23477.84	-17844.9	-44.41	97079	1.34	2.4	0.02	0.04
23477.04	-17846.4	-45.49	97079	1.23	2.1	0.05	0.51
23491.39	-17820.2	-26.4	97079	1.03	3.1	0.04	0.18
23489.49	-17818.8	-26.05	97080	12.52	39.83	1.29	1.37
23479.76	-17831.1	-35.82	97080	12.19	13.86	0.43	0.7
23490.02	-17818.1	-25.52	97080	10.45	33.45	1.08	1.21
23476.6	-17835.1	-38.99	97080	4.18	23.2	0.75	0.76
23480.81	-17829.8	-34.77	97080	3.63	68.6	0.36	0.24
23482.65	-17827.4	-32.92	97080	3.26	18.6	0.1	0.14
23482.26	-17827.9	-33.31	97080	3.26	18.6	0.1	0.14
23476.07	-17835.8	-39.52	97080	3.13	21.03	0.63	0.39
23480.28	-17830.4	-35.29	97080	3.07	18.95	0.45	0.6
23478.7	-17832.4	-36.88	97080	2.37	4.5	0.05	0.09
23477.65	-17833.8	-37.94	97080	2.16	4	0.05	0.13
23481.33	-17829.1	-34.24	97080	2.06	6.9	0.02	0.06
23471.86	-17841.1	-43.75	97080	1.78	2.1	0.02	0.02
23479.23	-17831.8	-36.35	97080	1.71	5.2	0.09	0.32
23478.18	-17833.1	-37.41	97080	1.54	4.7	0.08	0.32
23490.54	-17817.4	-24.99	97080	1.24	5.05	0.12	0.21
23481.86	-17828.4	-33.71	97080	1.23	8.1	0.05	0.08
23477.13	-17834.4	-38.46	97080	1.13	3.8	0.07	0.17
23490.48	-17818.1	-35.62	97081	17.31	30.8	0.41	1.31
23489.8	-17819.1	-37.26	97081	15.65	33.26	0.96	3.83
23489.46	-17819.5	-38.09	97081	14.4	29	0.79	3.26
23491.15	-17817.2	-33.98	97081	9.94	16.4	0.62	0.18
23491.49	-17816.8	-33.16	97081	8.98	16.1	0.31	0.21

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23489.2	-17819.9	-38.7	97081	6.86	8.8	0.17	0.51
23488.95	-17820.2	-39.32	97081	3.91	8.7	0.14	0.7
23488.71	-17820.5	-39.89	97081	3.91	8.7	0.14	0.7
23490.14	-17818.6	-36.44	97081	3.24	94.27	2.37	1.76
23485.07	-17825.4	-48.69	97081	2.09	4.27	0.08	0.25
23487.79	-17821.8	-42.11	97081	1.99	4.45	0.08	0.31
23484.73	-17825.9	-49.51	97081	1.79	5.41	0.12	0.32
23488.13	-17821.3	-41.29	97081	1.71	9.4	0.26	0.42
23486.43	-17823.6	-45.4	97081	1.49	2.84	0.06	0.58
23485.41	-17825	-47.86	97081	1.4	8.62	0.16	0.25
23486.09	-17824	-46.22	97081	1.26	2.54	0.04	0.18
23486.77	-17823.1	-44.58	97081	1.24	2.18	0.05	0.27
23510.65	-17839.9	-40.79	97082	24.57	226.67	4.92	5.83
23510.35	-17839.1	-40.22	97082	19.31	130.54	4.53	4.07
23511.54	-17842.2	-42.48	97082	19.25	174.3	5.2	7.02
23511.24	-17841.4	-41.91	97082	17.24	133.3	3.92	10.76
23510.95	-17840.6	-41.35	97082	16.63	86.13	2.39	5.76
23511.84	-17843	-43.04	97082	15.27	107.4	2.9	4.88
23512.44	-17844.5	-44.17	97082	14.84	724.9	18.45	8.32
23512.14	-17843.7	-43.61	97082	14.67	298.1	7.81	7.2
23512.74	-17845.3	-44.73	97082	11.21	552.5	13.65	15.29
23513.03	-17846	-45.3	97082	5.4	108.9	3.95	13.82
23503.7	-17821.9	-27.64	97082	4.15	22.4	0.16	0.17
23513.21	-17846.5	-45.64	97082	1.68	39.8	2.99	0.24
23503.77	-17821	-42.11	97083	17.31	108.5	1.81	1.42
23504.16	-17821.9	-43.84	97083	9.33	36.4	0.42	0.45
23503.96	-17821.4	-42.97	97083	6.93	33.7	0.22	1.01
23501.71	-17816.1	-33.04	97083	6.21	16.2	0.05	0.12
23504.55	-17822.8	-45.56	97083	4.05	239	0.28	0.22
23501.51	-17815.6	-32.18	97083	3.98	14.4	0.04	0.12
23505.33	-17824.7	-49.02	97083	3.83	6.9	0.64	0.49
23504.35	-17822.4	-44.7	97083	3.02	3.7	0.03	0.16
23501.32	-17815.2	-31.31	97083	2.38	8.7	0.05	0.12
23500.44	-17813.1	-27.42	97083	1.95	6.3	0.05	0.13
23500.58	-17813.4	-28.07	97083	1.95	6.3	0.05	0.13
23500.73	-17813.8	-28.72	97083	1.89	6	0.06	0.29
23506.12	-17826.5	-52.48	97083	1.85	6	0.08	1.9
23505.53	-17825.1	-49.88	97083	1.68	3.2	0.12	0.68
23482.46	-17817.6	-34.29	97085	25.23	151	4.5	4.94
23481.21	-17818.4	-35.65	97085	21.53	218	7.56	8.22
23481.83	-17818	-34.97	97085	21.46	69.5	2.56	5.08
23483.08	-17817.2	-33.62	97085	20.85	79.9	2.19	5.05
23480.58	-17818.8	-36.33	97085	13.87	78.08	1.89	2.66

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23470.28	-17825.2	-47.51	97085	4.49	5.4	0.03	0.06
23479.96	-17819.2	-37.01	97085	4.46	9.2	0.18	0.39
23479.34	-17819.6	-37.68	97085	3.85	7.83	0.17	0.56
23470.9	-17824.8	-46.84	97085	3.67	4.2	0.01	0.02
23468.4	-17826.4	-49.55	97085	3.63	2.7	0	0.12
23478.87	-17819.9	-38.19	97085	3.39	6.8	0.16	0.69
23469.65	-17825.6	-48.19	97085	3.28	3.9	0.01	0.05
23491.21	-17812.2	-24.8	97085	3.19	9.1	0.52	0.54
23475.27	-17822.1	-42.09	97085	3.09	8.3	0.57	1.57
23467.78	-17826.7	-50.23	97085	2.33	2.25	0	0.17
23471.53	-17824.4	-46.16	97085	2.16	2.55	0.01	0.03
23469.03	-17826	-48.87	97085	2.06	2.4	0	0.03
23489.96	-17813	-26.16	97085	1.71	18.8	0.21	0.3
23472.78	-17823.6	-44.8	97085	1.44	5.4	0.16	0.05
23473.4	-17823.3	-44.12	97085	1.32	5.1	0.15	0.09
23474.02	-17822.9	-43.45	97085	1.2	4.8	0.14	0.12
23490.58	-17812.6	-25.48	97085	1.06	5.1	0.07	0.1
23467.15	-17827.1	-50.9	97085	1.03	1.8	0.01	0.22
23464.67	-17791.3	-38.28	97086	45.09	196	7.08	6.71
23465.41	-17791.7	-37.81	97086	37.47	160.5	4.47	11.6
23468.52	-17793.2	-35.84	97086	37.27	26.5	2.42	2.94
23467.75	-17792.8	-36.33	97086	32.67	68.1	5.26	4.65
23466.97	-17792.5	-36.83	97086	32.06	112	3.21	8.73
23466.19	-17792.1	-37.32	97086	29.35	90.1	4.73	7.2
23471.64	-17794.8	-33.87	97086	28.6	269.45	5.24	8.6
23472.42	-17795.2	-33.38	97086	19.92	431	6.13	7.18
23470.08	-17794	-34.86	97086	13.38	85.4	2.67	8.52
23470.86	-17794.4	-34.37	97086	8.6	108	2.24	3.29
23477.08	-17797.5	-30.43	97086	6.94	18.64	3.26	0.39
23469.3	-17793.6	-35.35	97086	5.23	15.3	0.36	2.75
23462.38	-17790.2	-39.73	97086	4.15	50.36	1.33	0.92
23474.75	-17796.4	-31.91	97086	3.87	36.8	0.08	0.19
23477.86	-17797.9	-29.94	97086	1.67	4.77	0.58	0.2
23500.27	-17783.5	-35.15	97087	36.98	65.36	4.21	4.83
23500.8	-17779.6	-38.03	97087	32.3	43.6	1.37	2.77
23500.16	-17784.3	-34.56	97087	31.87	127.22	5	6.49
23500.59	-17781.1	-36.91	97087	28.26	66.44	2.81	7.47
23500.7	-17780.4	-37.47	97087	26.47	84.8	2.94	5.27
23501.97	-17770.9	-44.37	97087	22.56	211	6.25	9.19
23499.62	-17788.3	-31.63	97087	22.3	118.1	5.06	6.52
23502.07	-17770.2	-44.93	97087	21.46	339.33	9.4	4.74
23500.38	-17782.7	-35.74	97087	20.5	51.1	2.08	2.35
23501.77	-17772.4	-43.31	97087	12.82	36.95	0.22	0.37

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23499.15	-17791.9	-29.04	97087	11.19	41.53	0.85	0.93
23499.51	-17789.1	-31.04	97087	8.97	91.38	2.79	7.44
23501.66	-17773.2	-42.72	97087	8.88	77.95	1.74	2.41
23499.73	-17787.5	-32.21	97087	8.38	127.07	3.07	3.75
23500.05	-17785.1	-33.97	97087	7.58	110.61	1.66	2.37
23499.41	-17789.9	-30.45	97087	7.44	150.32	3.85	7.6
23500.49	-17781.9	-36.32	97087	7.34	52.04	1.39	2.18
23499.25	-17791.1	-29.63	97087	5.37	41.24	0.5	0.77
23501.56	-17774	-42.14	97087	4.8	226	1.82	2.55
23501.12	-17777.2	-39.79	97087	4.66	102	2.51	5.12
23501.02	-17778	-39.2	97087	1.99	44.5	1.38	0.82
23501.87	-17771.7	-43.84	97087	1.99	3.9	0.09	0.43
23502.17	-17769.4	-45.48	97087	1.54	11.44	0.21	0.33
23501.45	-17774.8	-41.55	97087	1.36	273	0.27	0.52
23499.84	-17786.7	-32.8	97087	1.27	33.78	0.42	0.37
23499.04	-17792.7	-28.45	97087	1.05	13.07	0.04	0.18
23499.33	-17790.5	-30.04	97087	1.03	36.5	0.21	0.57
23490.41	-17788.7	-33.07	97088	16.39	8.8	0.36	0.12
23490.2	-17788.2	-33.52	97088	16.39	8.8	0.36	0.12
23491.82	-17792.4	-30	97088	10.87	49.6	1.94	1.65
23488.58	-17783.9	-37.04	97088	6.48	9.87	0.32	0.64
23488.86	-17784.7	-36.43	97088	5.74	9.59	0.31	0.62
23491.26	-17791	-31.23	97088	3.63	32	0.95	0.47
23490.98	-17790.2	-31.84	97088	3.63	32	0.95	0.47
23492.1	-17793.2	-29.39	97088	3.33	16.7	0.76	0.69
23492.38	-17793.9	-28.78	97088	2.71	13.5	0.36	0.28
23491.54	-17791.7	-30.62	97088	2.71	4.3	0.28	0.15
23489.99	-17787.6	-33.98	97088	1.99	5.7	0.14	0.51
23492.67	-17794.7	-28.17	97088	1.58	7.4	0.18	0.12
23497.53	-17784.2	-41.09	97089	62.37	166	5.16	6.98
23497.53	-17784.9	-40.37	97089	36.1	432	5.63	6.3
23497.53	-17791.8	-33.22	97089	33.81	124	5.41	1.02
23497.52	-17779.3	-46.09	97089	33.44	328	6.88	8.93
23497.53	-17787.7	-37.51	97089	29.13	424.5	7.36	5.8
23497.53	-17787	-38.23	97089	28.55	462	7.27	6.05
23497.51	-17768.4	-57.17	97089	26.06	46.95	1.83	1.93
23497.52	-17778.6	-46.81	97089	25.52	207	2.57	4.58
23497.54	-17793.2	-31.79	97089	24.96	23.5	4.37	0.48
23497.53	-17786.3	-38.94	97089	23.4	455	8.21	7.76
23497.54	-17792.5	-32.51	97089	22.59	45.7	6.34	1.83
23497.53	-17790.5	-34.65	97089	20.37	21.7	0.63	1.03
23497.54	-17793.9	-31.08	97089	20.33	37.2	4.28	3.61
23497.53	-17788.4	-36.8	97089	15.94	202.05	4.93	3.88

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23497.53	-17789.8	-35.37	97089	13.41	28.4	0.74	1.24
23497.52	-17777.9	-47.52	97089	10.55	114.24	2.01	2.93
23497.52	-17780	-45.38	97089	10.24	128.62	3.87	4.19
23497.53	-17789.1	-36.08	97089	7.84	62.6	1.57	1.79
23497.53	-17785.6	-39.66	97089	7.07	503.9	2.31	1.05
23497.52	-17781.4	-43.95	97089	6.31	7.7	0.1	0.11
23497.52	-17775.1	-50.38	97089	6.07	78.05	0.37	0.34
23497.51	-17769.1	-56.46	97089	5.07	8.97	0.39	0.51
23497.52	-17777.2	-48.23	97089	4.87	26.45	0.64	1.4
23497.52	-17775.8	-49.66	97089	4.73	46.25	0.5	0.37
23497.52	-17774.5	-50.92	97089	3.91	76.7	0.17	0.15
23497.52	-17776.5	-48.95	97089	3.26	16.1	0.45	0.43
23497.53	-17782.8	-42.52	97089	2.88	19.2	0.25	0.38
23497.51	-17770.5	-55.03	97089	2.5	11.8	0.52	0.94
23497.54	-17797.6	-27.36	97089	2.4	49	0.71	0.17
23497.54	-17796.9	-28.08	97089	1.99	36.61	0.52	0.16
23497.51	-17767.7	-57.89	97089	1.99	11.2	0.23	0.52
23497.52	-17780.7	-44.66	97089	1.3	153	0.41	0.53
23497.53	-17783.5	-41.8	97089	1.27	3.6	0.07	0.16
23497.51	-17771.9	-53.6	97089	1.1	6	0.23	0.29
23495.93	-17792.9	-37.72	97090	6.14	21.5	0.51	0.29
23496.06	-17794.1	-36.11	97090	4.77	7	0.02	0.08
23496	-17793.5	-36.92	97090	4.15	5.2	0.03	0.04
23495.86	-17792.3	-38.53	97090	3.39	5.5	0.16	0.05
23496.13	-17794.7	-35.3	97090	3.02	7	0.06	0.06
23495.8	-17791.7	-39.3	97090	2.85	2.8	0.1	0.12
23496.2	-17795.2	-34.5	97090	1.82	7.3	0.13	0.17
23497.04	-17802.6	-24.41	97090	1.58	6.8	0.18	0.6
23496.27	-17795.8	-33.69	97090	1.47	10.3	0.06	0.09
23464.01	-17825.7	-30.97	97091	33.07	308.5	3.51	6.03
23465.52	-17821.5	-25.59	97091	25.99	126.25	5.53	4.45
23463.8	-17826.3	-31.74	97091	22.69	145.5	2.32	3.18
23465.3	-17822.1	-26.36	97091	22.2	82.4	4.45	2.43
23464.23	-17825.1	-30.2	97091	17.47	199.2	2.09	3.38
23465.09	-17822.7	-27.13	97091	14.47	74.55	2.88	2.48
23465.73	-17820.9	-24.82	97091	12.74	94.2	2.47	3.37
23464.87	-17823.3	-27.89	97091	11.21	65.5	2.84	2.75
23464.66	-17823.9	-28.66	97091	9.39	36.95	1.75	2.67
23464.44	-17824.5	-29.43	97091	6.97	25.8	0.87	1.53
23462.72	-17829.3	-35.58	97091	2.98	3.2	0.05	0.11
23463.36	-17827.5	-33.27	97091	2.78	11.3	0.14	0.22
23466.11	-17819.8	-23.48	97091	2.67	29.9	0.24	0.51
23463.15	-17828.1	-34.04	97091	2.47	2.5	0.06	0.05

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23465.95	-17820.3	-24.05	97091	2.45	36.4	0.31	0.48
23462.93	-17828.7	-34.81	97091	2.3	4.3	0.12	0.66
23462.5	-17829.9	-36.35	97091	2.26	2.5	0.04	0.14
23463.58	-17826.9	-32.51	97091	1.95	2.7	0.05	0.02
23466.27	-17819.4	-22.9	97091	1.92	12.7	0.35	5.09
23462.34	-17830.4	-36.92	97091	1.85	2.6	0.03	0.1
23471.09	-17802.5	-43.61	97092	51.22	39.6	0.98	0.96
23471.33	-17801.7	-43.61	97092	51.22	39.6	0.98	0.96
23486.44	-17754.3	-43.61	97092	41.11	354	6.04	7.66
23485.83	-17756.2	-43.61	97092	40.87	208	2.36	2.24
23472.76	-17797.2	-43.61	97092	39.94	125	14.3	2.6
23484.92	-17759.1	-43.61	97092	31.78	272	3.65	4
23486.13	-17755.3	-43.61	97092	29.62	78.6	2.29	4.29
23473.06	-17796.3	-43.61	97092	27.84	59.2	2.18	3.64
23473.37	-17795.3	-43.61	97092	19.78	95.64	3.01	10.43
23473.97	-17793.4	-43.61	97092	18.94	278.5	7.41	4.44
23473.67	-17794.4	-43.61	97092	17.81	214.75	5.93	10.35
23474.28	-17792.4	-43.61	97092	14.26	323	9.03	1.77
23467.28	-17814.4	-43.61	97092	11.83	6	0.06	0.71
23474.58	-17791.5	-43.61	97092	11.01	309	9.1	0.68
23474.81	-17790.8	-43.61	97092	10.7	217	6.59	0.5
23466.98	-17815.3	-43.61	97092	10.68	5.2	0.08	0.65
23466.68	-17816.3	-43.61	97092	7.82	3.2	0.12	0.49
23465.46	-17820.1	-43.61	97092	7.68	28.2	0.08	0.15
23466.07	-17818.2	-43.61	97092	3.77	4.7	0.06	0.12
23465.76	-17819.1	-43.61	97092	2.67	11.6	0.08	0.16
23486.74	-17753.4	-43.61	97092	2.47	72.2	0.52	1.47
23464.7	-17822.5	-43.61	97092	2.32	6.35	0.24	0.25
23466.37	-17817.2	-43.61	97092	1.78	4.3	0.06	0.45
23465.23	-17820.8	-43.61	97092	1.68	5.9	0.39	0.13
23465	-17821.5	-43.61	97092	1.6	4.55	0.29	0.24
23500.05	-17772.1	-43.49	97093	25.71	85.5	4.01	8.95
23503.14	-17767.1	-43.49	97093	22.46	32.1	0.97	0.46
23499.6	-17772.8	-43.49	97093	22.21	106.5	3.99	6.99
23507.37	-17760.3	-43.49	97093	17.07	210	6.3	5.76
23506.84	-17761.2	-43.49	97093	14.47	193	5.13	22.8
23506.31	-17762	-43.49	97093	14.3	83.7	2.84	2.69
23481.74	-17801.5	-43.49	97093	13.81	78.45	1.53	2.13
23481.21	-17802.3	-43.49	97093	13.61	53.4	1.12	2.05
23503.67	-17766.3	-43.49	97093	11.11	190	5.9	6.41
23482.8	-17799.8	-43.49	97093	10.08	49.95	1.16	1.13
23504.73	-17764.6	-43.49	97093	10.05	227	7.09	3.64
23482.27	-17800.6	-43.49	97093	9.85	70.65	1.45	1.32

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23480.68	-17803.2	-43.49	97093	8.47	10.5	0.31	1.34
23483.32	-17798.9	-43.49	97093	8.4	11.55	0.3	1.07
23483.72	-17798.3	-43.49	97093	7.47	3.9	0.03	1
23502.08	-17768.8	-43.49	97093	7.27	3	0.11	0.08
23485.17	-17796	-43.49	97093	5.49	4.2	0.06	0.27
23497.86	-17775.6	-43.49	97093	4.49	2.1	0.09	0.19
23505.25	-17763.7	-43.49	97093	4.49	70.21	2.57	1.22
23486.23	-17794.3	-43.49	97093	3.26	4.2	0.09	0.18
23486.76	-17793.4	-43.49	97093	2.95	4.8	0.13	0.22
23485.7	-17795.1	-43.49	97093	2.88	1.8	0.03	0.06
23495.74	-17779	-43.49	97093	2.85	7.2	0.26	0.2
23489.82	-17788.5	-43.49	97093	2.43	6	0.25	1.15
23490.14	-17788	-43.49	97093	2.43	6	0.25	1.15
23500.5	-17771.4	-43.49	97093	2.3	5.1	0.11	0.29
23490.46	-17787.5	-43.49	97093	2.16	1.8	0.1	0.54
23495.21	-17779.8	-43.49	97093	1.65	2.7	0.07	0.17
23499.26	-17773.4	-43.49	97093	1.13	2.7	0.14	0.22
23507.9	-17759.5	-43.49	97093	1.06	7.2	0.44	1.68
23466.1	-17825.3	-31.91	97094	51.6	434	6.63	7.87
23465.75	-17825.9	-32.61	97094	42	188	2.66	3.65
23468.5	-17820.9	-27.03	97094	23.77	183.15	3.9	6.51
23468.84	-17820.2	-26.33	97094	21.6	218.69	3.25	3.37
23465.41	-17826.5	-33.31	97094	19.61	226	4.84	5.89
23466.44	-17824.6	-31.22	97094	16.18	525	4.24	5.4
23464.9	-17827.5	-34.36	97094	10.06	42.15	1.18	1.78
23464.55	-17828.1	-35.06	97094	9.44	23.9	0.85	1.68
23468.16	-17821.5	-27.72	97094	5.82	19.99	0.75	1.88
23467.13	-17823.4	-29.82	97094	5.42	17	0.38	1.51
23466.78	-17824	-30.52	97094	5.26	160.58	1.3	1.79
23465.15	-17827	-33.83	97094	4.83	39.1	0.77	0.68
23467.81	-17822.1	-28.42	97094	3.65	5.5	0.21	0.58
23464.21	-17828.7	-35.75	97094	3.02	3.25	0.08	0.32
23463.87	-17829.4	-36.45	97094	2.43	3.9	0.05	0.17
23463.52	-17830	-37.15	97094	1.75	1.6	0.04	0.17
23467.47	-17822.8	-29.12	97094	1.03	3	0.11	0.24
23474.88	-17813.8	-55.5	97095	5.62	3.5	0.03	0.06
23476.89	-17810.8	-57.17	97095	5.07	4.9	0.02	0.08
23473.38	-17816.1	-54.25	97095	4.49	3.9	0.02	0.13
23477.39	-17810.1	-57.59	97095	4.49	3.8	0.01	0.05
23480.91	-17804.8	-60.52	97095	4.18	4.2	0.03	0.35
23484.42	-17799.5	-63.45	97095	3.98	2.7	0.02	0.03
23484.8	-17798.9	-63.76	97095	3.98	2.7	0.02	0.03
23477.89	-17809.3	-58.01	97095	3.91	2.7	0.01	0.03

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23475.38	-17813.1	-55.92	97095	3.74	3.4	0.05	0.15
23475.89	-17812.3	-56.34	97095	3.7	3.4	0.05	0.25
23476.39	-17811.6	-56.76	97095	3.67	3.4	0.04	0.36
23474.38	-17814.6	-55.08	97095	3.46	2.55	0.03	0.05
23472.87	-17816.9	-53.83	97095	3.28	3.25	0.02	0.12
23483.92	-17800.2	-63.03	97095	3.22	2.6	0.02	0.14
23483.41	-17801	-62.61	97095	3.18	2.65	0.01	0.09
23482.91	-17801.7	-62.19	97095	3.15	2.7	0.01	0.04
23478.4	-17808.5	-58.43	97095	3.02	3.3	0.04	0.34
23478.9	-17807.8	-58.85	97095	3.02	3.3	0.04	0.34
23480.4	-17805.5	-60.1	97095	2.89	3.35	0.04	0.23
23467.1	-17825.6	-49.02	97095	2.61	2.4	0.02	0.05
23467.6	-17824.8	-49.44	97095	2.59	2.85	0.03	0.07
23468.11	-17824.1	-49.86	97095	2.57	3.3	0.04	0.09
23489.19	-17792.3	-67.42	97095	2.33	2.3	0.02	0.12
23472.37	-17817.6	-53.41	97095	2.06	2.6	0.02	0.1
23485.17	-17798.3	-64.07	97095	2.06	3.7	0.02	0.06
23468.61	-17823.3	-50.28	97095	2.02	4.5	0.02	0.16
23468.98	-17822.7	-50.59	97095	2.02	4.5	0.02	0.16
23488.69	-17793	-67	97095	2.02	2.15	0.03	0.18
23465.09	-17828.6	-47.35	97095	1.71	6.2	0.06	0.07
23488.18	-17793.8	-66.58	97095	1.71	2	0.04	0.24
23479.9	-17806.3	-59.68	97095	1.61	2.5	0.05	0.11
23473.88	-17815.4	-54.67	97095	1.3	1.6	0.02	0.04
23485.67	-17797.6	-64.49	97095	1.24	3.1	0.01	0.05
23520.46	-17817.5	-45.24	97096	32.23	43.3	3.43	5.91
23528.98	-17814.9	-45.48	97096	24.41	63.3	4.63	13.3
23511.84	-17820	-45	97096	11.38	22.6	0.56	0.57
23491.73	-17826.1	-44.44	97096	8.13	15.4	0.2	1.01
23499.39	-17823.8	-44.66	97096	6.51	16.45	0.11	2.28
23492.69	-17825.8	-44.47	97096	5.74	11.35	0.19	0.67
23477.75	-17830.2	-44.05	97096	5.49	27.3	0.21	0.33
23475.26	-17831	-43.98	97096	5.31	7.14	0.15	0.11
23477.17	-17830.4	-44.04	97096	4.73	22.26	0.18	0.3
23500.35	-17823.5	-44.68	97096	4.66	11.5	0.06	2.29
23496.52	-17824.6	-44.58	97096	4.46	9.8	0.44	0.41
23525.25	-17816	-45.38	97096	3.84	212	0.22	1.08
23486.94	-17827.5	-44.31	97096	3.6	2.9	0.1	0.35
23498.43	-17824	-44.63	97096	3.53	14.6	0.21	0.25
23493.64	-17825.5	-44.5	97096	3.36	7.3	0.17	0.32
23488.86	-17826.9	-44.36	97096	3.29	7.7	0.22	0.34
23495.56	-17824.9	-44.55	97096	3.28	7.81	0.31	0.3
23504.18	-17822.3	-44.79	97096	3.26	2.6	0.05	0.6

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23502.26	-17822.9	-44.74	97096	3.02	4.8	0.14	0.6
23489.81	-17826.6	-44.39	97096	2.96	5.85	0.15	0.46
23527.16	-17815.4	-45.43	97096	2.78	23.9	1.59	2.93
23528.12	-17815.2	-45.46	97096	2.78	23.9	1.59	2.93
23494.6	-17825.2	-44.52	97096	2.74	6.9	0.25	0.25
23490.77	-17826.3	-44.42	97096	2.64	4	0.08	0.57
23481.19	-17829.2	-44.15	97096	2.09	3.8	0.04	0.28
23508.01	-17821.2	-44.9	97096	2.06	2.5	0.07	0.16
23522.37	-17816.9	-45.3	97096	2.06	10	0.04	0.2
23497.47	-17824.3	-44.6	97096	1.99	16.2	0.28	0.27
23501.3	-17823.2	-44.71	97096	1.96	4.4	0.08	0.35
23524.29	-17816.3	-45.35	97096	1.95	271	0.58	2.64
23507.05	-17821.5	-44.87	97096	1.92	2.3	0.07	0.12
23521.42	-17817.2	-45.27	97096	1.85	18.6	0.23	0.93
23506.09	-17821.8	-44.84	97096	1.78	2.1	0.07	0.07
23476.21	-17830.7	-44.01	97096	1.68	2.1	0.04	0.17
23505.14	-17822	-44.82	97096	1.68	2.2	0.04	0.07
23474.63	-17831.2	-43.97	97096	1.58	5.2	0.15	0.03
23519.12	-17817.9	-45.21	97096	1.58	11.5	0.14	0.41
23519.79	-17817.7	-45.23	97096	1.58	11.5	0.14	0.41
23474.01	-17831.4	-43.95	97096	1.5	6.55	0.19	0.08
23473.05	-17831.6	-43.92	97096	1.41	7.9	0.23	0.13
23478.32	-17830.1	-44.07	97096	1.3	1.9	0.06	0.08
23482.15	-17828.9	-44.18	97096	1.3	2.6	0.03	0.19
23518.16	-17818.1	-45.18	97096	1.02	9.97	0.32	0.25
23469.19	-17833.1	-34.46	97097	46.22	172.1	5.14	5.79
23469.87	-17832.9	-33.75	97097	34.3	157.7	6.23	7.92
23471.23	-17832.5	-32.34	97097	12.46	70.9	1.89	4.24
23470.55	-17832.7	-33.04	97097	9.89	84.1	3.27	5.99
23471.91	-17832.3	-31.63	97097	5.51	312.48	1.08	1.04
23472.35	-17832.2	-31.17	97097	5.18	344	1.14	1
23482.54	-17829.4	-20.58	97097	4.8	6.6	0.07	0.65
23468.71	-17833.2	-34.96	97097	3.7	7.2	0.09	0.26
23466.19	-17833.9	-37.58	97097	3.6	7.8	0.1	0.41
23466.87	-17833.7	-36.87	97097	3.49	8.7	0.14	0.47
23468.23	-17833.3	-35.45	97097	3.07	5.85	0.09	0.26
23481.86	-17829.6	-21.29	97097	3	4.8	0.08	0.49
23464.83	-17834.3	-38.99	97097	2.78	2.1	0.02	0.04
23465.51	-17834.1	-38.28	97097	1.82	2.55	0.05	0.11
23483.22	-17829.3	-19.87	97097	1.61	2.7	0.03	0.26
23467.55	-17833.5	-36.16	97097	1.54	4.65	0.13	0.28
23481.18	-17829.8	-22	97097	1.2	3	0.08	0.32
23480.49	-17830	-22.7	97097	1.17	4.5	0.18	0.3

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23483.9	-17829.1	-19.16	97097	1.04	2.55	0.03	0.16
23505.71	-17820.7	-63.26	97098	73.17	71.1	2.46	0.96
23505.14	-17820.9	-63.01	97098	41.98	52.62	2.3	1.2
23504.26	-17821.2	-62.63	97098	16.02	35.52	1.23	1.32
23493.28	-17824.8	-57.86	97098	8.19	6.3	0.05	0.47
23493.94	-17824.5	-58.14	97098	8.19	6.3	0.05	0.47
23495.48	-17824	-58.81	97098	7.03	6.3	0.09	1.04
23494.6	-17824.3	-58.43	97098	5.76	3.9	0.04	1.26
23492.4	-17825	-57.48	97098	5.66	5.1	0.01	0.05
23502.51	-17821.7	-61.86	97098	3.87	11.4	0.22	1.64
23499.87	-17822.6	-60.72	97098	3.39	33.9	0.09	0.57
23498.99	-17822.9	-60.34	97098	3.33	3	0.04	0.15
23500.75	-17822.3	-61.1	97098	2.98	32.85	0.09	0.82
23503.38	-17821.4	-62.25	97098	2.79	14.55	0.16	1.29
23501.63	-17822	-61.48	97098	2.57	31.8	0.08	1.08
23510.82	-17843.5	-43.42	97099	40.18	101.5	4.92	3.74
23509.83	-17843.4	-43.42	97099	27.7	90.8	2.55	6.69
23501.88	-17842.5	-43.42	97099	22.08	334	8.18	8.85
23502.88	-17842.6	-43.42	97099	21.46	341	8.99	8.02
23500.89	-17842.4	-43.42	97099	15.98	436	10.5	5.72
23508.83	-17843.3	-43.42	97099	14.19	123.5	3.25	3.62
23503.87	-17842.7	-43.42	97099	12.45	377	11.2	11.3
23505.85	-17842.9	-43.42	97099	11.59	145	3.66	2.33
23493.05	-17841.4	-43.42	97099	9.15	84.62	2.89	3.53
23504.86	-17842.8	-43.42	97099	8.72	102.23	2.8	2.83
23507.84	-17843.2	-43.42	97099	6.93	47.8	1.29	1.27
23495.03	-17841.7	-43.42	97099	6.28	27.92	0.46	3.52
23489.47	-17841	-43.42	97099	5.9	20	0.67	1.09
23497.02	-17841.9	-43.42	97099	5.81	168.88	5.61	0.99
23496.03	-17841.8	-43.42	97099	5.16	123.08	4.08	0.94
23488.48	-17840.9	-43.42	97099	4.89	14.7	0.43	0.65
23499.95	-17842.2	-43.42	97099	4.39	138	3.69	0.65
23487.49	-17840.7	-43.42	97099	3.87	9.4	0.18	0.22
23478.55	-17839.7	-43.42	97099	3.81	90.5	2.56	0.47
23506.85	-17843.1	-43.42	97099	3.22	33.7	0.1	0.45
23499	-17842.1	-43.42	97099	3.16	21.81	1.1	0.37
23479.54	-17839.8	-43.42	97099	2.66	50.45	1.43	0.29
23481.53	-17840	-43.42	97099	2.02	3.7	0.13	0.21
23480.54	-17839.9	-43.42	97099	1.51	10.4	0.31	0.11
23486.49	-17840.6	-43.42	97099	1.47	57.7	0.16	0.24
23498.01	-17842	-43.42	97099	1.45	3.86	0.15	0.24
23485.5	-17840.5	-43.42	97099	1.3	47.25	0.25	0.29
23484.51	-17840.4	-43.42	97099	1.13	36.8	0.33	0.35

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23468.44	-17838.5	-39.36	97100	4.39	11.1	0.44	0.34
23473.63	-17839.2	-36.42	97100	3.7	42.3	0.68	0.37
23469.3	-17838.6	-38.87	97100	3.5	16.2	0.52	0.67
23474.49	-17839.3	-35.93	97100	3.42	23.55	0.35	0.2
23466.28	-17838.2	-40.58	97100	3.15	21.3	0.28	0.15
23471.03	-17838.8	-37.89	97100	2.95	5.4	0.31	0.54
23470.17	-17838.7	-38.38	97100	2.61	21.3	0.6	0.99
23471.9	-17838.9	-37.4	97100	2.43	4.57	0.24	0.47
23465.41	-17838.1	-41.07	97100	1.83	11.85	0.18	0.09
23482.37	-17840.2	-53.12	97101	4.76	3.6	0.03	0.07
23493.67	-17841.5	-58.27	97101	4.08	4.8	0.05	0.16
23483.27	-17840.3	-53.53	97101	3.57	2.5	0.02	0.03
23492.77	-17841.4	-57.85	97101	3.41	4.35	0.05	0.27
23498.56	-17842.1	-60.49	97101	2.79	29.24	0.27	0.14
23491.86	-17841.3	-57.44	97101	2.74	3.9	0.06	0.38
23494.58	-17841.6	-58.68	97101	2.57	3.9	0.07	0.13
23479.65	-17839.8	-51.88	97101	2.47	3.6	0.08	0.14
23480.56	-17839.9	-52.29	97101	2.43	3	0.05	0.12
23481.46	-17840	-52.7	97101	2.4	2.4	0.02	0.09
23473.32	-17839.1	-48.99	97101	2.3	3.9	0.06	0.1
23470.61	-17838.7	-47.76	97101	1.95	4.5	0.12	0.17
23490.51	-17841.1	-56.82	97101	1.75	3	0.03	0.14
23491.18	-17841.2	-57.13	97101	1.75	3	0.03	0.14
23495.48	-17841.8	-59.09	97101	1.56	2.55	0.08	0.16
23472.42	-17838.9	-48.58	97101	1.42	3.9	0.09	0.16
23491.78	-17878.9	-42.75	97102	13.1	102	2.69	2.32
23491.18	-17878.1	-42.76	97102	2.19	4.5	0.16	0.19
23469.82	-17849.1	-43.26	97102	1.68	9	0.2	1.54
23494.74	-17882.9	-42.68	97102	1.61	24	0.03	0.06
23495.34	-17883.7	-42.67	97102	1.61	24.3	0.04	0.05
23495.93	-17884.6	-42.65	97102	1.61	24.6	0.04	0.05
23476.94	-17858.8	-43.09	97102	1.06	2.4	0.08	0.32
23477.7	-17859.8	-34.86	97103	8.64	10.2	0.04	0.46
23477.13	-17859	-35.16	97103	7.92	20.85	0.26	0.63
23476.56	-17858.3	-35.46	97103	7.2	31.5	0.48	0.8
23470.88	-17850.6	-38.43	97103	7.17	12.6	0.45	1.53
23471.45	-17851.4	-38.13	97103	5.21	5.1	0.13	0.42
23470.31	-17849.8	-38.73	97103	5.13	9	0.29	0.99
23472.02	-17852.1	-37.84	97103	4.92	4.05	0.12	0.43
23487.92	-17873.6	-29.51	97103	4.9	11.1	0.12	0.24
23486.22	-17871.3	-30.4	97103	4.7	6.9	0.05	0.3
23472.58	-17852.9	-37.54	97103	4.63	3	0.11	0.43
23485.65	-17870.5	-30.7	97103	4.16	6.3	0.03	0.15

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23485.08	-17869.8	-31	97103	3.63	5.7	0	0
23478.83	-17861.3	-34.27	97103	3.43	5.4	0	0.19
23468.04	-17846.8	-39.92	97103	3.38	40.95	0.87	0.34
23469.74	-17849.1	-39.03	97103	3.09	5.4	0.13	0.44
23483.38	-17867.5	-31.89	97103	2.98	5.1	0.11	0.03
23487.35	-17872.9	-29.81	97103	2.65	7.35	0.07	0.17
23479.97	-17862.9	-33.67	97103	2.64	4.2	0.02	0.41
23480.54	-17863.6	-33.38	97103	2.64	4.2	0.02	0.41
23483.95	-17868.2	-31.59	97103	2.54	5.25	0.06	0.05
23466.34	-17844.5	-40.81	97103	2.3	6.3	0.21	0.34
23466.9	-17845.2	-40.51	97103	2.3	6.3	0.21	0.34
23482.81	-17866.7	-32.19	97103	2.19	3	0.01	0.02
23484.51	-17869	-31.29	97103	2.09	5.4	0.01	0.06
23469.18	-17848.3	-39.32	97103	1.89	2.7	0.05	0.16
23468.61	-17847.5	-39.62	97103	1.66	2.25	0.05	0.19
23481.67	-17865.2	-32.78	97103	1.34	6	0.13	1.36
23478.27	-17860.6	-34.57	97103	1.03	2.1	0	0.07
23475.44	-17856.1	-52.64	97104	2.71	2.7	0.01	0.02
23465.24	-17842.8	-46.05	97104	2.13	7.5	0.03	0.06
23465.81	-17843.5	-46.41	97104	1.99	5.25	0.02	0.04
23474.87	-17855.3	-52.27	97104	1.89	3.3	0.02	0.05
23466.38	-17844.2	-46.78	97104	1.85	3	0.01	0.02
23474.3	-17854.6	-51.91	97104	1.53	2.4	0.01	0.04
23464.11	-17841.3	-45.32	97104	1.48	2.1	0.01	0.03
23464.68	-17842	-45.68	97104	1.41	2.1	0.01	0.02
23476	-17856.8	-53.01	97104	1.36	1.45	0.01	0.01
23469.77	-17848.7	-48.98	97104	1.3	1.8	0.01	0.01
23470.34	-17849.4	-49.34	97104	1.27	1.5	0.01	0.02
23463.55	-17840.6	-44.95	97104	1.18	1.8	0.01	0.04
23473.74	-17853.8	-51.54	97104	1.17	1.5	0.01	0.03
23472.53	-17838.8	-45.33	97105	3.46	8.1	0.08	0.16
23481.37	-17839.7	-46.76	97105	3.09	5.1	0.1	0.35
23473.51	-17838.9	-45.49	97105	2.78	6.75	0.06	0.1
23474.49	-17839	-45.65	97105	2.09	5.4	0.04	0.04
23495.11	-17841.1	-49	97105	1.34	3	0.11	0.31
23496.1	-17841.2	-49.15	97105	1.23	4.8	0.02	0.02
23486.28	-17840.2	-47.56	97105	1.2	10.2	0.26	0.35
23478.42	-17839.4	-46.29	97105	1.17	2.1	0.02	0.11
23483.33	-17839.9	-47.08	97105	1.13	3	0.04	0.17
23482.35	-17839.8	-46.92	97105	1.06	3	0.06	0.1
23471.55	-17838.7	-45.17	97105	1.03	2.7	0.02	0.07
23497.08	-17841.3	-49.31	97105	1.02	3.6	0.03	0.06
23479.4	-17839.5	-46.45	97105	1.01	2.55	0.03	0.13

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23422.99	-18118.5	-61.32	97106	12.55	111.5	3.93	11.9
23422.99	-18118.5	-59.32	97106	12.2	187.2	6.27	9.54
23422.99	-18118.5	-57.37	97106	9.67	493	9.61	7.73
23422.99	-18118.5	-58.32	97106	8.6	289	8.52	7.69
23422.99	-18118.5	-60.32	97106	6.66	95.7	3.14	5.02
23422.99	-18118.5	-63.32	97106	6.31	280	8.76	14.4
23422.99	-18118.5	-55.42	97106	3.09	1.8	0.04	0.05
23422.99	-18118.5	-62.32	97106	1.97	57.44	1.81	2.95
23422.99	-18118.5	-54.42	97106	1.46	0.9	0.02	0.03
23436.26	-18110.5	-66.32	97107	29.73	15	0.25	1.84
23437.91	-18109.3	-66.24	97107	26.23	15.9	0.5	7.5
23435.43	-18111	-66.36	97107	23.16	39.23	1.25	0.83
23438.74	-18108.8	-66.2	97107	20.75	21.08	0.54	14.18
23433.77	-18112.1	-66.43	97107	16.83	174.69	5.55	5.42
23432.95	-18112.7	-66.47	97107	16	200.3	6.34	5.7
23434.6	-18111.6	-66.4	97107	13.89	15.75	0.54	0.28
23432.12	-18113.3	-66.51	97107	10.74	145.26	4.59	4
23428.81	-18115.5	-66.66	97107	10.51	99.03	2.87	5.84
23440.4	-18107.7	-66.13	97107	9.87	346	12.7	13.6
23429.63	-18114.9	-66.63	97107	8.34	131.65	3.71	4.24
23430.46	-18114.4	-66.59	97107	7.18	131.87	3.89	5.07
23427.98	-18116.1	-66.7	97107	3.81	362.25	10.53	4.46
23435.13	-18127.6	-66.59	97108	18.17	250	7.98	0.8
23434.26	-18127.1	-66.61	97108	17.35	83.7	1.98	4.4
23452.51	-18137.5	-66.33	97108	12.38	132.5	4.47	2.48
23431.65	-18125.6	-66.64	97108	12.34	346	10.7	3.58
23448.16	-18135	-66.4	97108	9.91	151	4.58	4.5
23450.77	-18136.5	-66.36	97108	8.81	180	5.94	6.78
23454.25	-18138.5	-66.31	97108	8.71	180.5	6.39	7
23436.86	-18128.6	-66.57	97108	8.3	87.3	2.68	11.1
23442.95	-18132.1	-66.48	97108	7.89	50.1	1.5	4.3
23442.08	-18131.6	-66.49	97108	7.82	1070	33.9	0.55
23446.42	-18134	-66.42	97108	7.71	182.5	5.53	5.77
23440.34	-18130.6	-66.51	97108	6.96	71.1	2.11	11.2
23453.38	-18138	-66.32	97108	6.65	110	3.58	9.9
23437.73	-18129.1	-66.55	97108	6.38	147.5	4.69	2.22
23451.64	-18137	-66.35	97108	6.38	275	9.18	19.6
23444.69	-18133.1	-66.45	97108	6.31	35.1	1.22	0.63
23433.39	-18126.6	-66.62	97108	6.27	21	0.76	4.39
23443.82	-18132.6	-66.46	97108	6.17	19.8	0.61	1.69
23449.03	-18135.5	-66.39	97108	5.55	227	7.51	16.4
23435.99	-18128.1	-66.58	97108	5.31	236	7.59	14.6
23445.56	-18133.6	-66.44	97108	5.14	54.9	1.59	4.34

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23449.9	-18136	-66.37	97108	4.35	77.4	2.44	7.38
23439.47	-18130.1	-66.53	97108	3.98	97.5	3.18	9
23432.52	-18126.1	-66.63	97108	3.36	87.9	3.21	5.93
23430.78	-18125.1	-66.66	97108	3.09	88.2	3.02	3.27
23447.29	-18134.5	-66.41	97108	2.19	48.6	1.32	3.5
23441.21	-18131.1	-66.5	97108	1.92	57.9	2.35	8.1
23427.3	-18123.2	-66.71	97108	1.85	5.4	0.11	0.56
23429.91	-18124.7	-66.67	97108	1.17	29.1	0.59	2.82
23423.97	-18124.5	-63.94	97109	34.86	232.17	7.72	6.43
23424.18	-18125.2	-63.35	97109	21.56	694.6	24.06	11.04
23424.4	-18126	-62.76	97109	16.18	619	23.5	8.57
23423.75	-18123.7	-64.52	97109	12.04	8.55	0.25	1.26
23426.54	-18133.8	-56.9	97109	11.79	105.5	3.46	11.7
23425.26	-18129.1	-60.42	97109	10.58	96.49	2.98	2.35
23427.4	-18137	-54.55	97109	10.25	335	8.31	8.42
23427.62	-18137.7	-53.96	97109	6.27	1169	27.26	5.53
23424.61	-18126.8	-62.18	97109	5.04	593	19.9	21.7
23424.83	-18127.6	-61.59	97109	5.04	703.25	23.8	16.33
23426.33	-18133.1	-57.48	97109	4.35	396	13.4	12.2
23423.54	-18122.9	-65.11	97109	3.16	191.64	5.3	3.67
23427.83	-18138.5	-53.38	97109	1.61	417.55	11.77	1.89
23425.47	-18129.9	-59.83	97109	1.32	74.64	2.52	0.71
23425.04	-18128.4	-61	97109	1.06	106.25	3.4	0.93
23426.11	-18132.3	-58.07	97109	1.06	83.52	2.8	2.53
23521.54	-18061.6	-116.44	97110	5.49	13.5	0.33	0.24
23516.19	-18062.2	-109.64	97112	17.86	159.5	0.81	3.24
23512.21	-18062.7	-109.64	97112	3.67	106.5	0.11	0.2
23515.19	-18062.3	-109.64	97112	3.09	227	0.66	0.5
23518.18	-18062	-109.64	97112	2.57	4.5	0.04	0.1
23513.2	-18062.5	-109.64	97112	2.26	6.6	0.13	0.4
23514.2	-18062.4	-109.64	97112	1.78	6.6	0.05	0.16
23519.17	-18061.9	-109.64	97112	1.71	3	0.14	0.37
23517.18	-18062.1	-109.64	97112	1.1	3.6	0.08	0.45
23518.27	-18062.1	-108.74	97113	46.66	388	10.6	0.74
23519.23	-18061.9	-108.99	97113	34.53	271	9.48	5.69
23516.35	-18062.3	-108.23	97113	21.6	394	11	1.33
23517.31	-18062.2	-108.48	97113	16.59	263	5.15	1.45
23513.48	-18062.7	-107.47	97113	14.19	294	7.43	0.47
23512.52	-18062.8	-107.21	97113	13.51	82.8	2	0.12
23508.68	-18063.3	-106.19	97113	5.01	5.1	0.32	0.17
23510.6	-18063.1	-106.7	97113	3.84	4.2	0.23	0.16
23514.44	-18062.6	-107.72	97113	2.54	9.6	0.16	0.25
23515.39	-18062.4	-107.97	97113	1.99	5.1	0.15	0.32

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23518.91	-18085.4	-112.78	97114	14.95	38.55	1.83	4.34
23518.91	-18085.4	-115.78	97114	2.37	26.1	0.16	1.09
23523.4	-18083.3	-116.17	97115	31.23	336.29	4.42	2.38
23520.69	-18084.7	-112.39	97115	24.31	83.7	2.87	5.76
23521.25	-18084.4	-113.17	97115	20.95	79.8	2.81	5.22
23520.13	-18085	-111.61	97115	16.11	28.93	0.9	3
23522.37	-18083.8	-114.73	97115	11.79	43.2	0.94	0.9
23522.93	-18083.6	-115.51	97115	10.83	76.35	1.11	1.34
23523.85	-18083.1	-116.79	97115	1.3	69.3	0.27	0.35
23516.8	-18086.1	-109.02	97116	14.67	24	0.56	2.61
23515.81	-18086.2	-109.02	97116	3.94	15.6	0.36	0.45
23516.36	-18086.2	-108.42	97117	19.7	52.92	2.1	3.42
23509.84	-18086.7	-105.94	97117	17.42	62.7	1.6	0.17
23515.43	-18086.3	-108.06	97117	16.21	21.24	0.62	1.08
23514.5	-18086.3	-107.71	97117	15.69	13.05	0.28	0.34
23508.91	-18086.8	-105.59	97117	12.86	27.42	0.93	0.76
23507.18	-18087	-104.93	97117	12.13	51.09	1.32	4.66
23513.57	-18086.4	-107.35	97117	9.77	23.64	0.55	0.71
23512.63	-18086.5	-107	97117	9.75	51.24	1.58	2.65
23511.7	-18086.6	-106.65	97117	8.16	13.8	0.37	0.74
23507.97	-18086.9	-105.23	97117	6.34	11.25	0.35	1.38
23515.21	-18091.3	-110.04	97118	21.87	161	3.81	1.82
23517.41	-18088	-110.04	97118	13.23	23.7	0.09	1.5
23515.76	-18090.5	-110.04	97118	4.8	67.8	1.64	0.44
23516.31	-18089.6	-110.04	97118	4.63	14.7	0.88	3.41
23507.63	-18103.6	-100.24	97119	25.65	235.75	6.68	7.95
23514.14	-18093.3	-105.98	97119	21.74	265.5	5.51	8.27
23517.03	-18088.7	-108.54	97119	19.56	125.31	3.93	4.06
23508.11	-18102.8	-100.67	97119	18.1	214.5	5.77	4.38
23513.65	-18094	-105.56	97119	17.93	209.5	4.63	7.18
23516.55	-18089.4	-108.11	97119	17.76	121	3.74	3.76
23517.51	-18087.9	-108.96	97119	17.01	98.2	5.17	6.78
23510.52	-18099	-102.8	97119	17.01	155	4.72	4.73
23514.62	-18092.5	-106.41	97119	16.59	150.25	3.16	11.91
23516.06	-18090.2	-107.68	97119	14.68	67.4	2.29	2.34
23506.38	-18105.6	-99.14	97119	14.16	357	12.3	3.5
23507.15	-18104.4	-99.82	97119	13.21	321.29	9.83	8.77
23510.04	-18099.8	-102.37	97119	12.72	85.8	2.38	2.23
23506.67	-18105.1	-99.39	97119	11.73	365.5	11.9	6.03
23515.58	-18091	-107.26	97119	11.59	13.8	0.84	0.92
23515.1	-18091.7	-106.83	97119	11.18	116.5	2.74	9.82
23512.21	-18096.3	-104.28	97119	5.73	11.7	0.35	1.19
23510.88	-18098.4	-103.11	97119	2.4	9.3	0.56	0.23

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23506.09	-18106	-98.88	97119	1.34	15.9	2.18	0.21
23512.69	-18095.6	-104.71	97119	1.17	2.1	0.04	0.06
23520.74	-18085.3	-111.55	97120	21.84	236	6.35	2.44
23522.54	-18085.1	-113.95	97120	20.98	22.5	1.12	2.73
23523.14	-18085	-114.74	97120	20.57	13.5	0.5	2.13
23523.74	-18085	-115.54	97120	19.82	48.9	1.7	4.62
23521.94	-18085.2	-113.15	97120	16.46	27.6	1.79	3.73
23525.32	-18084.8	-117.66	97120	15.91	142.5	3.41	3.65
23521.34	-18085.2	-112.35	97120	13.95	88.5	2.05	13.8
23524.33	-18084.9	-116.34	97120	11.46	51.99	2.25	1.83
23524.93	-18084.9	-117.14	97120	3.56	24.24	0.59	0.9
23517.61	-18108.9	-110.65	97121	9.7	58.8	2.03	7.3
23517.07	-18109.1	-110.65	97121	9.7	58.8	2.03	7.3
23516.54	-18109.2	-110.65	97121	4.11	5.7	0.17	1.35
23515.56	-18109.4	-110.65	97121	1.69	3	0.13	0.8
23519.98	-18052.2	-109.77	97122	32.19	192	4.13	9.04
23518.07	-18049.9	-109.77	97122	32.06	195.5	5.07	12.4
23517.59	-18049.3	-109.77	97122	30.82	559	8.47	4.8
23520.62	-18052.9	-109.77	97122	26.57	102	2.08	5.44
23519.34	-18051.4	-109.77	97122	16.63	226	6.02	6.98
23518.7	-18050.6	-109.77	97122	16.29	287	4.45	6.5
23521.26	-18053.7	-109.77	97122	6.66	27.84	0.6	2.13
23516.47	-18047.9	-109.77	97122	4.65	29.88	0.48	0.66
23517.11	-18048.7	-109.77	97122	2.67	8.7	0.13	0.37
23521.9	-18054.5	-109.77	97122	1.76	252.09	0.79	0.64
23868.27	-18675.3	-211.33	97123	8.23	442	13.5	15
23869.21	-18674.2	-212.73	97123	8.09	668	20.7	5.44
23867.33	-18676.3	-209.93	97123	8.02	506	14.2	12.5
23867.8	-18675.8	-210.63	97123	8.02	506	14.2	12.5
23868.74	-18674.7	-212.03	97123	8.02	539	16.5	9.47
23660.02	-18288.9	-214.41	97124	12.09	24.9	2.77	2.36
23658.2	-18291.2	-214.41	97124	6.48	24	0.42	0.26
23657.59	-18292	-214.41	97124	2.4	5.7	0.09	0.03
23664.86	-18282.5	-214.41	97124	1.68	3	0.2	0.3
23664.26	-18283.3	-214.41	97124	1.68	3	0.2	0.3
23656.99	-18292.8	-214.41	97124	1.21	2.95	0.05	0.02
23663.65	-18284.1	-214.41	97124	1.1	19.2	0.51	1.06
23663.05	-18284.9	-214.41	97124	1.1	19.2	0.51	1.06
23662.44	-18285.7	-214.41	97124	1.03	2.4	0.11	0.41
23673.47	-18305.2	-214.62	97125	11.09	30	0.96	4.18
23674.21	-18304.5	-214.62	97125	10.32	20.25	0.74	1.93
23680.14	-18299.1	-214.62	97125	9.67	291	8.39	5.52
23677.17	-18301.8	-214.62	97125	8.5	45.6	1.36	4.23

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23676.43	-18302.5	-214.62	97125	8.4	184	5.91	3.33
23672.73	-18305.8	-214.62	97125	7.66	79.6	2.61	4.49
23671.99	-18306.5	-214.62	97125	7.57	80.35	2.64	1.4
23677.92	-18301.1	-214.62	97125	7.27	25.5	0.74	8.95
23680.88	-18298.4	-214.62	97125	6.55	68.1	1.94	2.49
23675.69	-18303.1	-214.62	97125	5.23	57.51	1.83	1.16
23669.76	-18308.5	-214.62	97125	4.87	28.5	1.47	2.1
23670.5	-18307.8	-214.62	97125	4.39	27	0.99	0.81
23674.95	-18303.8	-214.62	97125	4.32	7.76	0.31	1.26
23679.4	-18299.8	-214.62	97125	3.46	10.8	0.29	0.78
23669.02	-18309.2	-214.62	97125	3.2	18.59	0.97	1.37
23678.66	-18300.5	-214.62	97125	3.12	9.6	0.22	0.49
23671.25	-18307.2	-214.62	97125	3.12	14.25	0.5	0.42
23682.95	-18327.4	-215.29	97126	33.94	127	4.63	4.69
23682.12	-18328	-215.29	97126	33.94	127	4.63	4.69
23668.84	-18336.9	-215.29	97126	20.8	219.75	7.95	4.27
23669.67	-18336.4	-215.29	97126	20.32	159.85	5.93	5.57
23681.29	-18328.5	-215.29	97126	19.89	221	7.34	3.75
23684.61	-18326.3	-215.29	97126	18.86	787	24.2	0.79
23671.33	-18335.2	-215.29	97126	18.62	229.8	7.93	6.31
23670.5	-18335.8	-215.29	97126	18.51	81.15	3.37	7.43
23673.82	-18333.6	-215.29	97126	17.49	125.5	3.85	9.2
23685.44	-18325.8	-215.29	97126	16.72	780.8	23.56	1.44
23677.97	-18330.8	-215.29	97126	12.93	140.5	4.48	4.74
23668.01	-18337.5	-215.29	97126	11.64	128.88	4.77	2.55
23680.46	-18329.1	-215.29	97126	10.9	412	12.7	6.66
23678.8	-18330.2	-215.29	97126	8.85	337	10.1	6.53
23686.27	-18325.2	-215.29	97126	8.17	763.8	20.88	6.07
23687.1	-18324.6	-215.29	97126	7.06	675.89	17.35	12.08
23672.16	-18334.7	-215.29	97126	6.59	107.4	3.45	2.87
23679.63	-18329.7	-215.29	97126	4.77	593	19.3	14.1
23674.65	-18333	-215.29	97126	4.71	40.63	1.28	1.51
23672.99	-18334.1	-215.29	97126	4.22	42	1.26	2.63
23664.69	-18339.7	-215.29	97126	3.74	5.4	0.18	0.39
23675.48	-18332.5	-215.29	97126	3.29	31.2	1	0.66
23663.86	-18340.3	-215.29	97126	1.88	2.8	0.09	0.2
23667.18	-18338	-215.29	97126	1.29	7.68	0.28	0.53
23697.45	-18319.9	-215.42	97127	6.92	324.25	9.48	13.36
23696.59	-18320.4	-215.42	97127	6.71	221.63	5.55	12.4
23695.73	-18320.9	-215.42	97127	6.55	193.5	4.46	11.7
23698.32	-18319.4	-215.42	97127	6.07	379	11.5	9.93
23694	-18321.9	-215.42	97127	3.87	273	8.44	11.9
23694.86	-18321.4	-215.42	97127	3.87	273	8.44	11.9

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23700.04	-18318.4	-215.42	97127	2.23	281	8.07	1.66
23700.91	-18317.9	-215.42	97127	2.23	281	8.07	1.66
23687.77	-18347.7	-210.7	97128	3.15	18.9	0.47	0.15
23687.77	-18347.7	-209.7	97128	3.15	18.9	0.47	0.15
23687.77	-18347.7	-208.7	97128	3.15	18.9	0.47	0.15
23687.8	-18347.3	-223.3	97129	4.49	80.7	2.46	1.55
23873.76	-18670.8	-218.13	97130	12.65	591	11.1	3.6
23874.23	-18670.3	-218.83	97130	12.05	526	13.2	5.12
23874.69	-18669.7	-219.52	97130	9.81	678	13.95	4.59
23870.99	-18674.2	-213.98	97130	8.64	361	13	5.43
23872.38	-18672.5	-216.05	97130	8.23	334	14.1	16
23871.45	-18673.6	-214.67	97130	8.16	332	11.75	7.3
23875.04	-18669.3	-220.04	97130	8.16	895	12.6	2.55
23870.06	-18675.3	-212.59	97130	8.06	46.8	0.95	2.65
23870.53	-18674.7	-213.28	97130	8.06	46.8	0.95	2.65
23871.91	-18673.1	-215.36	97130	7.68	303	10.5	9.18
23872.84	-18671.9	-216.75	97130	7.41	323.5	11.73	16.15
23869.6	-18675.8	-211.9	97130	7.2	257	9.19	12.5
23873.3	-18671.4	-217.44	97130	6.58	313	9.37	16.3
23867.01	-18678.9	-208.02	97130	3.46	384	11.7	7.76
23867.43	-18678.4	-208.64	97130	3.46	384	11.7	7.76
23784.8	-18592.8	-207.69	97131	10.22	269	8.84	13.2
23786.26	-18592.2	-207.69	97131	7.31	107.61	4.3	16.46
23785.32	-18592.6	-207.69	97131	6.87	130.23	4.15	6.6
23793.79	-18589.5	-207.69	97131	5.97	117.41	3.12	7.05
23787.2	-18591.9	-207.69	97131	4.87	563	22.1	6.85
23788.15	-18591.6	-207.69	97131	4.58	503	19.58	10.21
23794.74	-18589.2	-207.69	97131	4.35	85.34	2.28	5.13
23791.91	-18590.2	-207.69	97131	3	284.57	11.13	20.37
23789.09	-18591.2	-207.69	97131	2.49	375.4	14.9	23.34
23790.97	-18590.5	-207.69	97131	2.2	304	11.62	17.14
23792.85	-18589.9	-207.69	97131	1.64	135.83	5.36	17.82
23794.82	-18577.9	-209.6	97132	34.83	80.1	2.67	9.24
23794.82	-18577.9	-214.6	97132	30.36	156.4	5.59	3.64
23794.82	-18577.9	-215.6	97132	29.74	139.22	5.21	2.78
23794.82	-18577.9	-216.6	97132	14	70.74	2.51	4.11
23794.82	-18577.9	-218.6	97132	12.35	132.2	4.37	4.7
23794.82	-18577.9	-217.6	97132	9.52	40.14	1.37	1.95
23794.82	-18577.9	-211.6	97132	8.02	123	4.44	3.42
23794.82	-18577.9	-210.6	97132	7.95	157.5	5.84	3.27
23794.82	-18577.9	-224.17	97132	7.82	311	8.31	10.5
23794.82	-18577.9	-219.6	97132	7.51	390.4	12.7	11.91
23794.82	-18577.9	-223.6	97132	7.16	191.05	5.52	12.75

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23794.82	-18577.9	-213.6	97132	6.67	41	1.47	0.84
23794.82	-18577.9	-222.6	97132	6.09	97.58	3.81	15.08
23794.82	-18577.9	-221.6	97132	3.98	230	9.2	15.5
23794.82	-18577.9	-220.6	97132	3.43	356.4	11.68	9.79
23794.82	-18577.9	-212.6	97132	2.7	39.75	1.45	0.89
23762.99	-18530.3	-208.37	97133	17.38	188.5	6.86	8.52
23764.94	-18529.9	-208.37	97133	16.11	60.3	2.21	0.62
23763.97	-18530.1	-208.37	97133	14.95	93.3	3.16	0.77
23756.16	-18531.8	-208.37	97133	9.48	149.9	5.2	16.14
23759.09	-18531.2	-208.37	97133	7.58	58.2	2.24	12.2
23757.13	-18531.6	-208.37	97133	7.4	99.3	3.58	11.98
23755.18	-18532.1	-208.37	97133	4.04	68.66	2.45	7.17
23762.01	-18530.5	-208.37	97133	3.94	429	18.2	15.5
23758.11	-18531.4	-208.37	97133	3.69	23.76	0.98	7.76
23761.04	-18530.8	-208.37	97133	3.19	179.5	6.95	6.97
23760.06	-18531	-208.37	97133	3.12	48.6	2.13	10.7
23660.78	-18294.5	-199.14	97134	21.45	87.56	2.63	5.71
23661.45	-18294.2	-198.44	97134	21.15	121.08	3.84	9.52
23658.79	-18295.3	-201.23	97134	19.73	100.36	2.98	6.43
23658.12	-18295.6	-201.92	97134	18.03	73.56	2.52	6.13
23659.45	-18295	-200.53	97134	16.77	158.8	4.14	6.43
23660.12	-18294.8	-199.84	97134	16.73	124.14	3.22	4.46
23662.11	-18293.9	-197.75	97134	13.81	68.64	2.34	7.21
23657.46	-18295.8	-202.62	97134	13.78	79.8	2.64	6.26
23656.79	-18296.1	-203.31	97134	12.34	73.5	2.26	5.57
23655.46	-18296.7	-204.7	97134	9.26	47.1	1.24	2.8
23656.13	-18296.4	-204.01	97134	9.26	47.1	1.24	2.8
23664.11	-18293.1	-195.66	97134	3.61	3.66	0.11	0.28
23664.77	-18292.8	-194.97	97134	3.21	2.7	0.09	0.15
23662.78	-18293.7	-197.05	97134	2.74	25.8	0.7	1.53
23663.44	-18293.4	-196.36	97134	1.43	7.8	0.24	0.64
23866.91	-18679.1	-207.24	97135	3.5	924	37.1	1.92
23867.79	-18678.1	-206.04	97135	1.3	542	14.8	2.76
23654.09	-18297	-198.84	97136	39.98	135.32	3.88	2.21
23654.09	-18297	-197.84	97136	39.26	95.04	2.72	2.52
23654.09	-18297	-199.84	97136	33.53	67.94	1.92	1.25
23654.09	-18297	-195.84	97136	28.63	85.04	2.99	2.73
23654.09	-18297	-196.84	97136	27.25	89.79	2.68	2.01
23654.09	-18297	-194.84	97136	18.53	30.63	1.17	1.63
23654.09	-18297	-203.84	97136	13.51	46.5	1.4	10.1
23654.09	-18297	-193.84	97136	12.36	20.22	0.59	0.22
23654.09	-18297	-200.84	97136	12.22	34.02	1.03	1.8
23654.09	-18297	-202.84	97136	9.31	66.84	1.95	7.01

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23654.09	-18297	-201.84	97136	7.15	55.74	1.65	3.21
23654.09	-18297	-192.84	97136	3.51	33	1.06	0.27
23664.71	-18325.1	-208.23	97137	15.09	234.4	7.47	6.2
23664.71	-18325.1	-207.23	97137	14.95	52.8	2.03	4.81
23664.71	-18325.1	-211.23	97137	12.8	202.78	6.52	4.96
23664.71	-18325.1	-209.23	97137	12	319.37	9.86	5.75
23664.71	-18325.1	-216.23	97137	9.33	40.2	1.13	1.88
23664.71	-18325.1	-212.23	97137	5.87	82.27	2.61	2.22
23664.71	-18325.1	-210.23	97137	4.49	93.9	2.78	1.48
23691.26	-18420.6	-204.08	97138	55.47	52.2	1.78	1.49
23691.83	-18420.2	-203.34	97138	38.75	92.19	3.27	3.18
23690.12	-18421.3	-205.57	97138	32.42	31.32	1.6	1.41
23690.69	-18420.9	-204.82	97138	31.04	40.44	1.77	1.21
23692.4	-18419.9	-202.59	97138	30.38	41.7	1.3	8.95
23689.55	-18421.6	-206.31	97138	23.41	131.73	4.44	3.79
23716.84	-18462.9	-204.76	97139	64.46	31.2	1.07	1.49
23717.47	-18462.5	-204.09	97139	39.6	29.1	1.1	0.32
23716.21	-18463.2	-205.43	97139	33.7	116	4.15	5.89
23715.58	-18463.6	-206.11	97139	19.06	107.5	3.78	1.7
23719.37	-18461.3	-202.06	97139	10.42	2.4	0.03	0
23718.74	-18461.7	-202.74	97139	9.4	2.28	0.03	0
23714.95	-18464	-206.78	97139	9.39	449	14.7	4.12
23729.13	-18488.2	-208.48	97140	16.25	14.9	0.4	10.1
23731.84	-18486.9	-208.48	97140	15.12	141	4.93	5.37
23730.94	-18487.3	-208.48	97140	14.19	76.15	2.77	3.43
23730.03	-18487.7	-208.48	97140	13.27	11.3	0.61	1.5
23728.23	-18488.6	-208.48	97140	12.43	55.8	1.81	11.32
23727.33	-18489	-208.48	97140	8.61	96.7	3.22	12.55
23733.64	-18486	-208.48	97140	2.09	18.3	0.55	2.58
23734.54	-18485.6	-208.48	97140	2.09	18.3	0.55	2.58
23736.34	-18484.7	-208.48	97140	1.61	7.4	0.24	0.27
23737.25	-18484.3	-208.48	97140	1.61	7.4	0.24	0.27
23794.43	-18642.2	-188.66	97141	14.33	132.5	4.9	10.6
23794.99	-18641.7	-188.66	97141	12.86	174	6.48	10.62
23795.78	-18641.1	-188.66	97141	6.96	340	12.8	10.7
23802.58	-18634.4	-188.65	97142	19.27	386	15	12.8
23802.13	-18634.8	-188.65	97142	15.91	308	13.55	11.55
23801.38	-18635.4	-188.65	97142	12.55	230	12.1	10.3
23800.63	-18636.1	-188.65	97142	8.23	318	13.1	7.48
23783.31	-18600.1	-188.93	97143	7.27	199	5.96	4.57
23768.65	-18547.1	-189.59	97144	15.02	156.5	6.43	3.5
23767.69	-18548.7	-189.59	97144	11.93	140	5.73	4.49
23768.21	-18547.8	-189.59	97144	9.37	248.75	10.18	10.88

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23767.17	-18549.5	-189.59	97144	8.54	311	13	1.07
23765.27	-18552.7	-189.59	97144	6.69	206	8.29	11.4
23764.23	-18554.4	-189.59	97144	6.24	159	6.92	6.06
23765.78	-18551.8	-189.59	97144	5.97	451	13.6	7.57
23764.75	-18553.6	-189.59	97144	5.55	90.6	3.35	21.1
23763.72	-18555.3	-189.59	97144	4.8	151	6.51	14.4
23766.17	-18551.2	-189.59	97144	2.54	474	18	4.26
23769.08	-18546.4	-189.59	97144	2.54	3	0.08	0.06
23770.12	-18544.6	-189.59	97144	1.87	11.31	0.27	0.51
23702.21	-18472.9	-189.74	97145	7.92	206	7.03	10.8
23669.19	-18398.3	-193.81	97146	33.46	194.5	6.77	4.3
23668.28	-18398.7	-193.81	97146	21.33	69	2.59	1.62
23670.1	-18397.9	-193.81	97146	16.05	65.4	3.04	4.06
23667.37	-18399.1	-193.81	97146	11.79	325	11.8	8.35
23661.91	-18401.6	-193.81	97146	8.02	570.8	19.09	5.55
23662.82	-18401.2	-193.81	97146	7.18	378.1	11.81	12.15
23665.55	-18399.9	-193.81	97146	5.83	160.11	6.13	15.45
23666.46	-18399.5	-193.81	97146	4.39	221	8.63	21.9
23661	-18402	-193.81	97146	3.6	263.7	8.09	5.41
23663.73	-18400.8	-193.81	97146	2.3	91.05	2.63	5.16
23664.64	-18400.3	-193.81	97146	2.28	35.53	1.12	8.34
23626.37	-18235.3	-200.74	97147	13.71	178.5	5.85	6.6
23626.37	-18235.3	-197.74	97147	5.57	168.03	5.59	5.55
23626.37	-18235.3	-201.74	97147	4.16	53.76	1.81	2.02
23626.37	-18235.3	-196.74	97147	2.95	55.5	1.76	1.81
23626.37	-18235.3	-199.74	97147	2.4	11.7	0.51	0.47
23626.37	-18235.3	-195.74	97147	2.16	30.6	0.98	1.2
23626.37	-18235.3	-194.74	97147	1.37	5.7	0.2	0.59
23641.55	-18240.3	-206.29	97148	1.99	11.8	0.31	0.33
23640.86	-18240	-205.61	97148	1.6	8.25	0.25	0.2
23642.92	-18240.7	-207.67	97148	1.41	3.8	0.09	0.21
23643.61	-18241	-208.35	97148	1.41	3.8	0.09	0.21
23640.18	-18239.8	-204.92	97148	1.2	4.7	0.18	0.07
23639.49	-18239.6	-204.23	97148	1.13	22.3	0.43	0.1
23763.69	-18552.9	-178.21	97150	22.16	115.22	5.05	6.4
23763.69	-18552.9	-193.21	97150	19.17	65.4	2.49	11.4
23763.69	-18552.9	-194.21	97150	16.9	237	8.02	0.53
23763.69	-18552.9	-192.21	97150	16.87	183	7.31	11.55
23763.69	-18552.9	-179.21	97150	9.38	58.72	2.59	3.11
23763.69	-18552.9	-191.21	97150	5.49	145	6.12	10.65
24030.48	-18187	-341.81	D351A	51.36	57.3	1.84	0.81
24030.18	-18187	-342.76	D351A	50.46	140	4.48	2.91
24031.07	-18187.1	-339.9	D351A	48.36	85.3	3.2	3.19

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24030.77	-18187	-340.85	D351A	44.3	120	3.79	0.7
24029.88	-18187	-343.72	D351A	37.85	102	3.19	0.55
24029.59	-18187	-344.67	D351A	18.84	114	4.18	6.21
24031.36	-18187.1	-338.94	D351A	13	237	8.83	7.33
24029.29	-18187	-345.63	D351A	12.9	57.3	1.94	11.3
24031.95	-18187.1	-337.03	D351A	4.84	149	3.73	9.69
24031.66	-18187.1	-337.99	D351A	3.94	257	9.54	9.34
24022	-18186.5	-368.49	D351A	3.69	0.2	0	0.01
24021.69	-18186.5	-369.44	D351A	3.69	0.2	0	0.01
24036.94	-18187.1	-320.78	D351A	3.4	46.1	1.43	0.72
24037.23	-18187.1	-319.82	D351A	2.48	4.1	0.08	0.03
24028.69	-18187	-347.54	D351A	2.04	603	23.7	1.08
24006.71	-18184.6	-413.94	D351A	1.89	77.8	1.31	0.03
24028.99	-18187	-346.58	D351A	1.8	816	27.4	0.77
23994.57	-18207.3	-338.11	D352	12.55	251.9	9.94	11.73
23994.23	-18207.3	-339.98	D352	4.77	377	13.2	7.57
23994.39	-18207.3	-339.1	D352	3.83	441.8	16.62	13.18
23994.74	-18207.4	-337.13	D352	3.24	325	12.4	13.8
23866.7	-18372	-395.95	D353	26.79	95.64	3.45	3.53
23866.53	-18371.9	-396.92	D353	22.3	52.93	2.08	5.94
23873.97	-18377	-353.25	D353	19.89	245.31	9.47	5.36
23873.81	-18376.9	-354.23	D353	18.08	489.16	19.54	10.06
23874.14	-18377.1	-352.27	D353	16.41	197.4	6.65	8.26
23864.51	-18370.4	-408.66	D353	15.09	34.24	1.3	4.42
23864.34	-18370.3	-409.64	D353	14.7	33.5	1.43	4.78
23864.18	-18370.1	-410.62	D353	14.7	33.5	1.43	4.78
23864.68	-18370.5	-407.68	D353	14.53	38.62	1.21	3.71
23866.36	-18371.7	-397.9	D353	14.35	38.75	1.32	5.35
23864.85	-18370.6	-406.71	D353	12.9	43.4	1.35	3.45
23874.3	-18377.2	-351.29	D353	12.8	310.2	10.33	13.82
23865.19	-18370.9	-404.75	D353	11.61	39.92	1.24	3.23
23866.19	-18371.6	-398.88	D353	11.19	41.5	1.42	6.18
23866.87	-18372.1	-394.97	D353	10.87	29.88	1.07	6.53
23867.54	-18372.6	-391.05	D353	10.65	41	3.11	7.19
23865.02	-18370.8	-405.73	D353	9.28	19.88	0.6	1.43
23874.47	-18377.3	-350.31	D353	8.99	382.2	13.82	16.84
23865.35	-18371	-403.77	D353	8.84	24.08	0.95	3.15
23866.03	-18371.5	-399.86	D353	8.81	36.3	1.11	4.14
23867.37	-18372.5	-392.03	D353	8.68	25.26	1.06	5.66
23865.86	-18371.4	-400.84	D353	7.07	24.54	0.67	6.04
23865.52	-18371.1	-402.79	D353	7.07	25.74	0.89	2.84
23872.81	-18376.2	-360.11	D353	6.39	253	9.51	14.6
23874.63	-18377.4	-349.33	D353	6.33	528	20.1	18.4

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23873.48	-18376.7	-356.19	D353	6.27	449	16.9	25.3
23867.2	-18372.3	-393.01	D353	6.11	42.71	1.29	3.6
23865.69	-18371.2	-401.81	D353	6	29.2	0.78	4.72
23867.04	-18372.2	-393.99	D353	5.03	31.8	1.16	3.53
23872.98	-18376.3	-359.13	D353	4.18	287.65	11.22	16.22
23873.64	-18376.8	-355.21	D353	3.98	424.52	16.47	23.28
23873.31	-18376.6	-357.17	D353	2.84	347.68	13.84	28.22
23872.07	-18375.7	-364.47	D353	2.67	2	0.03	0.03
23871.91	-18375.6	-365.45	D353	2.67	2	0.03	0.03
23863.47	-18369.6	-414.73	D353	1.89	0.9	0	0
23863.3	-18369.5	-415.7	D353	1.89	0.9	0	0
23873.14	-18376.5	-358.15	D353	1.39	320.4	13.01	21.85
24117.31	-18193.2	-383.38	D354	3.36	20.19	0.92	1.58
24117.11	-18193.2	-384.36	D354	2.33	31.6	2.78	0.96
24124.52	-18140.5	-328.69	D355	46.39	99.2	3.53	2.22
24124.9	-18140.3	-330.63	D355	41.07	62.2	2.3	3.83
24124.71	-18140.4	-329.66	D355	38.06	42.3	1.55	3
24125.09	-18140.1	-331.6	D355	10.18	110.37	3.93	15.33
24125.27	-18140	-332.57	D355	8.94	156.84	5.79	11.98
24123.2	-18141.5	-321.88	D355	7.72	121.69	4.25	3
24122.45	-18142.1	-318	D355	5.82	2.56	0.04	2.57
24123.77	-18141.1	-324.8	D355	5.44	97.93	3.35	5.42
24123.39	-18141.4	-322.86	D355	5.38	96.88	3.47	2.71
24125.46	-18139.8	-333.55	D355	4.75	88.75	3.32	5.04
24122.26	-18142.2	-317.03	D355	4.69	2.28	0.03	3.23
24123.58	-18141.3	-323.83	D355	4.41	94.12	3.38	3.93
24122.63	-18142	-318.97	D355	4.22	1.4	0.02	0.09
24122.82	-18141.8	-319.94	D355	2.43	41.66	1.62	0.11
24195.27	-18224.2	-452.14	D357	1.75	1.84	0.02	0.12
24267.67	-18227.5	-482.87	D359	19.78	25.52	0.86	4.6
24267.61	-18227.6	-483.87	D359	14.9	17.5	0.67	3.24
24267.55	-18227.6	-484.86	D359	5.62	12.5	0.57	1.13
24267.73	-18227.5	-481.87	D359	2.04	35.83	1.15	1.41
24011.68	-18265.8	-362.46	D360	27.12	150.5	5.51	10.5
24012.51	-18265.2	-357.56	D360	9.94	450	14	12.7
24011.84	-18265.7	-361.48	D360	7.03	200	7.87	15.1
24011.51	-18265.9	-363.43	D360	5.45	141.5	4.76	9.38
24011.4	-18266	-364.07	D360	5.45	141.5	4.76	9.38
24012.01	-18265.5	-360.5	D360	2.61	298	11.3	15.1
24012.18	-18265.4	-359.52	D360	2.02	567	20.6	14.3
24012.35	-18265.3	-358.54	D360	1.2	644	24.3	23.8
23984.35	-18005.6	-247.34	D501	32.4	107	3.03	8.3
23985.57	-18004.3	-250.9	D501	27.24	211.6	4.96	13.32

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23985.27	-18004.6	-250.01	D501	22.97	44.62	1.41	9.07
23984.96	-18004.9	-249.12	D501	19.49	29.1	0.79	1.89
23984.66	-18005.3	-248.23	D501	17.45	189.32	5.52	25.35
23986.17	-18003.6	-252.65	D501	11.07	753.22	21.06	13.23
23985.88	-18003.9	-251.79	D501	10.29	531.54	14.51	23.2
23980.23	-18010.1	-235.33	D501	4.19	73.72	2.08	6.11
23979.92	-18010.5	-234.44	D501	3.39	63.05	1.83	5.21
23983.9	-18006.1	-246.02	D501	2.09	2.28	0.04	0.03
23984.12	-18005.9	-246.68	D501	1.9	1.8	0.04	0.02
23982.67	-18007.5	-242.46	D501	1.38	0.2	0	0
23982.98	-18007.1	-243.35	D501	1.05	0.2	0	0
24032.18	-17961.5	-265.77	D503	5.12	4.8	0.26	0.06
24028.91	-17964.6	-261.77	D503	3.92	12.7	0.75	0.73
24029.45	-17964.1	-262.44	D503	3.32	12.4	0.28	0.15
24030	-17963.6	-263.1	D503	2.28	5.56	0.31	0.15
24030.54	-17963.1	-263.77	D503	2.16	4.8	0.31	0.15
24028.37	-17965.1	-261.1	D503	1.59	9	0.5	0.44
23949.77	-17999.7	-230.76	D505	30.05	89.79	2.37	7.51
23949.87	-18000.2	-229.92	D505	20.94	24.83	0.74	10.6
23949.98	-18000.6	-229.05	D505	13.96	90.5	3.03	7.25
23949.55	-17998.7	-232.47	D505	3.92	3.07	0.03	0.02
23950.04	-18000.9	-228.56	D505	1.22	7.8	0.28	0.23
23950.1	-18001.2	-228.07	D505	1.05	5.82	0.21	0.18
23982.44	-18080	-258.05	D506	10.27	121.92	2.97	14.99
23982.67	-18080.4	-258.91	D506	8.84	363.45	10.2	25.17
24003.86	-18130.6	-342.5	D506	8	0.2	0.01	0.01
24003.75	-18130.3	-342.04	D506	7.04	0.2	0.01	0.01
23983.25	-18081.7	-261.12	D506	3.18	540	25	18.9
23982.89	-18080.9	-259.76	D506	3.14	810.44	24.7	24.67
23983.12	-18081.4	-260.61	D506	2.97	615.02	25.44	20.13
23982.22	-18079.5	-257.2	D506	2.86	902	25.3	14.5
24033.74	-18053	-281.92	D508	43.08	233	8.53	4.81
24035.76	-18056.5	-281.92	D508	42.5	73.8	2.54	2.78
24029.71	-18046.1	-281.92	D508	31.68	170	5.56	8.69
24035.26	-18055.6	-281.92	D508	31.2	186	5.89	9.41
24036.27	-18057.4	-281.92	D508	27.66	27.8	1.1	0.67
24033.24	-18052.2	-281.92	D508	27.56	111	3.29	5.47
24030.72	-18047.9	-281.92	D508	26.9	83.7	2.57	11.6
24034.25	-18053.9	-281.92	D508	22.7	213	6.54	9.19
24031.73	-18049.6	-281.92	D508	21.7	31	1.04	12.4
24030.21	-18047	-281.92	D508	21.16	172	5.73	20.8
24031.22	-18048.7	-281.92	D508	17.58	446	12.5	16.9
24038.79	-18061.7	-281.92	D508	17.2	115	3.6	8.19

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24034.75	-18054.8	-281.92	D508	15.9	1160	29.2	5.17
24038.28	-18060.8	-281.92	D508	14.72	179	4.47	7.52
24029.21	-18045.3	-281.92	D508	14.08	8.6	0.22	3.13
24037.78	-18059.9	-281.92	D508	8.88	24.6	0.59	1.88
24039.29	-18062.5	-281.92	D508	1.34	5.7	0.2	0.07
24031.75	-17999.3	-249.27	D510	2.18	0.3	0	0.01
24032.19	-17998.8	-248.49	D510	2.18	0.3	0	0.01
24032.62	-17998.4	-247.72	D510	1.42	0.26	0	0.01
23748.85	-18490.5	-217.05	D514	13.57	9.64	0.32	2.02
23755.31	-18487.8	-217.05	D514	11.25	108.65	4.16	5.18
23747.93	-18490.9	-217.05	D514	8.44	8.22	0.28	3.05
23743.32	-18492.9	-217.05	D514	7.09	211.2	8.12	7.82
23744.24	-18492.5	-217.05	D514	6.73	210.6	6.52	7.55
23754.38	-18488.2	-217.05	D514	6.69	140.85	5.08	12.27
23745.17	-18492.1	-217.05	D514	6.41	133.6	5.46	17.99
23746.09	-18491.7	-217.05	D514	6.07	144.4	5.52	14.37
23749.78	-18490.2	-217.05	D514	5.79	26.44	0.99	6.42
23747.01	-18491.3	-217.05	D514	5.46	73.4	2.77	10.62
23742.4	-18493.3	-217.05	D514	5.16	7.9	5.66	13.2
23753.46	-18488.6	-217.05	D514	5.16	129.3	4.92	16.45
23756.23	-18487.4	-217.05	D514	3.79	125.7	4.84	6.82
23750.7	-18489.8	-217.05	D514	3.37	38.49	1.48	11.78
23752.54	-18489	-217.05	D514	3.02	49.04	1.86	15.62
23756.87	-18487.2	-217.05	D514	2.38	34	1.17	0.56
23751.62	-18489.4	-217.05	D514	1.67	17.77	0.63	8.36
23742.31	-18501.7	-211.67	D515	19.24	96.1	3.79	5.89
23743.28	-18501.5	-211.5	D515	18.26	104.47	4.05	5.5
23744.26	-18501.4	-211.33	D515	15.01	142.9	6.18	4.51
23746.21	-18501.1	-210.98	D515	13.7	71.48	4.05	5.94
23745.23	-18501.3	-211.15	D515	12.74	187	9.73	4.33
23738.41	-18502.2	-212.37	D515	8.56	290	10.6	8.54
23754.98	-18499.9	-209.42	D515	8.29	54.82	1.92	8.31
23754.01	-18500	-209.59	D515	8.28	54.44	1.95	2.69
23740.36	-18502	-212.02	D515	7.4	266	10.4	9.47
23741.33	-18501.8	-211.85	D515	5.64	223	8.48	1.55
23755.96	-18499.8	-209.24	D515	5.58	78.58	2.74	4.5
23750.11	-18500.6	-210.29	D515	5.18	20	0.7	0.55
23756.54	-18499.7	-209.14	D515	4.96	85	2.97	3.22
23753.03	-18500.2	-209.76	D515	4.86	22.2	0.72	1.14
23747.18	-18501	-210.81	D515	4.3	16.99	0.87	2.13
23739.38	-18502.1	-212.2	D515	4.24	398	14.7	15.7
23749.13	-18500.7	-210.46	D515	3.34	9.93	0.25	0.56
23752.06	-18500.3	-209.94	D515	3.28	13.65	0.49	0.52

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23751.08	-18500.4	-210.11	D515	3.2	13.2	0.48	0.49
23748.16	-18500.9	-210.63	D515	1.34	11.2	0.42	0.76
23737.94	-18466.7	-217.05	D516	23.22	243	9.65	1.46
23738.48	-18465.8	-217.05	D516	21.74	262	9.98	0.67
23738.95	-18465.1	-217.05	D516	21.74	262	9.98	0.67
23737.4	-18467.5	-217.05	D516	15.64	77.8	3.14	7.45
23925.74	-18036.3	-364.56	D518	3.56	5.3	0.1	0.06
23925.56	-18036.2	-365.54	D518	3.38	5.08	0.09	0.06
23928.02	-18036.5	-351.76	D518	1.57	49.4	0.41	0.13
23863.4	-18025.7	-323.39	D520	2.45	52.35	0.92	0.36
23941.02	-18009.8	-228.05	D522	20.44	226	7.92	6.97
23940.82	-18009.5	-228.76	D522	20.44	226	7.92	6.97
23941.52	-18010.6	-226.27	D522	12.44	271.56	8.94	6.92
23941.77	-18010.9	-225.38	D522	11.62	226.35	7.46	5.82
23942.01	-18011.3	-224.49	D522	5.58	3.5	0.27	0.07
23941.27	-18010.2	-227.16	D522	2.28	261	9.25	4.93
23889.41	-18614.7	-298.52	D524	8.48	25.97	1.14	9.46
23888.91	-18617.2	-303	D524	7.28	1.5	0.02	0.48
23888.97	-18616.9	-302.5	D524	5.96	13.2	0.45	0.48
23889.8	-18612.8	-295.04	D524	5.38	5	0.12	0.3
23889.03	-18616.6	-302	D524	5.15	12.06	0.41	0.47
23889.7	-18613.3	-295.91	D524	4.53	8.1	0.27	0.42
23889.61	-18613.7	-296.78	D524	3.48	11.9	0.46	0.56
23889.32	-18615.2	-299.39	D524	3.25	37.17	1.43	10.06
23889.22	-18615.7	-300.26	D524	1.01	24.8	0.91	5.75
23807.4	-18566	-274.15	D525	5.48	1.1	0.01	0.01
23807.18	-18566.4	-275	D525	5.48	1.1	0.01	0.01
23935.27	-18640.1	-320.36	D526	4.1	7.8	0.27	0.08
23935.42	-18640.5	-320.86	D526	4.1	7.8	0.27	0.08
23786.9	-18562.4	-219.01	D528	17.67	164.56	6.03	4.31
23787.61	-18561.8	-218.8	D528	16.04	141.06	5.17	4.03
23786.2	-18563.1	-219.22	D528	11.49	217	7.93	1.31
23785.49	-18563.8	-219.43	D528	9.76	233.8	8.71	3.42
23789.72	-18559.7	-218.17	D528	6.87	133	5.3	6.22
23791.83	-18557.7	-217.53	D528	6.48	256	9.37	1.83
23784.07	-18565.1	-219.84	D528	6.36	147	5.72	6.16
23783.56	-18565.6	-219.99	D528	6.36	147	5.72	6.16
23784.78	-18564.5	-219.63	D528	5.47	257.5	9.95	8.44
23791.13	-18558.4	-217.74	D528	5.32	309.46	10.69	0.49
23797	-18552.7	-215.93	D528	3.21	54.01	2.07	5.45
23788.32	-18561.1	-218.59	D528	3.11	32.04	1.33	1.86
23789.02	-18560.4	-218.38	D528	3.06	59.7	2.37	2.75
23790.43	-18559.1	-217.95	D528	2.61	110.11	3.91	1

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23861.86	-18641.6	-229.09	D529	9.78	102.84	2.9	1.81
23859.65	-18646.8	-230.3	D529	7.08	418	13.3	2.18
23862.24	-18640.7	-228.88	D529	4.05	385.5	11.8	13.8
23861.47	-18642.5	-229.3	D529	3.78	21.88	0.69	0.04
23861.09	-18643.4	-229.51	D529	2.81	16.75	0.43	0.03
23860.84	-18644	-229.65	D529	2.79	17	0.39	0.03
23785.75	-18534.1	-228.06	D530	3.38	1.42	0.01	0
23784.88	-18534.3	-228.53	D530	2.76	1.22	0.01	0
23800.88	-18531.7	-247.6	D531	7.29	270	10.1	9.78
23800.41	-18531.8	-248.47	D531	7.29	270	10.1	9.78
23798.51	-18532.2	-251.97	D531	7.26	330.78	12.84	9.91
23801.34	-18531.6	-246.77	D531	4.05	123	4.47	0.87
23798.03	-18532.4	-252.84	D531	4	316.8	12.47	19.22
23797.55	-18532.5	-253.71	D531	3.19	107.52	4.13	9.4
23797.29	-18532.5	-254.19	D531	3.15	84.8	3.22	8.18
23799.94	-18531.9	-249.35	D531	1.98	131	5.56	20.2
23798.98	-18532.1	-251.09	D531	1.61	79.02	2.88	21.42
23799.46	-18532	-250.22	D531	1.52	175.1	6.84	22.27
23806.33	-18580.6	-224.66	D532	32.34	30.4	1.06	1.36
23806.54	-18580	-224.46	D532	20.41	52.78	1.91	5.4
23807.17	-18578.2	-223.84	D532	14.34	92.05	3.16	6.09
23808.11	-18575.5	-222.89	D532	10.97	195	6.08	0.12
23806.86	-18579.1	-224.15	D532	10.65	71.1	2.6	8.71
23807.49	-18577.3	-223.52	D532	9.19	57.55	1.9	1.74
23809.03	-18572.8	-221.94	D532	6.39	126	4.85	7.11
23808.73	-18573.7	-222.26	D532	6.39	126	4.85	7.11
23811.66	-18564.8	-219.05	D532	3.48	5.8	0.12	0.11
23811.37	-18565.7	-219.38	D532	3.48	5.8	0.12	0.11
23811.07	-18566.6	-219.7	D532	2.67	52.1	1.68	1.79
23810.78	-18567.5	-220.03	D532	2.01	46.65	1.49	1.7
23810.49	-18568.4	-220.35	D532	1.83	14	0.38	0.62
23810.2	-18569.3	-220.68	D532	1.83	14	0.38	0.62
23809.9	-18570.2	-221	D532	1.83	14	0.38	0.62
23809.6	-18571.1	-221.33	D532	1.62	14.12	0.4	0.62
23836.19	-18597.5	-227.78	D533	10.44	60.9	2.02	6.4
23835.46	-18598	-228.03	D533	10.44	60.9	2.02	6.4
23836.98	-18596.9	-227.51	D533	3.81	60.5	2.11	10.5
23837.62	-18596.5	-227.28	D533	3.51	9.9	0.44	1.69
23833.95	-18599.1	-228.56	D533	1.32	11.6	0.36	0.17
23818.46	-18581.3	-217.4	D534	15.42	243	9.58	8.07
23818.36	-18582.2	-217.57	D534	14.07	256.65	10.02	8.45
23815.74	-18607.4	-221.84	D534	5.97	378.67	13.57	12.84
23818.27	-18583.2	-217.75	D534	5.82	292.63	10.96	10.22

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23815.24	-18611.9	-222.58	D534	5.25	124	4.3	6.5
23815.3	-18611.4	-222.49	D534	5.05	118.53	4.13	7.28
23815.63	-18608.4	-222	D534	4.77	336	11.7	20.4
23815.52	-18609.4	-222.17	D534	4.71	45.2	1.7	11.8
23818.19	-18584	-217.89	D534	3.69	137	5.15	8.81
23815.41	-18610.4	-222.33	D534	3.24	69.3	2.63	14.3
23817.83	-18587.7	-218.54	D534	1.11	35.8	1.23	1.37
23817.92	-18586.7	-218.37	D534	1.05	28.84	0.98	1.12
23856.78	-18579.7	-279.41	D535	6.27	41.7	1.02	0.56
23834.12	-18552.9	-272.94	D537	6.48	280	11	12.3
23870.37	-18519.5	-320.49	D539	12.27	205	5.5	8.75
23870.53	-18519.7	-319.83	D539	11.76	194	5.52	8.74
23870.76	-18519.9	-318.89	D539	7.9	121.94	4.52	7
23871.21	-18520.4	-317	D539	7.74	245.4	7.78	0.3
23872.02	-18521.2	-313.59	D539	1.44	49.1	1.54	2.16
23871.84	-18521	-314.35	D539	1.44	49.1	1.54	2.16
23776.96	-18444.1	-275.17	D542	15.64	192.32	6.71	3.76
23781.41	-18444.5	-272.91	D542	12.93	54	2.27	8.54
23789.41	-18445	-268.81	D542	12.3	58	1.67	0.13
23788.52	-18445	-269.27	D542	12.3	58	1.67	0.13
23775.19	-18444	-276.08	D542	9.39	118	3.82	21.2
23772.52	-18443.8	-277.43	D542	9.09	93.8	3.43	4.44
23782.3	-18444.5	-272.46	D542	6.76	27.4	1.15	4.3
23777.85	-18444.2	-274.72	D542	6.63	88.74	3.04	1.71
23783.19	-18444.6	-272	D542	5.46	23	0.82	2.12
23776.07	-18444.1	-275.62	D542	3.9	25.6	0.81	1.89
23771.63	-18443.8	-277.88	D542	3.81	215	7.85	8.83
23769.84	-18443.6	-278.78	D542	3.81	170	6.03	4.1
23769.35	-18443.6	-279.03	D542	3.81	170	6.03	4.1
23770.74	-18443.7	-278.33	D542	3.69	232	7.92	8.58
23773.41	-18443.9	-276.98	D542	3.21	107	3.71	3.08
23784.08	-18444.7	-271.55	D542	3.04	13.75	0.5	1.2
23774.3	-18444	-276.53	D542	2.73	343	11.8	2.31
23768.86	-18443.6	-279.27	D542	1.35	16.3	0.59	0.59
23847.15	-18501.9	-307.06	D543	20.16	135	5.46	5.16
23845.58	-18500.4	-310.46	D543	7.29	214	7.24	3.72
23847.54	-18502.2	-306.21	D543	5.28	127	4.65	8.19
23854.94	-18509	-290.31	D543	4.44	10.45	0.32	0.16
23839.44	-18494.9	-324.06	D543	3.36	1190	43.6	0.33
23840.21	-18495.6	-322.34	D543	3.33	195	7.45	24.7
23846.76	-18501.5	-307.91	D543	3.27	69.4	2.46	2.4
23839.82	-18495.3	-323.2	D543	3.27	497	19	1.1
23854.54	-18508.6	-291.15	D543	3.11	9.85	0.3	0.14

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23848.32	-18502.9	-304.51	D543	2.7	59.3	2.4	4.3
23845.2	-18500.1	-311.31	D543	2.64	42.4	1.71	25.4
23839.06	-18494.6	-324.92	D543	2.61	1580	56.4	0.31
23838.79	-18494.4	-325.52	D543	2.61	1580	56.4	0.31
23855.34	-18509.3	-289.47	D543	2.24	18.2	0.51	1.43
23842.48	-18497.6	-317.29	D543	1.89	20.1	0.65	3.11
23847.93	-18502.6	-305.36	D543	1.71	242	9.31	6.04
23796.84	-18473.6	-281.35	D544	7.66	82.27	3.39	0.14
23793.8	-18474.2	-283.37	D544	5.94	422	14.4	15.8
23792.97	-18474.4	-283.92	D544	2.08	148.44	4.94	4.96
23795.32	-18473.9	-282.36	D544	1.5	2.7	0.08	0.04
23799.3	-18473.1	-279.71	D544	1.17	28.8	1.12	2.31
23896.79	-18474.3	-406.67	D546	16.94	38.1	1	3.74
23896.76	-18470.5	-417.43	D546	14.5	207.2	10.26	11.68
23896.76	-18471.5	-414.6	D546	12.34	13.8	1.14	2.59
23896.79	-18468.9	-422.15	D546	11.79	48.3	1.3	1.44
23896.79	-18468.6	-422.76	D546	11.79	48.3	1.3	1.44
23896.76	-18470.2	-418.37	D546	11.41	138.46	5.74	5.76
23896.76	-18471.2	-415.54	D546	11.37	58.41	2.19	5.32
23896.76	-18470.8	-416.48	D546	10.54	177.35	6.61	12.15
23897.83	-18491.2	-359.76	D546	10.11	38.2	1.32	18.2
23896.84	-18467.1	-427.16	D546	6.99	21.45	0.51	2.41
23896.83	-18467.5	-426.21	D546	6.31	29.94	0.75	2.71
23896.78	-18469.2	-421.21	D546	4.52	16.8	0.5	0.51
23896.82	-18467.8	-425.27	D546	4.35	39.3	1.03	2.77
23897.73	-18489.8	-363.71	D546	4.2	8.4	0.25	8.52
23896.76	-18473	-410.16	D546	4.18	13.62	0.27	0.95
23897.85	-18491.6	-358.82	D546	3.03	405	15.5	24
23897.81	-18490.9	-360.7	D546	2.55	59.4	1.87	17.5
23897.79	-18490.7	-361.26	D546	2.55	59.4	1.87	17.5
23897.71	-18489.5	-364.58	D546	2.13	10	0.35	4.26
23896.81	-18468.1	-424.32	D546	1.98	12.42	0.34	0.87
23896.85	-18466.8	-428.11	D546	1.41	1.2	0.02	0.04
23896.76	-18472.7	-411.11	D546	1.33	4.3	0.08	0.28
23896.86	-18466.5	-429.05	D546	1.29	1.14	0.02	0.04
23770.66	-18431.5	-272.44	D547	19.05	65.1	1.9	5.01
23762.39	-18421.5	-261.48	D547	18.45	10.4	0.3	0.13
23759.47	-18418	-257.56	D547	13.83	24.84	0.77	0.5
23758.99	-18417.4	-256.9	D547	13.33	63.37	1.87	2.28
23757.53	-18415.7	-254.93	D547	12.69	545	10.7	3.89
23758.5	-18416.8	-256.25	D547	11.81	181.16	5.47	3.94
23758.02	-18416.2	-255.59	D547	10.68	296	9.04	3.27
23771.15	-18432.1	-273.07	D547	10.47	51.5	1.78	1.82

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23770.18	-18430.9	-271.8	D547	9.93	411	8.78	2.37
23760.93	-18419.7	-259.52	D547	8.99	45.34	1.52	0.05
23762.87	-18422	-262.13	D547	7.85	31.6	1.08	1.35
23761.9	-18420.9	-260.83	D547	7.5	6.12	0.18	0.08
23768.23	-18428.5	-269.24	D547	7	52.55	1.78	16.78
23774.08	-18435.7	-276.88	D547	6.66	100.4	3.66	9.91
23773.1	-18434.5	-275.62	D547	6.54	228.45	7.84	2.84
23767.74	-18427.9	-268.59	D547	5.62	36.71	1.25	12.16
23773.59	-18435.1	-276.25	D547	5.61	62.85	2.11	4.96
23772.61	-18433.9	-274.98	D547	5.58	278	9.35	4.39
23774.57	-18436.3	-277.52	D547	5.24	129	4.53	7.76
23769.69	-18430.3	-271.16	D547	5.19	143	5.15	5
23777.5	-18439.9	-281.3	D547	4.95	311.17	12.13	16.71
23781.41	-18444.7	-286.33	D547	4.92	3.7	0.07	0.41
23759.96	-18418.5	-258.21	D547	4.58	6.36	0.21	0.07
23761.42	-18420.3	-260.17	D547	3.97	13.68	0.44	0.06
23776.04	-18438.1	-279.41	D547	3.88	271	9.97	9.49
23746.92	-18403.2	-240.22	D547	3.48	1.3	0.03	0
23747.4	-18403.8	-240.9	D547	3.48	1.3	0.03	0
23771.64	-18432.7	-273.71	D547	3.48	96.8	2.99	2.08
23765.79	-18425.5	-266.02	D547	3.45	56.2	1.96	8.1
23772.13	-18433.3	-274.35	D547	3.19	129.9	4.09	3.64
23757.05	-18415.1	-254.27	D547	3.13	42.57	0.84	0.26
23756.57	-18414.5	-253.61	D547	2.97	176	3.66	0.37
23776.52	-18438.7	-280.04	D547	2.97	209	7.67	6.38
23763.85	-18423.2	-263.43	D547	2.91	21.5	0.68	0.88
23775.55	-18437.5	-278.78	D547	2.81	274.2	9.71	12.1
23781.9	-18445.3	-286.96	D547	2.51	2.4	0.04	0.22
23766.28	-18426.1	-266.66	D547	2.32	40.52	1.42	3.24
23775.06	-18436.9	-278.15	D547	2.25	169	5.49	6.39
23777.01	-18439.3	-280.67	D547	2.22	187	6.8	7.77
23763.36	-18422.6	-262.78	D547	2.13	33.05	1.12	1.49
23765.3	-18425	-265.37	D547	2.12	18.04	0.65	6.06
23768.71	-18429.1	-269.88	D547	2.09	19.1	0.64	4.32
23760.44	-18419.1	-258.87	D547	1.67	4.58	0.14	0.03
23767.25	-18427.3	-267.95	D547	1.52	3.84	0.14	2.63
23784.35	-18448.3	-290.11	D547	1.05	53.4	1.92	0.74
23917.22	-18495.5	-432.44	D548	24.6	73.65	2.29	10.78
23917.25	-18495.7	-433.42	D548	21.36	31.1	0.95	5.28
23917.19	-18495.3	-431.46	D548	16.67	433.5	12.78	14.05
23917.09	-18494.6	-427.54	D548	14.37	348	9.39	12.5
23917.36	-18496.5	-437.34	D548	13.41	11.6	0.24	0.13
23917.39	-18496.7	-438.32	D548	13.41	11.6	0.24	0.13

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23917.41	-18496.9	-439.3	D548	12.56	8.93	0.17	0.1
23917.03	-18494.2	-425.58	D548	11.25	296	8.16	11.9
23917.06	-18494.4	-426.56	D548	11.25	296	8.16	11.9
23917.44	-18497.1	-440.28	D548	10.56	2.7	0.01	0.02
23914.91	-18482.3	-365.48	D548	10.17	381	11.7	5.39
23917.28	-18495.9	-434.4	D548	9.68	32.17	0.95	3.59
23917.17	-18495.1	-430.48	D548	9.65	496.5	14.9	8.88
23917.11	-18494.8	-428.52	D548	9.48	206.65	5.68	8.85
23914.86	-18482.1	-364.5	D548	8.83	335.6	10.35	9.45
23915.07	-18483	-369.4	D548	8.07	9	0.25	14.2
23915.11	-18483.2	-370.38	D548	8.03	14.07	0.45	14.8
23915.14	-18483.4	-371.02	D548	7.95	25.9	0.91	16.2
23917.47	-18497.3	-441.26	D548	7.65	2.46	0.01	0.01
23914.95	-18482.5	-366.46	D548	7.29	127	4.5	0.65
23914.99	-18482.7	-367.44	D548	7.29	127	4.5	0.65
23916.73	-18492	-414.79	D548	6.09	134	4.08	11.9
23917.14	-18494.9	-429.5	D548	4.88	158.65	5.04	5.28
23914.82	-18481.9	-363.52	D548	3.48	154	4.96	25.7
23960.71	-18498.9	-387.83	D549	17.28	92.7	3.3	9.6
23961.02	-18498.7	-388.75	D549	17.28	92.7	3.3	9.6
23961.3	-18498.5	-389.57	D549	17.28	92.7	3.3	9.6
23960.4	-18499.2	-386.91	D549	13.03	330.48	10.81	8.56
23960.09	-18499.4	-385.99	D549	12.81	343	11.2	8.5
23958.31	-18500.9	-380.72	D549	7.32	172	6.62	19.9
23958.62	-18500.6	-381.64	D549	7.32	174.1	6.65	18.53
23958.93	-18500.4	-382.56	D549	7.29	193	6.94	6.21
23959.11	-18500.2	-383.11	D549	7.29	193	6.94	6.21
23955.72	-18503	-372.96	D549	1.53	343	13.5	4.35
23962.81	-18497.2	-394.07	D549	1.23	56.7	2.17	1.64
23963.12	-18497	-394.98	D549	1.23	56.7	2.17	1.64
23959.3	-18500.1	-383.66	D549	1.14	2	0.07	0.11
23959.61	-18499.8	-384.57	D549	1.14	2	0.07	0.11
23959.85	-18499.6	-385.28	D549	1.14	2	0.07	0.11
23744.24	-18401.2	-252.92	D550	136.41	145.97	3.68	0.71
23740.88	-18397.7	-246.62	D550	53.63	4.47	0.14	0
23741.29	-18398.1	-247.41	D550	49.19	6.75	0.35	0
23743.81	-18400.8	-252.13	D550	37.51	114.33	3.41	1.24
23740.46	-18397.2	-245.83	D550	37.27	5.55	0.15	0
23741.71	-18398.6	-248.19	D550	13.19	8.48	0.22	0
23750.67	-18407.8	-264.66	D550	12.48	25.23	0.58	0.45
23739.01	-18395.6	-243.07	D550	10.26	176.5	5.32	1.36
23740.05	-18396.7	-245.04	D550	9.15	2.9	0.06	0.04
23742.13	-18399	-248.98	D550	9.12	17.7	0.45	0

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23739.43	-18396.1	-243.86	D550	8.93	121.55	3.28	1.59
23742.97	-18399.9	-250.56	D550	8.36	101.16	3.19	0.22
23739.73	-18396.4	-244.45	D550	7.68	71.1	2.18	1.05
23743.39	-18400.4	-251.35	D550	7.15	103.37	3.27	0.41
23742.55	-18399.5	-249.77	D550	7.14	75.84	2.44	0.51
23738.6	-18395.1	-242.28	D550	5.3	97.4	3.22	0.4
23748.92	-18406	-261.51	D550	5.23	20.56	0.54	0.27
23749.36	-18406.5	-262.3	D550	4.92	14.12	0.31	0.29
23754.66	-18411.6	-271.75	D550	4.45	2.62	0.07	0.07
23755.11	-18412.1	-272.53	D550	3.75	2.88	0.07	0.03
23745.04	-18402.1	-254.42	D550	2.79	36.9	1	0.49
23745.47	-18402.5	-255.21	D550	2.45	3.96	0.14	0.1
23748.49	-18405.6	-260.72	D550	2.3	19.68	0.67	0.14
23751.11	-18408.2	-265.45	D550	1.9	4.57	0.12	0.22
23747.19	-18404.3	-258.36	D550	1.27	19.64	0.76	0.48
23752.44	-18409.5	-267.82	D550	1.27	27.33	0.85	2.09
23748.05	-18405.2	-259.94	D550	1.21	12.6	0.47	0.15
23745.9	-18403	-256	D550	1.06	3.6	0.12	0.11
23750.23	-18407.3	-263.88	D550	1.02	11.1	0.34	0.29
23941.19	-18512.4	-446.4	D551	29.86	34.8	0.72	1.02
23941.07	-18512.5	-445.61	D551	19	231.72	6.83	6.07
23939.44	-18514	-434.83	D551	17.16	393.3	11.47	17.38
23939.59	-18513.9	-435.81	D551	16.05	387	10.3	18.1
23939.29	-18514.1	-433.85	D551	15.53	642.8	15.92	9.02
23939.74	-18513.7	-436.79	D551	15.5	434	13.7	14.2
23939.89	-18513.6	-437.77	D551	14.46	517.3	14.68	7.22
23940.63	-18512.9	-442.67	D551	12.99	84.3	3	2.47
23940.77	-18512.8	-443.65	D551	12.53	134.86	3.83	4.22
23940.03	-18513.5	-438.75	D551	12.5	289.9	7.83	9.19
23939.14	-18514.3	-432.87	D551	12.22	234.3	5.89	13.56
23940.92	-18512.7	-444.63	D551	12.15	233.7	6.78	6.57
23940.48	-18513.1	-441.69	D551	10.5	32.19	0.83	3.72
23940.18	-18513.3	-439.73	D551	9.68	63.54	1.73	5.22
23940.33	-18513.2	-440.71	D551	9.43	35.58	0.95	2.8
23941.31	-18512.3	-447.18	D551	5.38	2.4	0.06	0.06
23938.69	-18514.7	-429.84	D551	3.4	19.48	0.68	3.48
23927.88	-18524.4	-360.35	D551	2.43	289.84	8.19	2.02
23938.83	-18514.5	-430.82	D551	1.62	15.48	0.58	1.7
23897.78	-18445.4	-403.23	D552	26.28	10.4	0.4	8.53
23897.8	-18445.4	-402.23	D552	19.2	17.1	0.62	11.1
23897.43	-18445	-417.67	D552	17.64	85.1	2.35	13.9
23897.33	-18444.8	-421.66	D552	17.4	107	3.09	7.43
23897.31	-18444.8	-422.24	D552	17.4	107	3.09	7.43

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23897.51	-18445.1	-414.67	D552	16.8	288	9.12	5.38
23897.41	-18444.9	-418.66	D552	15.93	46.6	1.39	5.65
23897.35	-18444.9	-420.66	D552	13.83	132	4.01	4.02
23897.49	-18445	-415.67	D552	12.96	653	19.6	5.45
23898.75	-18446.6	-359.63	D552	11.85	100	3.53	5.09
23897.38	-18444.9	-419.66	D552	11.04	66.7	1.96	6.94
23897.46	-18445	-416.67	D552	10.92	108	3.17	17.7
23897.76	-18445.4	-404.23	D552	9.94	28.82	1.4	11.88
23898.77	-18446.6	-358.7	D552	6.69	98	2.52	11.2
23898.79	-18446.6	-357.7	D552	5.67	100	1.41	16.2
23897.74	-18445.3	-405.22	D552	4.68	48.94	2.65	9.55
23897.54	-18445.1	-413.67	D552	4.56	18.6	0.53	0.2
23897.83	-18445.4	-401.23	D552	3.96	32.9	3.48	3.91
23897.56	-18445.1	-412.67	D552	3.15	115	2.8	0.9
23897.72	-18445.3	-405.85	D552	2.34	15.4	1.19	2.28
23898.94	-18446.8	-350.26	D552	1.56	0.6	0	0.01
23898.92	-18446.8	-351.26	D552	1.56	0.6	0	0.01
23708.89	-18358.5	-215.38	D554	11.31	7.9	0.22	0.03
23708.9	-18358.4	-216.38	D554	9.75	123.95	4.32	1.32
23708.91	-18358.4	-217.38	D554	8.19	240	8.41	2.6
23708.86	-18358.6	-212.39	D554	1.92	113	2.85	0.25
23708.87	-18358.6	-213.39	D554	1.77	71.95	1.86	0.45
23708.88	-18358.5	-214.38	D554	1.62	30.9	0.87	0.65
23708.92	-18358.3	-218.38	D554	1.16	24.43	0.85	0.27
23953.38	-18548.2	-471.86	D555	26.17	545.6	18.92	16.06
23952.69	-18548.2	-466.91	D555	17.22	160.18	6.29	11.11
23952.55	-18548.2	-465.92	D555	17.2	117.75	4.75	12.9
23951.3	-18548.2	-457	D555	16.94	183.63	6.81	13.6
23953.24	-18548.2	-470.87	D555	15.95	407	15.23	8.16
23952.41	-18548.2	-464.93	D555	14.64	169.88	6.73	10.01
23942.78	-18548.2	-400.29	D555	12.66	101.22	2.78	15.06
23951.16	-18548.2	-456.01	D555	12.49	249.18	9.84	14.36
23950.74	-18548.2	-453.04	D555	12.48	200	8.52	10.1
23953.11	-18548.2	-469.88	D555	11.26	346	11.06	1.32
23952.97	-18548.2	-468.89	D555	10.9	107.81	3.66	1.03
23952.27	-18548.2	-463.94	D555	10.85	284.75	10.78	9.58
23952.13	-18548.2	-462.95	D555	10.81	377.6	13.97	9.36
23952.83	-18548.2	-467.9	D555	10.64	171.6	6.11	6.09
23953.75	-18548.2	-474.43	D555	7.89	552	22.8	22.6
23953.52	-18548.2	-472.85	D555	7.48	307.33	11.59	8.01
23951.44	-18548.2	-457.99	D555	5.96	61.3	2.2	4.51
23951.99	-18548.2	-461.95	D555	5.02	167.88	6.19	3.49
23950.88	-18548.2	-454.03	D555	3.81	65.88	2.82	3.11

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23951.02	-18548.2	-455.02	D555	3.57	171.57	6.62	8.84
23953.66	-18548.2	-473.84	D555	3.43	285.17	11.65	10.34
23942.63	-18548.2	-399.3	D555	2.98	24.36	0.66	3.56
23951.57	-18548.2	-458.98	D555	2.85	12.72	0.48	0.81
23943.23	-18548.2	-403.26	D555	2.63	7.34	0.28	2.13
23942.33	-18548.2	-397.32	D555	1.03	0.78	0	0.02
23783.84	-18358.6	-298.13	D556	8.64	422	14.3	1.24
23780.08	-18358.6	-292.8	D556	8.46	507.44	18.79	10.96
23783.53	-18358.6	-297.7	D556	7.95	384.24	13.04	4.66
23767.03	-18358.6	-273.86	D556	7.77	209.47	7.99	11.57
23762.56	-18358.6	-267.22	D556	6.67	287.2	10.33	7.68
23773.8	-18358.6	-283.77	D556	6.6	83.46	3.3	13.37
23779.5	-18358.6	-291.98	D556	6.47	330.68	12.89	9.47
23765.92	-18358.6	-272.2	D556	6.4	128.91	4.58	0.92
23767.59	-18358.6	-274.68	D556	5.82	197.68	7.37	13.58
23773.23	-18358.6	-282.94	D556	5.75	28.04	1.19	15.8
23772.1	-18358.6	-281.29	D556	5.45	388.8	15.96	6.01
23772.67	-18358.6	-282.12	D556	4.87	349.18	13.85	6.98
23760.88	-18358.6	-264.74	D556	4.65	919	30.3	0.95
23762	-18358.6	-266.39	D556	4.56	209.2	7.07	6.5
23782.96	-18358.6	-296.89	D556	4.36	194	6.77	22.76
23761.44	-18358.6	-265.57	D556	4.22	635.8	22.04	1
23782.38	-18358.6	-296.07	D556	4.2	298.56	11.06	23.22
23774.93	-18358.6	-285.41	D556	4.08	89.91	3.59	5.99
23771.53	-18358.6	-280.47	D556	4.07	262.5	11.01	5.63
23780.65	-18358.6	-293.62	D556	3.75	307	11.19	23.46
23778.93	-18358.6	-291.16	D556	3.68	175.4	6.95	5.91
23775.5	-18358.6	-286.23	D556	3.43	62.28	2.5	3.99
23774.37	-18358.6	-284.59	D556	3.27	122	4.75	5.93
23768.16	-18358.6	-275.51	D556	3.24	124.27	4.8	5.24
23781.23	-18358.6	-294.43	D556	3.14	624.2	24.38	19.58
23781.8	-18358.6	-295.25	D556	3.11	637.56	24.09	20.75
23770.97	-18358.6	-279.64	D556	2.98	103.66	4.32	2.81
23776.64	-18358.6	-287.88	D556	2.84	44.83	1.71	3.93
23764.8	-18358.6	-270.54	D556	2.72	26.73	1.01	0.23
23766.47	-18358.6	-273.03	D556	2.43	59.7	2.31	1.44
23763.12	-18358.6	-268.05	D556	2.28	80.72	2.99	1.89
23768.72	-18358.6	-276.34	D556	2.26	70.19	2.68	3.54
23776.07	-18358.6	-287.06	D556	1.89	20.5	0.82	0.09
23770.41	-18358.6	-278.82	D556	1.71	19.55	0.77	0.8
23769.28	-18358.6	-277.17	D556	1.7	30.93	1.06	3.8
23942.09	-18464.3	-433.69	D557	30.23	74.68	2.6	8.11
23941.93	-18464.2	-432.71	D557	25.35	159.9	5.39	11.06

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23942.24	-18464.3	-434.68	D557	24.88	62.41	1.89	8.99
23942.39	-18464.4	-435.67	D557	19.87	32.54	0.98	8.43
23940.7	-18463.7	-424.82	D557	16.67	213.9	5.28	8.1
23941.78	-18464.1	-431.72	D557	13.13	68.99	4.04	10.66
23932.44	-18460.6	-374.38	D557	13.08	68.2	2.36	8.25
23942.55	-18464.4	-436.65	D557	12.26	348.32	9.56	14.33
23933.09	-18460.8	-378.32	D557	12.2	25.18	0.88	13.02
23942.7	-18464.5	-437.64	D557	11.88	189.1	9.48	5.61
23943	-18464.6	-439.61	D557	10.68	35.92	2.67	3.7
23942.85	-18464.6	-438.62	D557	10.58	139.95	6.83	5.49
23932.28	-18460.5	-373.4	D557	10.41	78.1	2.1	12.7
23932.93	-18460.8	-377.34	D557	8.97	19.3	0.48	6.68
23941.63	-18464.1	-430.73	D557	8.82	60.26	3.04	5.51
23932.6	-18460.7	-375.37	D557	6.57	16.2	0.36	23.8
23943.16	-18464.7	-440.6	D557	6.18	73.92	2.78	2.51
23940.54	-18463.6	-423.83	D557	5.86	73.38	1.8	2.84
23932.77	-18460.7	-376.35	D557	5.67	8.5	0.11	23.6
23933.58	-18461	-381.28	D557	5.07	36.78	1.33	22.7
23934.66	-18461.4	-387.78	D557	4.68	276	7.03	4.14
23933.91	-18461.1	-383.25	D557	4.51	104.32	3.66	35.06
23933.74	-18461.1	-382.26	D557	4.1	90.92	2.93	33.62
23934.07	-18461.2	-384.23	D557	3.55	133.88	4.95	24.64
23934.56	-18461.4	-387.19	D557	3.54	242	6.71	5.64
23933.42	-18461	-380.29	D557	3.21	26.18	0.93	6.08
23934.23	-18461.3	-385.22	D557	3.19	195	6.68	13.3
23931.38	-18460.2	-367.98	D557	2.61	73.7	2.21	4.32
23934.4	-18461.3	-386.2	D557	2.56	200.6	6.6	8.86
23931.54	-18460.3	-368.97	D557	2.1	94.7	3.24	12.8
23940.85	-18463.8	-425.8	D557	1.06	2.96	0.08	1.07
23943.31	-18464.8	-441.58	D557	1.03	40.62	1.42	1.25
23702.2	-18399.9	-220.29	D558	7.08	25.5	0.83	0.29
23701.75	-18404.1	-224.37	D558	5.56	164.36	5.36	12.28
23702.27	-18399.1	-219.6	D558	5.12	18.87	0.61	0.2
23701.83	-18403.3	-223.67	D558	3.17	41.26	1.32	4.69
23701.6	-18405.5	-225.76	D558	1.69	3.94	0.14	0.38
24047.56	-18666	-470.31	D559	15.6	145.5	4.91	8.44
24014.51	-18640.1	-410.94	D559	13.62	172.5	5.09	5.04
24014.05	-18639.8	-410.12	D559	13.29	125.45	3.3	2.61
24013.6	-18639.4	-409.3	D559	11.6	56	1.54	0.57
24014.96	-18640.5	-411.75	D559	11.2	135	4.29	8.81
24048.02	-18666.3	-471.12	D559	11.11	116.43	4.04	14.95
24012.69	-18638.7	-407.67	D559	11.04	187	7.56	0.21
24013.14	-18639.1	-408.49	D559	10.44	104.05	4.2	0.5

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24048.47	-18666.7	-471.94	D559	9.38	180.2	6.36	11.8
23989.73	-18620.8	-366.43	D559	8.47	23.98	1.01	7.82
24015.42	-18640.9	-412.57	D559	8.34	102.2	3.16	12.14
23995.3	-18625.1	-376.43	D559	8.13	4.07	0.16	0.26
24015.87	-18641.2	-413.39	D559	8.1	171	4.75	11.1
24016.15	-18641.4	-413.88	D559	8.1	171	4.75	11.1
24048.92	-18667	-472.74	D559	7.76	175.08	6.54	5.73
23989.27	-18620.4	-365.61	D559	7.71	4.8	0.18	2.74
23995.75	-18625.5	-377.25	D559	7.22	6.26	0.26	1.6
23996.66	-18626.2	-378.88	D559	7.03	9.73	0.42	3.95
23998.48	-18627.6	-382.15	D559	7.02	7.2	0.28	0.12
24010.87	-18637.3	-404.4	D559	6.99	275	4.34	5.28
24011.33	-18637.7	-405.22	D559	6.99	275	4.34	5.28
24047.11	-18665.6	-469.49	D559	6.99	81.6	2.7	4.45
23997.12	-18626.5	-379.7	D559	6.32	4.41	0.23	0.25
23992.12	-18622.6	-370.72	D559	6.21	4.1	0.11	0.55
24012.24	-18638.4	-406.85	D559	6.18	83.5	3.03	3.14
23990.18	-18621.1	-367.25	D559	6.16	22.78	0.96	7.02
23996.21	-18625.8	-378.07	D559	6.16	9.66	0.39	4.43
23999.74	-18628.6	-384.42	D559	5.88	7.7	0.31	0.08
23999.39	-18628.3	-383.78	D559	5.67	7.82	0.33	0.51
24011.78	-18638	-406.04	D559	5.64	72	2.53	3.47
23998.03	-18627.3	-381.33	D559	5.56	3.6	0.15	0.12
23998.94	-18628	-382.97	D559	5.14	8.15	0.39	1.73
23997.57	-18626.9	-380.52	D559	5.07	2.4	0.11	0.12
24051.27	-18668.9	-476.96	D559	4.39	348	12.7	10.2
24046.2	-18664.9	-467.86	D559	4.05	423	14.6	18.3
23988.82	-18620.1	-364.8	D559	4.02	4.88	0.18	0.77
23994.84	-18624.8	-375.62	D559	3.61	1.52	0.05	0.08
24051.64	-18669.2	-477.64	D559	3.57	191.5	7.14	16.4
24046.65	-18665.3	-468.67	D559	3.32	171.08	6.8	6.8
23992.57	-18623	-371.53	D559	1.93	2.97	0.04	0.14
24024.58	-18648	-429.03	D559	1.77	176	7.89	1.46
24010.1	-18636.7	-403.02	D559	1.59	5.5	0.06	0.03
24010.48	-18637	-403.71	D559	1.59	5.5	0.06	0.03
23782.7	-18340.7	-277.7	D560	5.64	173	5.9	22
23782.16	-18340.9	-277.05	D560	4.78	145.64	5.26	20.9
23779.63	-18341.5	-274.01	D560	4.05	341	11.5	8.32
23781.53	-18341	-276.29	D560	2.74	83.58	3.29	14.11
23952.09	-18453.1	-383.23	D561	4.31	477.1	16.59	4.78
23950.76	-18452.9	-378.42	D561	4.2	447.1	11.25	14.15
23952.89	-18453.2	-386.13	D561	3.94	753.8	21.48	3.93
23953.15	-18453.2	-387.09	D561	3.37	61.96	1	0.41

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23952.36	-18453.1	-384.2	D561	2.47	860.3	32.16	14.92
23952.62	-18453.1	-385.16	D561	2.39	704.1	26.69	18.63
23944.64	-18452.3	-356.26	D561	2.31	4.4	0.17	0.88
23951.03	-18452.9	-379.38	D561	2.27	219	7.3	7.66
23951.83	-18453	-382.27	D561	2.24	279.56	8.86	1.25
23944.91	-18452.3	-357.22	D561	1.74	3.55	0.13	0.67
23950.5	-18452.9	-377.45	D561	1.52	161.63	3.45	5.12
23749.92	-18338.9	-271.43	D563	1.39	83.28	3.37	0.23
23725.29	-18261.4	-276.47	D564	32.85	42.3	2.15	4.58
23725.48	-18260.7	-277.12	D564	29.87	25.6	1.34	2.99
23716.9	-18298	-244.35	D564	24	61.54	2.06	2.5
23714.66	-18310.4	-233.09	D564	21.69	12.52	0.24	0.02
23715.04	-18308.2	-235.11	D564	21.31	7.98	0.03	0.01
23714.79	-18309.6	-233.77	D564	21.3	11.03	0.11	0.01
23716.76	-18298.8	-243.69	D564	20.92	29.34	1.56	2.59
23714.54	-18311.1	-232.42	D564	20.85	13.2	0.56	0.04
23715.17	-18307.4	-235.78	D564	19.84	9.57	0.35	1.34
23714.91	-18308.9	-234.44	D564	19.41	7.4	0.04	0
23725.11	-18262.2	-275.83	D564	17.81	22.39	1.48	4.49
23717.04	-18297.3	-245.01	D564	15.51	248	7.72	11
23716.62	-18299.5	-243.02	D564	14.73	15.6	1.87	4.3
23724.74	-18263.7	-274.54	D564	14.67	14.1	1.69	2.02
23725.67	-18259.9	-277.76	D564	13.79	15.71	0.69	4.27
23716.08	-18302.3	-240.46	D564	12.93	6.5	0.14	1.27
23724.56	-18264.4	-273.9	D564	11.78	15.01	1.6	1.95
23724.37	-18265.1	-273.26	D564	11.19	15.2	1.58	1.93
23724.93	-18262.9	-275.19	D564	10.51	11.62	1.25	3.78
23715.95	-18303.1	-239.8	D564	10.2	6.6	0.25	3.02
23717.19	-18296.6	-245.67	D564	10.03	252.25	7.72	10.57
23715.3	-18306.7	-236.45	D564	9.75	15.8	1.82	7.42
23715.82	-18303.8	-239.13	D564	9.62	8.73	0.29	3.55
23715.43	-18306	-237.12	D564	9.59	15.2	1.51	5.95
23715.55	-18305.2	-237.79	D564	9.4	14.37	1.15	4.45
23723.83	-18267.4	-271.32	D564	9.39	10.8	0.88	0.71
23725.85	-18259.2	-278.4	D564	9.12	13.5	0.53	4.72
23725.96	-18258.7	-278.8	D564	9.12	13.5	0.53	4.72
23715.69	-18304.5	-238.46	D564	9.09	10.7	0.32	4.04
23717.3	-18296	-246.15	D564	9.06	253	7.72	10.5
23724.01	-18266.6	-271.97	D564	8.62	12.72	1.48	0.97
23727.19	-18253.8	-283.05	D564	6.15	34.1	2.54	3.71
23716.22	-18301.6	-241.13	D564	5.75	8.35	0.18	0.79
23719.29	-18286.6	-254.5	D564	3.42	4.7	0.28	0.46
23719.45	-18285.9	-255.16	D564	2.83	7.44	0.65	0.85

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23716.36	-18300.9	-241.79	D564	2.36	5.81	0.15	0.43
23719.62	-18285.2	-255.81	D564	2.33	9.4	0.92	1.12
23722.75	-18271.8	-267.47	D564	2.04	20.4	0.93	1.29
23716.49	-18300.2	-242.41	D564	1.83	5.2	0.14	0.37
23719.12	-18287.4	-253.85	D564	1.76	5.4	0.23	0.4
23718.64	-18289.6	-251.89	D564	1.65	2.3	0.15	0.32
23714.29	-18312.5	-231.06	D564	1.56	36.49	0.85	0.19
23722.58	-18272.5	-266.82	D564	1.55	14.83	0.67	0.96
23718.8	-18288.8	-252.54	D564	1.47	3.32	0.17	0.34
23727.01	-18254.6	-282.41	D564	1.11	2.8	0.39	0.64
23718.96	-18288.1	-253.2	D564	1.05	5.7	0.21	0.37
23719.79	-18284.4	-256.46	D564	1.02	3	0.21	0.31
23946.5	-18604.6	-405.63	D565	22.29	72.4	3.03	2.02
23946.7	-18604.9	-406.57	D565	22.25	67.5	3.08	6.07
23946.83	-18605.1	-407.23	D565	22.25	67.5	3.08	6.07
23935.9	-18590.6	-355.26	D565	12.16	17.58	0.45	2.42
23946.3	-18604.4	-404.68	D565	11.93	47.1	2	1.69
23937.92	-18593.2	-364.69	D565	9.69	12.6	0.52	1.67
23939.32	-18595.1	-371.29	D565	8.83	35.18	1.28	4.81
23937.72	-18593	-363.74	D565	8.19	10	0.58	0.49
23939.12	-18594.8	-370.35	D565	7.1	32.52	1.21	1.06
23937.12	-18592.2	-360.92	D565	6.9	5	0.2	0.05
23938.12	-18593.5	-365.63	D565	6.84	10.7	0.41	10.7
23938.32	-18593.8	-366.57	D565	6.33	39.9	1.64	8.25
23947.17	-18605.5	-408.84	D565	5.76	4.18	0.16	0.12
23939.72	-18595.6	-373.17	D565	5.52	9.45	0.3	0.35
23938.52	-18594	-367.52	D565	4.95	34.3	1.36	0.51
23941.77	-18598.4	-382.9	D565	4.71	59.8	2.31	8.47
23939.52	-18595.4	-372.23	D565	4.48	14.16	0.5	3.96
23937.52	-18592.7	-362.8	D565	4.41	3.1	0.07	0.3
23937.32	-18592.4	-361.86	D565	4.29	3.5	0.13	0.05
23941.57	-18598.1	-381.95	D565	4.11	35	1.41	6.21
23938.72	-18594.3	-368.46	D565	2.93	10.14	0.38	0.16
23943.95	-18601.2	-393.34	D565	2.51	19.74	0.65	3.25
23941.97	-18598.6	-383.84	D565	1.77	24	0.96	8.73
23942.07	-18598.8	-384.34	D565	1.77	24	0.96	8.73
23730.22	-18231.6	-281.11	D567	17.52	57.2	2.02	9.36
23730.31	-18231.8	-282.08	D567	17.26	36.76	1.4	5.69
23730.41	-18232	-283.04	D567	15.25	10.98	0.59	0.18
23730.68	-18232.8	-285.94	D567	12.75	32.8	1.07	0.9
23730.76	-18233	-286.91	D567	12.32	67.06	1.93	1.02
23730.84	-18233.2	-287.73	D567	11.31	147	3.94	1.31
23730.59	-18232.5	-284.98	D567	9.58	30.96	1.1	0.29

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23730.5	-18232.3	-284.01	D567	8.79	30.5	1.11	0.14
23727.5	-18225.1	-253.5	D567	4.77	3.8	0	0
23729.99	-18231	-278.69	D567	3.93	35.3	1.39	0.75
23729.9	-18230.7	-277.73	D567	2.87	21.58	0.84	0.46
23730.09	-18231.2	-279.66	D567	1.97	14.78	0.57	0.34
23730.92	-18233.4	-288.55	D567	1.92	122	0.01	0.01
23729.81	-18230.5	-276.76	D567	1.29	1	0.01	0.03
23724.15	-18218.6	-224.39	D567	1.14	8.2	0.33	0.92
23726.03	-18291.6	-267.33	D568	23.04	21.4	1.38	12.6
23726.02	-18290.1	-266.01	D568	18.24	244	6.34	7.52
23726.03	-18292.3	-267.99	D568	18.05	42.7	1.49	15.4
23726.02	-18290.8	-266.67	D568	16.05	65.05	2.23	4.28
23726.03	-18295.3	-270.62	D568	15.07	595	16.42	8.19
23726.03	-18295.8	-271.04	D568	15.05	871	24.2	6.68
23725.63	-18273	-250.58	D568	12.86	41.2	5.39	3.17
23726.03	-18293.8	-269.31	D568	11.76	93.85	2.52	3.37
23726.03	-18293.1	-268.65	D568	11.71	114.85	3.21	7.39
23725.35	-18267.2	-245.1	D568	10.94	6.5	0.9	0.21
23725.57	-18271.6	-249.21	D568	10.94	37.9	5	5.24
23726.03	-18294.6	-269.96	D568	10.87	171.35	4.6	6.28
23725.39	-18267.9	-245.79	D568	10.7	4.7	0.77	0.11
23726.01	-18289.3	-265.35	D568	9.31	160.26	4.15	5.07
23725.54	-18270.8	-248.53	D568	7.65	12	0.93	3.19
23725.66	-18273.8	-251.26	D568	6.75	7.3	0.21	0.6
23725.43	-18268.6	-246.48	D568	5.07	6.4	0.63	0.94
23725.69	-18274.5	-251.94	D568	4.59	44.2	6.1	2.02
23725.5	-18270.1	-247.85	D568	3.85	6.25	0.47	1.63
23725.47	-18269.4	-247.16	D568	1.95	2.74	0.24	0.41
23726.03	-18296.3	-271.47	D568	1.92	1.8	0.08	0.21
23726.02	-18297.1	-272.12	D568	1.92	1.8	0.08	0.21
23726.01	-18288.6	-264.69	D568	1.58	13.1	0.27	0.58
23725.99	-18287.1	-263.36	D568	1.27	5.4	0.09	0.29
23726	-18287.8	-264.03	D568	1.27	5.4	0.09	0.29
23725.6	-18272.3	-249.9	D568	1.23	7.2	0.75	1.5
23704.77	-18236.9	-218.75	D569	4.2	4.7	0.18	0.26
23704.47	-18237.6	-219.47	D569	2.73	3.13	0.12	0.17
23705.06	-18236.3	-218.02	D569	1.51	2.1	0.08	0.12
23693.32	-18259.5	-244.31	D569	1.5	1.8	0.03	0.23
23692.98	-18260.2	-245	D569	1.5	1.8	0.03	0.23
23707.07	-18232	-212.91	D569	1.47	5.34	0.1	0.7
23711.24	-18222.8	-201.79	D569	1.44	3.1	0.11	0.08
23706.79	-18232.6	-213.65	D569	1.35	5.57	0.09	1.06
23710.97	-18223.4	-202.54	D569	1.28	3.85	0.1	0.11

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23707.35	-18231.4	-212.18	D569	1.23	4.5	0.09	0.28
23709.59	-18226.5	-206.27	D569	1.14	4.1	0.06	0.09
23705.46	-18204.1	-217.2	D571	1.47	3.7	0.07	0.19
23705.16	-18204.1	-218.15	D571	1.47	3.7	0.07	0.19
23902.7	-18417.1	-367.69	D572	21.39	54.1	0.83	3.38
23900.34	-18414.9	-422.04	D572	16.53	100	2.88	3.53
23900.24	-18414.8	-424.04	D572	14.36	112.04	4.16	6.24
23900.29	-18414.9	-423.04	D572	12.39	74.9	2.35	11.2
23901.12	-18415.6	-405.12	D572	11.19	99.2	3	7.82
23901.16	-18415.6	-404.13	D572	10.35	477	13.2	4.48
23902.66	-18417.1	-368.69	D572	9.19	240.93	8.37	16.41
23901.03	-18415.5	-407.12	D572	8.64	143	5.17	10.6
23901.07	-18415.5	-406.12	D572	7.74	103	3.13	7.31
23900.98	-18415.5	-408.12	D572	7.11	477	14.9	2.19
23900.2	-18414.8	-425.04	D572	6.85	21.66	0.8	1.7
23900.75	-18415.3	-413.11	D572	6.54	10.8	0.3	1.99
23900.71	-18415.2	-414.11	D572	6.54	10.8	0.3	1.99
23900.16	-18414.8	-425.76	D572	6.45	16.8	0.62	1.47
23902.58	-18417	-370.69	D572	4.32	54.2	1.86	8.95
23900.38	-18414.9	-421.07	D572	4.2	12.3	0.47	0.33
23900.48	-18415	-419.1	D572	4.17	16.9	0.51	0.45
23900.43	-18415	-420.1	D572	4.17	16.9	0.51	0.45
23902.62	-18417.1	-369.69	D572	4.14	187.6	6.73	15.48
23900.85	-18415.3	-411.11	D572	3.54	30	0.75	2.66
23900.8	-18415.3	-412.11	D572	3.54	30	0.75	2.66
23900.57	-18415.1	-417.1	D572	3.15	11.9	0.49	1.11
23900.52	-18415.1	-418.1	D572	3.15	11.9	0.49	1.11
23900.94	-18415.4	-409.12	D572	2.73	119	2.65	0.77
23900.89	-18415.4	-410.12	D572	2.73	119	2.65	0.77
23902.28	-18416.7	-378.37	D572	2.51	79.4	3.06	3.23
23902.43	-18416.9	-374.53	D572	1.86	518	19.8	23.2
23902.54	-18417	-371.68	D572	1.77	306	10.7	9.42
23902.47	-18416.9	-373.68	D572	1.76	437.6	16.46	20.59
23900.66	-18415.2	-415.11	D572	1.74	30.1	1.06	1.11
23900.61	-18415.1	-416.1	D572	1.74	30.1	1.06	1.11
23902.51	-18416.9	-372.68	D572	1.53	250	8.66	14.5
23717.45	-18204.9	-219.86	D573	1.61	8.1	0.33	0.61
23717.42	-18204.9	-220.86	D573	1.61	8.1	0.33	0.61
23701.91	-18188.8	-222.91	D574	20.65	29.97	0.74	1.17
23701.57	-18188.5	-223.76	D574	13.1	6	0.37	3.14
23701.36	-18188.2	-224.28	D574	13.1	6	0.37	3.14
23707.01	-18194.6	-210.01	D574	2.23	5	0.14	0.16
23706.67	-18194.2	-210.87	D574	1.9	6.6	0.31	0.41

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23702.25	-18189.2	-222.05	D574	1.61	18.4	1.57	0.28
23706.33	-18193.8	-211.73	D574	1.58	8.2	0.49	0.67
23707.34	-18194.9	-209.15	D574	1.39	4.2	0.08	0.09
23694.41	-18214.7	-226.31	D575	1.32	2.5	0.06	0.21
23702.97	-18211.3	-210.85	D575	1.26	3.8	0.12	0.57
23702.5	-18211.5	-211.71	D575	1.26	3.8	0.12	0.57
23697.29	-18213.6	-221.17	D575	1.14	2.7	0.03	0.12
23696.81	-18213.7	-222.03	D575	1.14	2.7	0.03	0.12
23693.92	-18214.9	-227.17	D575	1.1	2.46	0.06	0.2
23793.93	-18198.8	-303.21	D576	34.83	58.5	1.03	1.45
23793.9	-18198.8	-304.21	D576	30.96	15.3	0.8	1.82
23793.96	-18198.8	-302.21	D576	21.67	20.1	0.77	10.8
23794.17	-18198.9	-296.02	D576	14.81	19.34	1.29	4.08
23793.54	-18198.7	-314.86	D576	12.89	148.5	8.45	13.7
23794.2	-18198.9	-295.02	D576	12.85	9.66	0.41	3.03
23794.14	-18198.9	-296.82	D576	12.51	26.7	2.01	4.78
23793.86	-18198.8	-305.16	D576	11.07	28	1.36	10.5
23794.12	-18198.9	-297.62	D576	1.54	2.7	0.16	0.52
23794.08	-18198.9	-298.62	D576	1.54	2.7	0.16	0.52
23793.99	-18198.9	-301.41	D576	1.23	2.2	0.17	0.52
23794.02	-18198.9	-300.62	D576	1.08	1.95	0.15	0.45
23941.51	-18422.6	-430.72	D577	25.2	161	5.14	7.07
23941.65	-18422.6	-431.71	D577	22.15	287	9.12	6.65
23933.81	-18421.1	-376.48	D577	19.06	226	7.64	5.4
23933.95	-18421.1	-377.47	D577	13.85	79.5	3.99	6.03
23941.78	-18422.7	-432.7	D577	12.55	354	10.8	8.23
23941.91	-18422.7	-433.69	D577	9.67	273	8.27	8.03
23942.02	-18422.8	-434.53	D577	8.71	246	7.43	7.96
23933.13	-18421	-371.86	D577	6.45	511	19.5	4.5
23934.1	-18421.2	-378.46	D577	5.64	412.05	15.97	15
23934.48	-18421.2	-381.01	D577	5.49	248	8.13	13.6
23934.39	-18421.2	-380.44	D577	4.25	184.44	6.15	10.01
23934.25	-18421.2	-379.45	D577	2.63	125.09	4.58	5.76
23941.4	-18422.6	-429.9	D577	2.23	15.2	0.55	0.7
23932.5	-18420.9	-367.63	D577	2.19	319	9.93	0.99
23931.44	-18420.7	-360.46	D577	1.82	73.32	3.16	0.96
23941.29	-18422.5	-429.08	D577	1.24	8.49	0.31	0.39
23934.56	-18421.2	-381.58	D577	1.17	53.4	0.98	0.45
23819.74	-18226.2	-312.23	D578	16.71	4.04	0.03	0.09
23814.4	-18220.9	-287.73	D578	15.51	26.7	3.33	2.73
23819.31	-18225.7	-310.33	D578	15.34	3.35	0.14	0.15
23814.75	-18221.2	-289.39	D578	14.7	17	4	0.04
23819.52	-18225.9	-311.28	D578	14.67	4.24	0.07	0.05

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23814.26	-18220.7	-287.04	D578	14.36	42.9	8.78	18.31
23814.55	-18221	-288.43	D578	13.53	8	0.6	0.16
23819.1	-18225.5	-309.37	D578	11.15	8.47	0.47	0.52
23820.8	-18227.3	-317	D578	10.16	11.4	0.9	4.18
23821.01	-18227.5	-317.95	D578	9.37	6.08	0.31	0.99
23821.18	-18227.7	-318.73	D578	9.24	5.5	0.24	0.62
23820.37	-18226.8	-315.09	D578	9.23	5.74	0.23	1.05
23818.68	-18225.1	-307.47	D578	9.09	7.3	0.36	2.5
23819.95	-18226.4	-313.19	D578	7.77	3.82	0.01	0.05
23818.89	-18225.3	-308.42	D578	7.25	9.73	0.41	2.02
23820.59	-18227	-316.05	D578	7.13	11.67	0.7	2.79
23820.16	-18226.6	-314.14	D578	6.7	3.44	0.16	0.26
23821.78	-18228.3	-321.42	D578	4.95	4	0.08	0.23
23822	-18228.5	-322.37	D578	4.71	3.81	0.08	0.22
23817.65	-18224.1	-302.78	D578	4.57	7.35	0.57	1.26
23817.44	-18223.9	-301.83	D578	4.32	1.2	0.04	0.02
23817.86	-18224.3	-303.74	D578	2.89	7.35	0.58	1.36
23818.48	-18224.9	-306.56	D578	1.77	0.4	0.03	0.15
23818.28	-18224.7	-305.65	D578	1.37	0.8	0.05	0.18
23866.69	-18414.4	-342.51	D579	35.06	75.92	2.83	6.6
23851.85	-18411.7	-394.94	D579	16.05	312	8.76	3.9
23866.42	-18414.3	-343.47	D579	14.4	47.98	1.62	17.57
23867.52	-18414.5	-339.58	D579	13.03	130	5.07	13.6
23867.38	-18414.5	-340.09	D579	13.03	130	5.07	13.6
23866.96	-18414.4	-341.55	D579	12.43	154.92	5.84	12.65
23866.15	-18414.3	-344.43	D579	12.16	51.81	2.03	9.74
23850.73	-18411.5	-398.77	D579	10.9	250	5.99	9.05
23851.01	-18411.6	-397.81	D579	7.17	183	7.27	5.24
23851.29	-18411.6	-396.85	D579	6.89	179	5.64	8.68
23851.57	-18411.7	-395.89	D579	6.55	133	4.64	7.36
23867.79	-18414.6	-338.62	D579	5.25	63.52	2.48	5.57
23850.48	-18411.5	-399.63	D579	4.66	68.7	1.99	4.41
23865.88	-18414.3	-345.4	D579	4.63	27.55	0.97	15.19
23865.61	-18414.2	-346.36	D579	3.36	102.5	4.29	13.1
23868.34	-18414.7	-336.7	D579	2.09	459	17.4	8.28
23863.18	-18413.8	-354.96	D579	1.8	150.28	6.85	6.19
23839.62	-18253.9	-339.89	D580	37.48	4.2	0.07	0.56
23840.74	-18255.6	-344.46	D580	37.34	6.3	0.07	1
23838.71	-18252.6	-336.23	D580	31.68	3.62	0.1	2.33
23839.84	-18254.3	-340.8	D580	30.79	4.84	0.1	0.76
23845.95	-18263.8	-366.24	D580	29.62	75.5	2.24	5.59
23840.51	-18255.3	-343.54	D580	28.3	6.39	0.05	4.43
23839.16	-18253.2	-338.06	D580	26.17	7.07	0.12	3.63

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23837.35	-18250.5	-330.75	D580	24.6	5.89	0.59	0.11
23838.94	-18252.9	-337.15	D580	23.28	6.09	0.18	7.29
23846.16	-18264.1	-367.16	D580	22.29	199	4	9.88
23839.39	-18253.6	-338.97	D580	22.08	8.92	0.17	1.34
23838.26	-18251.9	-334.41	D580	21.72	6.51	0.2	0.03
23836.89	-18249.9	-328.92	D580	20.65	8.05	0.47	0.16
23835.97	-18248.5	-325.26	D580	20.56	92.58	3.21	5.11
23833.75	-18245.4	-316.46	D580	20.37	103.5	3.64	4.46
23840.29	-18254.9	-342.63	D580	20.35	8.1	0.09	7.72
23837.8	-18251.2	-332.58	D580	19.57	11.28	1.18	0.14
23837.12	-18250.2	-329.84	D580	19.46	5.62	0.83	0.09
23837.57	-18250.9	-331.66	D580	19.27	5.82	0.55	0.07
23838.48	-18252.2	-335.32	D580	18.72	2.69	0.14	0.31
23841.18	-18256.3	-346.28	D580	18.6	8.19	0.08	6.61
23838.03	-18251.6	-333.49	D580	18.5	4.82	0.26	0.03
23840.07	-18254.6	-341.71	D580	17.95	16.65	0.47	4.28
23845.73	-18263.4	-365.33	D580	17.21	33.5	0.63	8.57
23845.52	-18263.1	-364.42	D580	15.98	61.1	1.37	3.45
23846.37	-18264.5	-368.07	D580	15.63	285	8.23	9.08
23842.51	-18258.3	-351.76	D580	13.08	11.47	0.18	16.45
23836.43	-18249.2	-327.09	D580	12.37	18	1.69	2.7
23841.4	-18256.6	-347.2	D580	11.25	9.7	0.28	5.11
23832.62	-18243.8	-312.01	D580	10.83	5.25	0.12	0.03
23836.2	-18248.9	-326.18	D580	10.82	12.2	0.87	4.63
23842.29	-18258	-350.85	D580	10.27	12.6	0.28	15.27
23842.73	-18258.7	-352.68	D580	9.72	11.71	0.24	13.69
23844.9	-18262.1	-361.77	D580	9.67	33.7	0.9	4.62
23836.66	-18249.5	-328.01	D580	9.51	8.84	0.91	1.05
23844.03	-18260.7	-358.11	D580	9.06	7.5	0.14	0.25
23845.11	-18262.4	-362.68	D580	8.89	50.98	1.36	3.13
23844.25	-18261.1	-359.03	D580	8.54	5.9	0.07	0.16
23845.32	-18262.8	-363.55	D580	8.37	62.5	1.66	2.13
23843.81	-18260.4	-357.2	D580	7.8	7.94	0.19	0.78
23842.95	-18259	-353.59	D580	7.06	32.4	0.9	9.52
23844.46	-18261.4	-359.94	D580	6.78	9.42	0.24	0.83
23843.12	-18259.3	-354.3	D580	6.58	43	1.22	7.64
23843.59	-18260	-356.29	D580	5.14	6.2	0.15	1.42
23831.76	-18242.6	-308.64	D580	5.02	13.4	0.51	0.67
23832.85	-18244.1	-312.92	D580	4.96	11.9	0.32	0.03
23832.42	-18243.5	-311.24	D580	4.7	54	1.85	0.03
23842.07	-18257.7	-349.94	D580	4.7	1.8	0.03	1.97
23844.68	-18261.8	-360.85	D580	4.7	16.6	0.53	2.12
23846.59	-18264.8	-368.98	D580	4.19	81.68	2.33	2.44

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23832.23	-18243.2	-310.48	D580	3.37	41.58	1.38	0.13
23833.95	-18245.7	-317.26	D580	2.95	21.6	1.23	1.81
23834.18	-18246	-318.17	D580	2.23	38.2	1.86	2.53
23841.85	-18257.3	-349.02	D580	2.23	1.56	0.03	0.83
23843.29	-18259.6	-355.01	D580	2.16	8.1	0.25	0.58
23843.44	-18259.8	-355.65	D580	2.16	8.1	0.25	0.58
23835.11	-18247.3	-321.83	D580	1.75	5.4	0.17	0.37
23835.34	-18247.6	-322.75	D580	1.68	4.44	0.15	0.26
23835.57	-18248	-323.66	D580	1.58	3	0.13	0.09
23835.77	-18248.3	-324.46	D580	1.58	3	0.13	0.09
23834.41	-18246.3	-319.09	D580	1.1	35.83	1.63	2.14
23758.11	-18399	-366.52	D581	2.82	1.4	0	0.01
23757.41	-18398.8	-367.22	D581	2.82	1.4	0	0.01
23800.86	-18316.1	-378.43	D582	26.34	134.65	5.01	5.12
23801.04	-18315	-376.78	D582	20.67	31.1	0.44	3.99
23801.13	-18314.4	-375.95	D582	19.52	19.94	0.31	1.66
23800.77	-18316.6	-379.26	D582	18.82	218	6.24	7.3
23800.68	-18317.2	-380.09	D582	17.11	193	6.06	8.17
23801.21	-18313.9	-375.12	D582	16.71	16.02	0.33	0.48
23802.17	-18307.2	-365.17	D582	15.29	231	5.94	18.5
23802.09	-18307.8	-366	D582	14.47	343	3.4	4.74
23802.24	-18306.7	-364.34	D582	14.16	556	9.14	5.74
23800.45	-18318.6	-382.23	D582	13.44	260	7.68	6.9
23800.95	-18315.5	-377.61	D582	11.93	86.5	2.18	2.72
23800.5	-18318.3	-381.74	D582	11.46	177.76	5.31	5.56
23801.63	-18311.1	-370.98	D582	10.25	28.3	0.67	4.42
23800.59	-18317.7	-380.91	D582	9.79	75.19	2.4	4.25
23801.3	-18313.3	-374.29	D582	6.41	22.75	0.57	1.08
23801.71	-18310.5	-370.15	D582	6.29	65.35	2.11	1.44
23802.02	-18308.3	-366.83	D582	5.66	41.9	0.97	5.61
23804.89	-18271.7	-310.06	D582	4.66	840	28.4	10.6
23804.88	-18272.2	-310.91	D582	4.66	840	28.4	10.6
23804.9	-18270.6	-308.35	D582	4.08	459	13.9	4.3
23804.9	-18271.2	-309.21	D582	4.08	459	13.9	4.3
23801.79	-18310	-369.32	D582	3.67	65	1.98	0.47
23801.94	-18308.9	-367.66	D582	3.46	51.9	1	3.86
23804.93	-18268.1	-304.22	D582	3	232.17	8.41	1.42
23801.38	-18312.7	-373.46	D582	2.67	9.46	0.24	0.17
23801.87	-18309.4	-368.49	D582	2.37	52.3	1.37	0.49
23802.31	-18306.1	-363.51	D582	1.48	55.96	0.93	0.62
23801.46	-18312.2	-372.63	D582	1.37	4.6	0.12	0.15
23893.62	-18364	-405.75	D583	15.03	84.56	3.08	5.35
23893.58	-18364	-406.75	D583	11.49	64.65	2.31	4.03

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23895.36	-18363.3	-356.89	D583	9.6	283	9.65	17.5
23895.42	-18363.2	-354.99	D583	2.61	655	25.3	13.3
23895.53	-18363.2	-351.29	D583	2.06	94.42	3.33	8.28
23895.39	-18363.3	-355.99	D583	1.82	750	29.1	13.1
23895.5	-18363.2	-352.29	D583	1.51	60.4	2.01	6.15
23895.48	-18363.2	-352.89	D583	1.51	60.4	2.01	6.15
23787.81	-18246	-300.81	D584	14.81	3.7	0.11	0.27
23788.13	-18244.9	-298.04	D584	14.74	25.83	1.09	4.26
23787.92	-18245.6	-299.88	D584	12.82	21.65	0.42	0.45
23788.02	-18245.3	-298.96	D584	10.97	3.7	0.11	0.45
23787.6	-18246.7	-302.62	D584	10.46	4	0.27	0.27
23788.23	-18244.5	-297.12	D584	7.61	17.1	1.21	7.64
23785.22	-18254.3	-321.29	D584	7.41	235	8.36	19.2
23785.32	-18254.1	-320.59	D584	6.84	250.3	8.31	20.22
23788.49	-18243.6	-294.81	D584	5.99	15.53	0.82	3.31
23785.57	-18253.3	-318.75	D584	5.07	367	11.1	23.8
23788.39	-18244	-295.73	D584	4.77	14.98	0.73	1.42
23785.44	-18253.7	-319.67	D584	3.63	337	8	26
23785.74	-18252.8	-317.47	D584	2.95	47.3	1.67	2.52
23785.65	-18253	-318.11	D584	2.95	47.3	1.67	2.52
23788.31	-18244.3	-296.42	D584	2.88	8.8	0.56	1.67
23786.1	-18251.6	-314.71	D584	2.85	29.1	1.15	0.93
23788.59	-18243.2	-293.88	D584	2.27	8.16	0.56	1.69
23789.09	-18241.4	-289.26	D584	2.17	15.7	0.71	2.43
23786.59	-18250.1	-310.87	D584	1.97	6.9	0.25	0.5
23786.71	-18249.7	-309.95	D584	1.65	7	0.27	0.43
23787.38	-18247.5	-304.42	D584	1.51	13.61	0.59	0.7
23786.48	-18250.5	-311.79	D584	1.5	4.56	0.16	0.37
23787.27	-18247.8	-305.34	D584	1.41	12.84	0.56	0.64
23787	-18393.6	-287.22	D585	1.37	136.5	2.55	1.1
23861.95	-18383.1	-342.2	D587	49.51	-999	10.6	19
23861.68	-18383.3	-343.15	D587	14.54	16.1	3.01	4.99
23847.24	-18391.8	-395.47	D587	9.05	121.5	3.78	0.8
23861.27	-18383.5	-344.65	D587	3.43	518	18.5	9.7
23861.42	-18383.4	-344.1	D587	3.18	292.14	10.39	5.48
23815.44	-18381.5	-379.96	D588	26.26	98.4	3.05	4
23815.01	-18381.3	-380.84	D588	23.02	113.58	3.34	3.67
23814.59	-18381.1	-381.72	D588	20.63	161	4.49	5.03
23814.16	-18380.9	-382.6	D588	19.09	182.2	5.79	8.57
23815.87	-18381.7	-379.08	D588	15.7	392	9.59	4.41
23813.73	-18380.7	-383.49	D588	13.36	94.63	4.31	9.18
23813.33	-18380.5	-384.32	D588	8.37	54	2.65	8.89
23840.78	-18393.4	-329.06	D588	5.14	178.5	7.04	10.2

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23841.2	-18393.6	-328.23	D588	3.53	137.1	5.43	9.91
23842.09	-18394	-326.48	D588	2.94	180.23	4.8	6.91
23841.64	-18393.8	-327.35	D588	1.1	55.6	2.22	5.53
23733.17	-18247.5	-286.04	D589	26.34	49.9	2.68	11.2
23733.69	-18247.2	-285.25	D589	25.71	39.2	1.31	4.79
23736.75	-18245.2	-280.49	D589	24.09	36.7	2.41	6.24
23735.22	-18246.2	-282.87	D589	20.49	9.7	0.18	2.69
23732.66	-18247.9	-286.83	D589	18.24	188	3.9	5.54
23737.26	-18244.9	-279.69	D589	15.15	112	6.2	6.19
23734.2	-18246.9	-284.45	D589	12.87	48	1.68	13.4
23736.24	-18245.6	-281.28	D589	11.25	13	0.74	9.37
23734.71	-18246.5	-283.66	D589	8.94	167	4.5	8.81
23735.73	-18245.9	-282.07	D589	8.61	12.9	0.26	7.19
23737.77	-18244.6	-278.9	D589	4.83	25.9	1.52	1.43
23738.79	-18243.9	-277.31	D589	2.97	43.8	0.89	1.32
23738.28	-18244.2	-278.11	D589	2.97	43.8	0.89	1.32
23740.81	-18242.5	-274.14	D589	2.19	10.1	0.46	0.36
23740.3	-18242.9	-274.93	D589	2.19	10.1	0.46	0.36
23908.38	-18390.3	-367.48	D591	5.38	51.7	0.84	1.24
23908.39	-18390.2	-368	D591	5.38	51.7	0.84	1.24
23908.29	-18391.7	-359	D591	3.74	353.96	10.04	4.16
23908.37	-18390.5	-366.49	D591	3.24	33.78	0.61	0.86
23908.3	-18391.6	-359.98	D591	1.58	88.4	3.05	2.19
23908.31	-18391.4	-360.77	D591	1.58	88.4	3.05	2.19
23767.81	-18225.8	-295.64	D592	23.25	8.6	0.5	0.19
23772.89	-18221.8	-275.67	D592	14.88	18.1	1.33	1.7
23768.57	-18225.3	-292.78	D592	14.4	6.3	0.52	0.22
23767.56	-18226	-296.59	D592	11.75	6.36	0.24	0.87
23768.32	-18225.5	-293.74	D592	11.65	8	0.87	0.85
23770.06	-18224.2	-287.08	D592	9.05	16.7	1.45	2.37
23769.81	-18224.4	-288.03	D592	9.05	16.7	1.45	2.37
23769.57	-18224.6	-288.98	D592	9.05	16.7	1.45	2.37
23768.06	-18225.6	-294.69	D592	8.91	9.7	1.21	1.48
23767.39	-18226.1	-297.21	D592	8.88	5.8	0.18	1.04
23768.82	-18225.1	-291.83	D592	8.23	6.4	0.46	0.79
23769.07	-18224.9	-290.88	D592	5.42	7.6	0.44	0.93
23771.97	-18222.6	-279.47	D592	2.69	0.96	0.03	0.07
23769.32	-18224.7	-289.93	D592	2.61	8.8	0.42	1.06
23767.22	-18226.2	-297.83	D592	2.61	4.8	0.09	1.17
23766.71	-18226.6	-299.73	D592	2.1	28.27	0.96	1.54
23766.46	-18226.7	-300.68	D592	1.99	22.99	0.79	1.18
23770.78	-18223.6	-284.23	D592	1.89	4.7	0.22	0.98
23770.54	-18223.8	-285.18	D592	1.89	4.7	0.22	0.98

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23771.73	-18222.8	-280.42	D592	1.72	0.6	0.01	0.03
23766.97	-18226.4	-298.78	D592	1.68	6.24	0.43	0.97
23771.26	-18223.2	-282.32	D592	1.44	2.4	0.13	0.28
23839.21	-18349	-336.8	D593	35.1	137.07	5.03	0.86
23838.81	-18349	-337.71	D593	33.29	90.42	3.21	2.26
23815.57	-18344.6	-390.83	D593	24.27	2.7	5.79	13.5
23819.46	-18345.3	-381.93	D593	19.2	125.75	4.27	6.85
23821.06	-18345.7	-378.27	D593	19.02	55.92	1.83	6.48
23821.45	-18345.7	-377.36	D593	16.01	226	9.44	6.58
23821.85	-18345.8	-376.45	D593	13.23	120.5	5.05	2.3
23819.06	-18345.3	-382.84	D593	12.74	215	7.35	6.37
23818.66	-18345.2	-383.75	D593	12.1	337.57	9.63	8.12
23815.87	-18344.6	-390.15	D593	11.13	67.08	2.35	5.48
23839.61	-18349.1	-335.88	D593	9.77	354.5	11.83	12.11
23838.41	-18348.9	-338.62	D593	9.53	69.9	2.66	11
23817.06	-18344.9	-387.41	D593	8.68	90.45	2.37	4.01
23819.86	-18345.4	-381.01	D593	8.41	43.53	1.31	2.29
23818.26	-18345.1	-384.67	D593	7.85	26.7	0.73	5.36
23817.46	-18345	-386.49	D593	6.38	47.64	1.17	2.59
23817.86	-18345	-385.58	D593	5.26	13.14	0.32	0.81
23816.66	-18344.8	-388.32	D593	5.21	3.9	0.08	0.08
23816.26	-18344.7	-389.24	D593	3.79	56.95	0.07	0.11
23841.25	-18349.4	-332.14	D593	3.75	40.62	1.06	1.79
23822.67	-18346	-374.57	D593	3.04	2.63	0.09	0.92
23838.01	-18348.8	-339.54	D593	3.01	22.44	0.85	3.53
23840.85	-18349.3	-333.05	D593	2.64	60.6	1.81	3.28
23820.26	-18345.5	-380.1	D593	2.49	3.3	0.11	0.19
23836.54	-18348.6	-342.9	D593	2.47	185	7.22	5.29
23836.81	-18348.6	-342.28	D593	2.44	133.08	5.2	3.97
23837.21	-18348.7	-341.37	D593	2.41	61.92	2.42	4.41
23820.66	-18345.6	-379.19	D593	2.37	1.2	0.08	0.09
23823.07	-18346	-373.66	D593	2.34	1.6	0.07	0.7
23840.01	-18349.2	-334.97	D593	2.28	207.55	7.37	3.87
23837.61	-18348.7	-340.45	D593	1.54	44.04	1.71	4.95
23841.65	-18349.5	-331.23	D593	1.4	8.61	0.17	0.24
23793.28	-18246.9	-273.73	D594	13.22	50.85	4.78	3.11
23793.28	-18246.4	-272.85	D594	6.61	27.47	2.99	2.5
23950.54	-18388.8	-386.89	D595	32.87	92.91	3.63	13.74
23950.34	-18389	-385.92	D595	18.4	159.1	5.41	19.96
23950.14	-18389.1	-384.96	D595	13.59	277.15	9.76	15.22
23949.94	-18389.3	-383.99	D595	10.56	478	17.4	4.85
23949.73	-18389.4	-383.02	D595	8.35	418.5	15.37	7.64
23949.53	-18389.6	-382.06	D595	7.22	478.75	16.99	6.91

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23949.33	-18389.8	-381.09	D595	4.99	408.24	13.86	2.38
23950.95	-18388.5	-388.82	D595	3.98	186.82	6.96	14.83
23949.12	-18389.9	-380.13	D595	2.19	63.6	2.26	0.93
23948.92	-18390.1	-379.16	D595	1.45	514.23	18.84	16.82
23948.51	-18390.4	-377.23	D595	1.34	47.7	1.5	3.13
23948.72	-18390.3	-378.19	D595	1.34	478.33	17.36	17.92
23785.44	-18340.4	-294.61	D596	3.94	266	9.34	14.6
23784.77	-18340.3	-295.11	D596	2.6	129.04	4.67	6.54
23779.34	-18339.1	-299.12	D596	1.3	40.7	1.38	0.94
23767.4	-18189	-282.4	D597	8.47	46.18	3.03	8.47
23767.2	-18189	-283.14	D597	8.33	37.7	3.01	5.91
23767.92	-18189.2	-280.47	D597	6.1	36.2	2.03	5.54
23767.66	-18189.1	-281.44	D597	5.82	35.99	1.92	7.1
23861.58	-18296.9	-344.32	D600	37.68	209	7.06	4.82
23854.41	-18284.5	-372.81	D600	33.81	238	7.18	8.79
23854.18	-18284.1	-373.7	D600	33.81	238	7.18	8.79
23861.8	-18297.3	-343.42	D600	32.6	257.3	8.79	5.88
23861.36	-18296.5	-345.21	D600	26.99	192.85	6.07	1.86
23861.14	-18296.1	-346.11	D600	25.1	190	5.9	1.34
23857.08	-18289.1	-362.34	D600	24.21	90.5	2.83	2.36
23856.85	-18288.7	-363.23	D600	24.21	90.5	2.83	2.36
23854.86	-18285.3	-371.03	D600	14.57	37.1	1.11	14.1
23854.64	-18284.9	-371.92	D600	14.57	37.1	1.11	14.1
23860.91	-18295.8	-347.01	D600	8.64	139	4.65	8.96
23853.96	-18283.7	-374.59	D600	7.34	309	10.3	8.75
23853.73	-18283.3	-375.49	D600	7.34	309	10.3	8.75
23853.54	-18283	-376.22	D600	7.34	309	10.3	8.75
23858.91	-18292.3	-355.06	D600	6.69	66.9	2.55	20.3
23859.13	-18292.7	-354.17	D600	6.07	72.01	2.78	18.78
23860.69	-18295.4	-347.9	D600	5.73	130	4.43	10.3
23855.32	-18286.1	-369.25	D600	5.69	40	1.14	1.76
23855.09	-18285.7	-370.14	D600	5.69	40	1.14	1.76
23862.46	-18298.4	-340.73	D600	4.22	263	9.31	10.1
23862.24	-18298.1	-341.62	D600	3.92	477.4	16.74	11.54
23862.02	-18297.7	-342.52	D600	3.84	531	18.6	11.9
23859.8	-18293.8	-351.49	D600	3.53	77.9	2.94	3.5
23863.34	-18300	-337.13	D600	3.26	209	8.65	10.2
23858.68	-18291.9	-355.96	D600	3.07	129.88	5.99	7.94
23863.78	-18300.7	-335.33	D600	3.06	474.23	9.71	7.61
23863.12	-18299.6	-338.03	D600	3.05	278.46	11.03	11.44
23860.03	-18294.2	-350.59	D600	3.01	66.85	2.5	2.99
23859.58	-18293.5	-352.38	D600	2.69	97.54	3.88	9.19
23862.68	-18298.8	-339.83	D600	2.56	481.24	17.84	14.94

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23859.36	-18293.1	-353.27	D600	2.54	101	4.05	10.2
23858.53	-18291.6	-356.58	D600	2.43	141	6.6	5.76
23862.9	-18299.2	-338.93	D600	2.33	511	19	15.6
23858.37	-18291.4	-357.21	D600	1.13	14.3	0.42	0.39
23858.15	-18291	-358.1	D600	1.13	14.3	0.42	0.39
23817.61	-18179.9	-311.77	D601	29.01	126	1.99	5.73
23817.51	-18180	-311.13	D601	26.22	98.7	1.57	4.44
23817.35	-18180.1	-310.15	D601	17.58	108.48	0.97	2.83
23817.19	-18180.2	-309.18	D601	17.21	246	1.98	6.21
23816.94	-18180.5	-307.61	D601	6.45	27.1	1.01	1
23816.62	-18180.7	-305.65	D601	5.49	1.4	0	0.01
23816.78	-18180.6	-306.63	D601	5.49	1.4	0	0.01
23815.66	-18181.5	-299.78	D601	1.82	4.7	0.28	0.85
23815.82	-18181.4	-300.76	D601	1.82	4.7	0.28	0.85
23873.65	-18324.5	-350.79	D603	17.12	39.49	2.44	5.27
23873.82	-18324.7	-349.83	D603	11.26	56.64	2.76	4.78
23874	-18324.9	-348.86	D603	4.29	289	10.2	15.2
23868.26	-18318.2	-381.29	D603	1.62	128.71	3.82	1.17
23867.75	-18317.6	-384.18	D603	1.1	162.03	6.22	4.41
23825.64	-18201.5	-308.68	D604	18.87	7	0.2	0.39
23825.85	-18201.5	-309.66	D604	15.48	5.55	0.17	0.43
23824	-18201.2	-300.85	D604	13.2	11.9	1.16	2.11
23824.21	-18201.3	-301.83	D604	13.2	11.9	1.16	2.11
23826.04	-18201.6	-310.59	D604	12.09	4.1	0.15	0.46
23826.57	-18201.6	-313.08	D604	11.31	37	1	1.77
23826.74	-18201.7	-313.91	D604	11.31	37	1	1.77
23823.7	-18201.2	-299.39	D604	8.46	5.5	0.47	0.03
23823.85	-18201.2	-300.12	D604	8.46	5.5	0.47	0.03
23825.23	-18201.4	-306.72	D604	7.89	8.3	0.61	2.54
23825.44	-18201.5	-307.7	D604	7.89	8.3	0.61	2.54
23824.82	-18201.4	-304.77	D604	5.88	7.4	0.86	2.69
23825.03	-18201.4	-305.74	D604	5.88	7.4	0.86	2.69
23824.41	-18201.3	-302.81	D604	4.44	12.6	1.3	3.34
23824.62	-18201.3	-303.79	D604	4.44	12.6	1.3	3.34
23823.49	-18201.1	-298.41	D604	4.24	4.2	0.25	0.05
23826.24	-18201.6	-311.52	D604	1.86	0.8	0.02	0.08
23826.4	-18201.6	-312.3	D604	1.86	0.8	0.02	0.08
23826.92	-18201.7	-314.74	D604	1.77	1.1	0.02	0.03
23827.74	-18201.8	-318.66	D604	1.56	18.6	0.67	0.09
23827.53	-18201.8	-317.68	D604	1.44	13.8	0.51	0.1
23827.12	-18201.7	-315.72	D604	1.35	2.15	0.1	0.11
23827.33	-18201.8	-316.7	D604	1.17	2.6	0.13	0.14
23982.14	-18577.9	-429.14	D605	12.73	65.42	2.5	4.77

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23982.14	-18577.9	-437.57	D605	11.59	29	1.23	6.92
23982.14	-18577.9	-430.09	D605	9.33	88.8	3.48	9.53
23982.14	-18577.9	-427.04	D605	1.51	9.2	0.27	0.55
23982.14	-18577.9	-428.04	D605	1.51	9.2	0.27	0.55
23982.14	-18577.9	-428.59	D605	1.51	9.2	0.27	0.55
24004.18	-18085.9	-284.28	D606	7.68	274	8.4	21.4
24004.23	-18085.8	-283.28	D606	3.57	596.4	16.72	19.72
24004.28	-18085.8	-282.28	D606	1.14	271.16	7.54	7.74
23996.99	-18071.5	-281.12	D608	8.41	98.8	2.78	4.22
23997.21	-18071.9	-280.24	D608	2.79	41.78	1.15	1.94
23979.46	-18608.2	-422.93	D611	5.49	7	0.25	0.06
23979.44	-18608.4	-423.92	D611	5.49	7	0.25	0.06
23979.7	-18606.5	-410.65	D611	4.97	8.6	0.33	0.13
23979.68	-18606.7	-411.64	D611	4.97	8.6	0.33	0.13
23979.34	-18609.1	-428.87	D611	4.59	137	5.07	8.96
23979.33	-18609.2	-429.56	D611	4.59	137	5.07	8.96
23978.44	-18615.5	-474.97	D611	1.75	463	19.4	19.2
23978.42	-18615.6	-475.84	D611	1.75	463	19.4	19.2
23978.37	-18616	-478.58	D611	1.61	238	8.69	13
23978.35	-18616.1	-479.37	D611	1.61	238	8.69	13
23980.62	-18600	-363.51	D611	1.53	18.94	0.28	0.79
23980.6	-18600.1	-364.5	D611	1.53	18.94	0.28	0.79
23979.64	-18606.9	-413.62	D611	1.44	9.1	0.34	0
23979.62	-18607.1	-414.61	D611	1.44	9.1	0.34	0
23979.4	-18608.7	-425.9	D611	1.44	5.1	0.17	0.1
23883	-18269.3	-385.35	D615	12.93	155.58	6.15	4.71
23885.93	-18285.6	-351.43	D615	5.97	538	17	0.82
23886	-18286	-350.74	D615	3.44	284.86	9.03	0.54
23949.73	-18629.4	-350.6	D616	12.39	13.19	0.61	0.15
23949.49	-18629.7	-351.52	D616	9.39	6.5	0.21	0.12
23947.78	-18632	-357.92	D616	8.16	10.8	0.46	0.14
23950.46	-18628.4	-347.86	D616	7.75	27.09	0.5	0.85
23950.22	-18628.8	-348.77	D616	7.75	7.3	0.29	1.47
23948.76	-18630.7	-354.26	D616	6.48	10.9	0.38	0.1
23948.52	-18631	-355.18	D616	6.44	10.75	0.38	0.1
23948.27	-18631.3	-356.09	D616	5.01	5.8	0.26	0.06
24030.14	-18094.6	-298.13	D617	75.77	97.5	3.07	0.72
24030.56	-18094.7	-299.03	D617	68.23	127.5	4.11	4.65
24029.72	-18094.5	-297.23	D617	46.05	346	9.94	0.1
24029.3	-18094.4	-296.34	D617	44.16	60.3	1.87	0.71
24033.5	-18095.6	-305.32	D617	42.07	84.3	2.59	1.3
24033.92	-18095.7	-306.22	D617	28.87	182.5	5.85	9.7
24037.71	-18096.9	-314.31	D617	12.48	128	3.62	3.79

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24036.02	-18096.4	-310.72	D617	9.63	31.2	1	6.74
24035.18	-18096.1	-308.92	D617	8.02	18.6	0.58	4.24
24038.13	-18097	-315.21	D617	7.17	153.5	5.27	1.09
24040.23	-18097.6	-319.7	D617	6.31	44.1	1.77	5.29
24039.39	-18097.4	-317.91	D617	6.24	127.5	4.76	10.9
24041.07	-18097.9	-321.5	D617	6.07	104.5	3.45	7.29
24034.76	-18096	-308.02	D617	4.94	11.7	0.35	2.75
24037.29	-18096.7	-313.41	D617	4.9	125	3.1	4.08
24035.6	-18096.2	-309.82	D617	4.63	19.5	0.57	5.78
24034.34	-18095.9	-307.12	D617	4.53	84	3.05	8.92
24039.81	-18097.5	-318.8	D617	4.18	393	12.4	20.8
24040.65	-18097.7	-320.6	D617	3.43	91.2	3.58	6.11
24033.08	-18095.5	-304.42	D617	2.43	12.9	0.43	0
24038.97	-18097.2	-317.01	D617	2.26	60	2.07	10.7
24029.02	-18094.3	-295.75	D617	2.06	1.8	0.02	0.15
24028.75	-18094.2	-295.17	D617	1.65	2.07	0.04	0.16
24041.49	-18098	-322.4	D617	1.51	15.3	0.93	0.47
24020.82	-18066.1	-279.88	D619	41.04	9.41	0.28	1.03
24020.45	-18066.6	-279.11	D619	35.79	18.3	0.7	0.04
24021.19	-18065.5	-280.64	D619	35.25	37.03	1.04	3.97
24021.43	-18065.2	-281.14	D619	31.8	50.5	1.44	5.05
24024.28	-18061.1	-287.06	D619	14.61	290	11	8.73
24023.92	-18061.7	-286.31	D619	6.3	67.82	2.39	1.47
23932.73	-18569.2	-456.3	D620	1.78	617	20.3	16.6
23939.83	-18570.5	-419.12	D620	1.58	531	16.6	22.3
23928.91	-18288.1	-419.48	D622	6.31	148.08	3.06	1.82
23972.15	-18515.3	-447.89	D623	21.91	173.5	4.44	7.24
23972.04	-18514.6	-450.8	D623	21.26	239	7.36	0.9
23972	-18514.4	-451.78	D623	19.75	213	7.07	1.83
23972.08	-18514.8	-449.83	D623	18.93	222	8.18	2.93
23972.11	-18515.1	-448.86	D623	18.27	41	1.41	11.6
23971.93	-18513.9	-453.72	D623	17.9	83.5	2.18	8.32
23971.97	-18514.2	-452.75	D623	15.91	167.5	3.67	2.37
23971.89	-18513.7	-454.69	D623	13.1	284	8.89	14.3
23972.19	-18515.5	-446.92	D623	12.89	202	6.38	8.58
23972.63	-18518.3	-435.25	D623	12.34	42.2	1.61	1.85
23972.59	-18518.1	-436.22	D623	12.34	42.2	1.61	1.85
23972.26	-18516	-444.97	D623	11.73	179	5.01	9.71
23971.86	-18513.5	-455.67	D623	11.21	120	5.52	9.39
23973.97	-18526.2	-401.7	D623	11.04	77.8	2.74	20.7
23972.67	-18518.5	-434.27	D623	10.62	41.26	1.73	1.4
23974.01	-18526.5	-400.73	D623	10.35	50.5	1.73	23.3
23972.22	-18515.8	-445.94	D623	10.35	180.5	5.23	12.9

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23974.05	-18526.7	-399.76	D623	9.43	48.7	1.5	22
23974.28	-18528	-394.31	D623	7.52	222.87	8.3	18.11
23974.24	-18527.8	-395.23	D623	7.3	50.7	1.5	19.1
23972.56	-18517.8	-437.19	D623	6.61	23.15	0.88	1.03
23973.75	-18525	-407.05	D623	6.27	6.2	0.68	0.75
23973.79	-18525.2	-406.08	D623	4.75	8.44	0.57	5.53
23974.47	-18529.1	-389.67	D623	3.36	316	13.4	20.7
23972.3	-18516.2	-444	D623	2.33	34.5	1.11	1.64
23973.93	-18526	-402.67	D623	2.19	74.8	2.67	37.6
23973.9	-18525.8	-403.4	D623	2.19	74.8	2.67	37.6
23971.82	-18513.2	-456.64	D623	1.85	185	6.46	11.5
23972.33	-18516.5	-443.03	D623	1.66	24.24	0.78	1.15
23972.74	-18519	-432.33	D623	1.3	15.4	0.46	1.39
23972.71	-18518.8	-433.3	D623	1.3	15.4	0.46	1.39
24042.61	-18561.2	-408.84	D625	4.25	904	29	5
24042.88	-18561.1	-409.81	D625	3.5	372	12	15.4
24043.08	-18561.1	-410.53	D625	3.5	372	12	15.4
24037.93	-18562.1	-392.21	D625	2.26	453	14.2	12.4
24044.37	-18560.8	-415.09	D625	1.85	296	2.18	3.1
24013.72	-18144.1	-298.75	D628	35.24	319.62	7.93	3.66
24012.38	-18144.4	-300.21	D628	22.71	230.09	7.46	1.58
24020.09	-18142.9	-291.81	D628	12.97	120.38	3.9	11.01
24013.05	-18144.2	-299.48	D628	12.37	121.08	4.02	4.79
24019.42	-18143	-292.55	D628	10.24	49.82	1.64	3.38
24019.06	-18143.1	-292.95	D628	9.84	42.3	1.39	2.42
24023.43	-18142.2	-288.15	D628	9.66	599.2	18.24	11.72
24022.1	-18142.5	-289.62	D628	9.39	119	4.11	8.67
24006.97	-18145.4	-306.01	D628	8.09	242	8.13	13.8
24021.43	-18142.6	-290.35	D628	8	157.15	5.14	8.79
24009	-18145	-303.84	D628	7.29	88.92	2.96	10.54
24024.1	-18142.1	-287.42	D628	6.99	602	18.8	11.3
24020.76	-18142.7	-291.08	D628	6.94	147.1	4.39	5.01
24007.65	-18145.3	-305.29	D628	5.9	171.11	5.74	10.47
24016.01	-18143.7	-296.27	D628	5.28	33.6	1.06	9.22
24026.09	-18141.7	-285.21	D628	5.14	265	8.76	4.65
24025.43	-18141.8	-285.95	D628	4.97	588	17.4	8.66
24008.32	-18145.1	-304.56	D628	4.39	41.17	1.34	7.87
24011.7	-18144.5	-300.94	D628	2.19	54.9	1.71	4
24004.93	-18145.8	-308.18	D628	2.09	164.5	4.45	16.8
24004.57	-18145.8	-308.56	D628	2.09	164.5	4.45	16.8
24005.61	-18145.6	-307.46	D628	1.91	226.38	7.32	22.95
24011.03	-18144.6	-301.66	D628	1.79	44.76	1.39	3.27
24015.34	-18143.8	-297	D628	1.7	11.55	0.37	2.98

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24011.84	-18180.3	-300.55	D629	9.91	341.1	9.87	15.22
24011.38	-18180.7	-301.05	D629	9.63	101.5	2.95	23.7
23940.29	-18363.9	-376.04	D630	5.07	230	8.78	9.31
23940.48	-18363.9	-377.02	D630	2.3	103.83	3.97	4.21
23941.96	-18364.2	-384.32	D630	1.21	70.4	1.89	0.88
23525.2	-17811.1	-42.11	D631	45.12	71.2	4.46	7.35
23524.96	-17810.9	-41.5	D631	10.35	33.9	3.27	5.15
23524.28	-17810.2	-39.74	D631	7.82	14.9	0.91	1.51
23525.77	-17811.7	-43.61	D631	2.76	19.42	0.51	1.53
23528.22	-17814.1	-50.04	D631	2.07	16.48	0.36	0.34
23524.62	-17810.5	-40.62	D631	1.95	6	0.26	1.13
23525.44	-17811.4	-42.73	D631	1.83	49.3	1.11	1.14
23526.11	-17812	-44.49	D631	1.5	12.14	0.04	0.2
23526.45	-17812.4	-45.36	D631	1.18	15.64	0.08	0.31
23527.22	-17813.1	-47.39	D631	1.09	11.06	0.88	0.84
23515.07	-17801.5	-39.42	D632	36.07	476	5.79	11.1
23515.05	-17801.5	-40.42	D632	20.19	31	1.78	3.24
23515.12	-17801.5	-36.42	D632	19.58	323	3.72	3.05
23515.1	-17801.5	-37.42	D632	18	130	2.07	6.6
23515.09	-17801.5	-38.42	D632	15.84	87.8	2.78	3.09
23515.04	-17801.5	-41.42	D632	13.99	87.2	1.1	1.31
23515.02	-17801.5	-42.42	D632	7.54	20.8	1.97	1.68
23514.29	-17801.8	-79.41	D632	4.83	88.7	0.32	0.14
23515.15	-17801.5	-34.42	D632	4.32	29	0.69	0.54
23514.72	-17801.7	-60.92	D632	3.19	3.7	0.02	0.44
23515.17	-17801.5	-33.42	D632	2.78	9.3	0.46	0.56
23514.73	-17801.6	-59.92	D632	2.69	3.2	0.03	0.28
23514.32	-17801.8	-78.41	D632	2.61	38.8	0.23	0.61
23514.62	-17801.7	-66.67	D632	2.3	3.3	0.07	0.92
23514.75	-17801.6	-58.92	D632	2.19	2.7	0.04	0.11
23514.54	-17801.7	-70.41	D632	2.16	6	0.09	0.37
23515.13	-17801.5	-35.42	D632	1.89	30.1	0.37	1.86
23514.52	-17801.7	-71.41	D632	1.71	14.3	0.1	0.42
23514.56	-17801.7	-69.41	D632	1.65	5.3	0.14	0.2
23514.61	-17801.7	-67.42	D632	1.58	3.7	0.11	0.2
23515	-17801.5	-43.42	D632	1.27	1.8	0.03	0.18
23514.44	-17801.7	-74.41	D632	1.03	36.5	0.13	0.5
24032.09	-18171.6	-316.23	D633	37.71	177	5.5	3.58
24030.46	-18173.7	-320.42	D633	34.56	223.6	7.04	4.19
24032.41	-18171.1	-315.39	D633	32.09	311	9.16	7.88
24029.49	-18175.1	-322.94	D633	30.78	178.2	5.82	5.34
24029.16	-18175.5	-323.78	D633	28.38	242.8	7.42	5.47
24031.76	-18172	-317.07	D633	26.69	136	3.98	1.43

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24028.84	-18175.9	-324.61	D633	24.59	114.98	3.84	4.57
24034.04	-18168.9	-311.2	D633	24.14	99.6	3.09	1.35
24032.74	-18170.7	-314.55	D633	16.8	185.5	5.51	4.21
24030.14	-18174.2	-321.26	D633	16.56	176.7	6.04	6.98
24034.36	-18168.5	-310.36	D633	16.25	34.8	1.28	0.77
24033.71	-18169.4	-312.04	D633	15.98	110.5	3.38	9.76
24031.44	-18172.4	-317.91	D633	15.98	16.2	0.4	0.26
24027.86	-18177.2	-327.13	D633	14.81	171.7	5.39	12.69
24029.81	-18174.6	-322.1	D633	12.94	168.2	5.93	8.85
24033.39	-18169.8	-312.88	D633	12.31	42.6	1.3	0.16
24027.54	-18177.7	-327.97	D633	10.74	308.9	10.56	14.87
24028.19	-18176.8	-326.29	D633	10.35	295.29	9.72	10.59
24027.21	-18178.1	-328.81	D633	7.94	280.1	8.45	15.19
24025.59	-18180.3	-333	D633	4.83	194.7	7.47	16.62
24034.69	-18168.1	-309.52	D633	4.66	75.6	2.08	1.81
24026.56	-18179	-330.48	D633	4.62	676.4	21.26	11.55
24026.89	-18178.6	-329.64	D633	4.03	226.4	7.48	12.32
24033.06	-18170.2	-313.71	D633	3.5	26.7	0.78	0.18
24024.61	-18181.6	-335.51	D633	3.22	258.6	8.43	10.75
24025.26	-18180.7	-333.84	D633	3.17	175.32	7.11	11.57
24024.29	-18182.1	-336.35	D633	3.12	387	12.5	15.3
24024.06	-18182.4	-336.94	D633	3.12	387	12.5	15.3
24025.91	-18179.9	-332.16	D633	2.75	82.04	2.94	9.79
24035.01	-18167.6	-308.68	D633	2.74	8.1	0.12	0.09
24024.94	-18181.2	-334.68	D633	2.61	105.38	3.42	8.02
24026.24	-18179.4	-331.32	D633	2.45	310.24	9.91	6.99
24028.51	-18176.4	-325.45	D633	1.3	54.9	1.79	0.59
24061.76	-18628.1	-454.06	D634	18.65	8.18	0.33	1.84
24062.57	-18628.8	-456.86	D634	13.3	12.9	0.44	2.32
24062.71	-18629	-457.35	D634	13.3	12.9	0.44	2.32
24061.49	-18627.9	-453.12	D634	12.97	7.41	0.29	2.71
24058.72	-18625.6	-443.64	D634	12.89	54.3	1.7	6.68
24058.87	-18625.7	-444.16	D634	12.89	54.3	1.7	6.68
24061.22	-18627.7	-452.19	D634	10.01	12	0.5	5.58
24053.83	-18621.5	-426.71	D634	8.16	373.05	11.18	13.84
24059.73	-18626.4	-447.08	D634	7.82	59.7	2.28	10.1
24053.56	-18621.2	-425.77	D634	6.46	103.05	3.01	13.9
24062.03	-18628.4	-454.99	D634	5.97	3.13	0.11	0.47
24059.49	-18626.2	-446.26	D634	5.89	66.84	2.43	16.05
24054.36	-18621.9	-428.58	D634	5.86	25.67	0.8	8.51
24052.24	-18620.1	-421.08	D634	5.76	112.5	2.11	10.2
24052.5	-18620.3	-422.02	D634	5.16	41.22	1.11	9.62
24062.3	-18628.6	-455.93	D634	5.09	2.83	0.08	0.23

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24059.02	-18625.8	-444.67	D634	4.08	13.8	0.49	1.21
24059.26	-18626	-445.47	D634	4.08	13.8	0.49	1.21
24054.63	-18622.1	-429.52	D634	3.77	81.25	2.81	2.53
24064.8	-18630.8	-464.67	D634	3.63	261	9.89	13.7
24065.06	-18631	-465.61	D634	3.63	261	9.89	13.7
24065.27	-18631.2	-466.33	D634	3.63	261	9.89	13.7
24052.77	-18620.6	-422.96	D634	2.99	11.34	0.39	4.7
24054.1	-18621.7	-427.65	D634	2.82	128.94	4.24	3.67
24054.9	-18622.4	-430.46	D634	2.38	99.13	3.59	14.32
24053.03	-18620.8	-423.9	D634	2.05	12.9	0.34	2.98
24055.15	-18622.6	-431.35	D634	1.92	25.5	0.64	29.9
24058.56	-18625.4	-443.08	D634	1.23	1.2	0.06	0.05
24047.61	-18616.3	-404.65	D634	1.22	172.5	3.22	1.16
24058.39	-18625.3	-442.52	D634	1.09	1.29	0.06	0.07
24061	-18627.5	-451.44	D634	1.03	42.6	1.5	19.8
24045.31	-18221.7	-366.28	D636	50.51	249	7.26	5.31
24045.44	-18221.1	-365.47	D636	46.27	121.8	3.65	1.68
24045.7	-18220	-363.85	D636	39.78	150.32	5.01	4.07
24045.96	-18218.8	-362.23	D636	31.84	181.9	6.33	6.82
24045.18	-18222.3	-367.09	D636	28.35	357.4	9.33	6.01
24045.57	-18220.5	-364.66	D636	26.34	51.48	1.51	1.41
24046.09	-18218.2	-361.42	D636	25.47	114.14	3.91	4.63
24045.83	-18219.4	-363.04	D636	25.39	188.8	6.39	4.78
24046.22	-18217.7	-360.61	D636	19.83	110.36	3.79	5.53
24046.34	-18217.1	-359.8	D636	14.66	228.3	8.09	8.74
24046.6	-18215.9	-358.19	D636	14.16	199.8	6.99	12.44
24046.72	-18215.4	-357.38	D636	13.73	191.95	6.41	12.16
24046.47	-18216.5	-359	D636	11.08	295.4	10.55	13.89
24046.85	-18214.8	-356.57	D636	10.56	235	7.36	13
24044.54	-18225	-370.97	D636	6.31	69.9	2.4	19.2
24044.41	-18225.6	-371.78	D636	6.31	69.9	2.4	19.2
24046.98	-18214.2	-355.76	D636	5.9	242.2	7.9	17.72
24047.35	-18212.5	-353.33	D636	4.53	801	26.7	2.56
24047.1	-18213.6	-354.95	D636	4.28	267.4	8.65	14.53
24047.48	-18211.9	-352.52	D636	4.25	997	31.7	1.13
24047.23	-18213.1	-354.14	D636	3.22	322	10.1	4.32
24045.06	-18222.8	-367.81	D636	2.67	215	5.84	0.19
24050.45	-18197.4	-332.14	D636	1.17	1.2	0	0
24050.34	-18198	-332.94	D636	1.03	1.11	0	0
23964.91	-18385.4	-390.67	D637	25.68	37.8	1.42	13.9
23963.39	-18384.5	-385.45	D637	8.25	548.07	21.55	13.15
23963.67	-18384.7	-386.4	D637	7.23	86.7	3	15.2
23962.83	-18384.2	-383.56	D637	5.86	539.35	21.22	15.56

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23962.55	-18384.1	-382.61	D637	2.71	244.13	9.35	17.45
23961.99	-18383.8	-380.72	D637	1.68	172.44	6.34	1.2
23523.43	-17843.4	-47.83	D638	23.59	28.47	3.38	0.74
23519.93	-17824.3	-33.71	D638	1.88	1.8	0.01	0.13
23519.77	-17823.5	-33.13	D638	1.68	1.8	0.01	0.09
23520.08	-17825.1	-34.3	D638	1.32	5.15	0.04	0.23
24051.24	-18151.3	-318.09	D639	21.36	297.72	9.81	15.2
24051.47	-18150.9	-316.14	D639	18.31	87	3.04	3.67
24050.32	-18152.9	-325.75	D639	7.95	167	5.82	12.4
24050.78	-18152.2	-321.98	D639	7.81	280.99	9.28	8.62
24050.66	-18152.4	-322.95	D639	7.37	427.88	11.83	8.67
24050.43	-18152.8	-324.89	D639	6.99	420.98	11.78	10.14
24050.54	-18152.6	-323.92	D639	6.07	665	17.5	7.96
24050.89	-18152	-321.01	D639	5.28	522	18.3	6.23
24051.01	-18151.8	-320.03	D639	2.71	266.63	9.34	3.19
23516.32	-17813	-38.16	D640	36.84	69.75	4.34	2.56
23516.08	-17810.4	-33.32	D640	29.86	109.72	1.37	0.41
23516.12	-17810.9	-34.2	D640	5.79	12.9	0.48	1
23516.35	-17813.4	-38.82	D640	2.33	26.7	0.31	0.59
23516.28	-17812.7	-37.5	D640	1.65	1.8	0.13	0.06
23516.21	-17811.8	-35.96	D640	1.51	3.3	0.13	0.01
23516.25	-17812.3	-36.84	D640	1.51	3.3	0.13	0.08
24068.46	-18185.1	-340.66	D641	23.13	59.91	1.83	4.34
24068.4	-18184.6	-339.78	D641	22.68	167.16	5.06	7.04
24067.24	-18176.7	-324.77	D641	12.73	32.79	0.89	3.59
24067.31	-18177.2	-325.65	D641	10.91	21.63	0.56	3.67
24068.66	-18186.5	-343.31	D641	10.83	63.3	1.55	1.36
24067.52	-18178.6	-328.3	D641	8.85	116.5	3.42	7.09
24067.45	-18178.1	-327.42	D641	8.47	16.78	0.44	0.86
24067.38	-18177.7	-326.53	D641	7.62	9.48	0.21	2.03
24068.83	-18187.7	-345.6	D641	7.17	159	5.92	12.6
24067.93	-18181.4	-333.6	D641	7.03	13.2	0.28	0.36
24068.59	-18186	-342.43	D641	6.9	21.51	0.52	0.59
24068.79	-18187.4	-345.07	D641	6.65	336.2	11.22	13.02
24067.16	-18176.3	-323.88	D641	6.58	28.8	0.8	1.03
24067.86	-18180.9	-332.71	D641	6.51	16.26	0.34	0.3
24068	-18181.8	-334.48	D641	6.48	35.72	0.93	1.21
24068.06	-18182.3	-335.36	D641	6.33	36.57	0.95	1.28
24068.53	-18185.6	-341.54	D641	6.04	4.41	0.11	0.4
24068.73	-18187	-344.19	D641	5.5	897.74	27.77	12.7
24068.27	-18183.7	-338.01	D641	4.94	46.8	1.48	1.51
24068.2	-18183.2	-337.13	D641	4.6	41.03	1.26	1.65
24067.79	-18180.4	-331.83	D641	4.42	28.5	0.59	0.05

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24068.13	-18182.8	-336.25	D641	3.98	30.3	0.84	1.9
24067.72	-18180	-330.95	D641	3.02	19.05	0.39	0.04
24068.33	-18184.2	-338.89	D641	2.7	13.65	0.37	0.49
24067.59	-18179.1	-329.18	D641	2.15	13.26	0.38	0.74
24043.56	-18648.3	-453.14	D642	19.32	130.25	4.78	7.28
24043.34	-18648.1	-452.21	D642	17.54	80.5	3.2	6.67
24042.89	-18647.5	-450.33	D642	16.69	226	8.41	8.1
24043.12	-18647.8	-451.27	D642	15.03	173.75	6.64	8.93
24043.76	-18648.6	-453.99	D642	14.67	211	7.57	9.4
24039.45	-18643.3	-435.81	D642	11.25	113	4.02	1.89
24042.67	-18647.3	-449.4	D642	10.39	306.5	11.57	14.02
24042.23	-18646.7	-447.52	D642	8.67	253.5	9.83	13.61
24042.45	-18647	-448.46	D642	7.86	337	12.7	20.4
24034.07	-18636.8	-413.14	D642	6.99	35.1	1.19	10.2
24034.21	-18637	-413.7	D642	6.99	35.1	1.19	10.2
24040.89	-18645.1	-441.9	D642	6.21	39.3	1.46	4.3
24042	-18646.4	-446.59	D642	5.62	241	9.83	5.91
24038.12	-18641.7	-430.19	D642	5.43	19.2	0.5	1.9
24038.34	-18642	-431.13	D642	4.87	9.12	0.27	1.11
24037.9	-18641.5	-429.25	D642	4.35	33.6	0.88	3.63
24041.12	-18645.4	-442.84	D642	4.16	118.08	3.99	5.83
24041.56	-18645.9	-444.71	D642	3.36	142	5.76	1.98
24041.78	-18646.2	-445.65	D642	3.33	197	7.98	2.94
24041.34	-18645.6	-443.78	D642	3.27	147.55	5.64	3.38
24038.56	-18642.3	-432.06	D642	2.78	12.9	0.44	0.69
24032.45	-18634.8	-406.3	D642	1.65	0.8	0.01	0.02
24032.67	-18635.1	-407.24	D642	1.65	0.8	0.01	0.02
24038.78	-18642.5	-433	D642	1.1	15.6	0.58	0.05
23495.15	-17790.2	-38.51	D644	21.76	269.9	3.73	5.2
23494.52	-17789.8	-39.19	D644	18.88	98.47	1.68	1.37
23484.72	-17784	-49.95	D644	10.11	36.6	0.12	0.47
23497.02	-17791.3	-36.45	D644	8.18	325.1	1.44	2.28
23496.4	-17791	-37.13	D644	7.84	212.29	0.72	0.63
23493.28	-17789.1	-40.56	D644	6.34	31.5	0.35	0.47
23484.09	-17783.6	-50.64	D644	5.86	5.1	0.05	0.15
23483.63	-17783.3	-51.15	D644	5.86	5.1	0.05	0.15
23485.97	-17784.7	-48.58	D644	5.83	3	0.06	0.52
23493.9	-17789.5	-39.88	D644	5.74	12.18	0.17	0.26
23489.53	-17786.8	-44.67	D644	5.07	7.5	0.16	0.85
23492.65	-17788.7	-41.25	D644	5.04	3.3	0.06	0.49
23495.77	-17790.6	-37.82	D644	4.99	67.36	0.91	1.36
23492.03	-17788.3	-41.93	D644	4.82	3.48	0.1	0.56
23491.4	-17788	-42.62	D644	4.29	3.9	0.18	0.73

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23480.35	-17781.3	-54.75	D644	4.15	11.1	0.15	0.16
23479.82	-17781	-55.33	D644	4.15	11.1	0.15	0.16
23506.27	-17796.9	-26.3	D644	1.82	3.6	0.18	0.14
23506.89	-17797.2	-25.62	D644	1.8	4.8	0.17	0.12
23507.52	-17797.6	-24.93	D644	1.78	6	0.16	0.09
23508.14	-17798	-24.25	D644	1.71	6.3	0.44	0.07
23481.91	-17782.3	-53.04	D644	1.68	9.6	0.16	0.4
23498.77	-17792.4	-34.53	D644	1.61	3.6	0.06	0.12
23481.28	-17781.9	-53.72	D644	1.51	3.6	0.06	0.31
23480.82	-17781.6	-54.24	D644	1.51	3.6	0.06	0.31
23505.64	-17796.5	-26.99	D644	1.37	4.2	0.02	0.21
23501.9	-17794.3	-31.1	D644	1.34	4.2	0.1	0.03
23499.4	-17792.8	-33.84	D644	1.3	2.85	0.08	0.09
23502.52	-17794.6	-30.42	D644	1.23	3.9	0.05	0.11
23497.59	-17791.7	-35.83	D644	1.23	24.3	0.15	0.11
23487.22	-17785.5	-47.21	D644	1.2	2.85	0.11	1.23
23498.15	-17792	-35.22	D644	1.17	3.3	0.07	0.09
23487.84	-17785.8	-46.52	D644	1.13	3.3	0.13	0.65
23503.14	-17795	-29.73	D644	1.04	3.9	0.04	0.13
23487.19	-17786	-34.48	D645	39.77	351	6.76	7.9
23487.66	-17786.3	-34.18	D645	36.01	369.6	6.13	7.12
23495.26	-17790.7	-29.38	D645	27.87	35.1	7.02	1.86
23489.94	-17787.6	-32.74	D645	26.78	131.5	6.13	3.36
23494.5	-17790.2	-29.86	D645	23.59	59.4	3.2	1.78
23493.74	-17789.8	-30.34	D645	23.59	59.4	3.2	1.78
23483.63	-17783.9	-36.72	D645	23.47	122.26	4.17	11.38
23484.39	-17784.4	-36.24	D645	22.49	340.25	9.8	12.36
23485.91	-17785.3	-35.28	D645	22.15	200	5.98	10.7
23485.15	-17784.8	-35.76	D645	20.09	401.6	11.44	11.1
23490.7	-17788	-32.26	D645	19.41	342	3.91	7.91
23492.98	-17789.3	-30.82	D645	17.49	68.1	2.87	7.62
23492.22	-17788.9	-31.3	D645	17.04	101.5	4.64	4.72
23496.02	-17791.1	-28.9	D645	16.35	34.2	3.77	4.5
23483.06	-17783.6	-37.08	D645	14.47	48.2	2.69	4.56
23478.81	-17781.2	-39.77	D645	10.63	363	15.2	3.82
23489.18	-17787.2	-33.22	D645	8.29	435.63	1.87	0.94
23496.78	-17791.5	-28.42	D645	7.54	38.4	1.61	3.91
23491.46	-17788.5	-31.78	D645	4.46	125.5	2.78	8.01
23482.49	-17783.3	-37.44	D645	4.35	4.6	0.33	0.28
23486.71	-17785.7	-34.78	D645	3.6	38.1	1.03	1.93
23486.31	-17785.5	-35.03	D645	3.6	38.1	1.03	1.93
23499.06	-17792.9	-26.98	D645	2.43	66	0.2	0.47
23498.3	-17792.4	-27.46	D645	2.43	66	0.2	0.47

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23504.75	-17796.1	-23.38	D645	2.26	7.8	0.59	0.14
23488.42	-17786.7	-33.7	D645	2.13	537	0.45	0.14
23503.99	-17795.7	-23.86	D645	1.92	8.4	0.57	0.14
23503.23	-17795.3	-24.34	D645	1.58	9	0.56	0.13
24098.41	-18199.3	-349.16	D646	38.88	80.4	2.19	4.01
24107.13	-18213.8	-372.46	D646	22.35	81.9	2.15	2.24
24106.87	-18213.4	-371.78	D646	14.13	78.78	2.05	1.81
24095.84	-18195	-342.29	D646	12.51	58.8	1.76	1.62
24096.45	-18196	-343.91	D646	10.94	299	8.15	13.2
24105.13	-18210.5	-367.12	D646	10.52	205.76	6.36	6.15
24105.38	-18210.9	-367.77	D646	9.81	40.8	1.16	5.05
24096.14	-18195.5	-343.1	D646	9.22	291	7.91	7.28
24106.57	-18212.9	-370.97	D646	8.69	43.32	1.37	2.29
24104.83	-18210	-366.32	D646	8.66	418	11.84	7.64
24095.54	-18194.5	-341.48	D646	7.44	220	6.3	1.02
24106.27	-18212.4	-370.16	D646	6.24	26.94	0.91	0.66
24105.97	-18211.9	-369.35	D646	5.91	37.77	1.12	0.68
24099.9	-18201.8	-353.13	D646	5.7	26.9	0.79	6.11
24094.33	-18192.5	-338.24	D646	4.73	26.1	1.01	1.8
24094.63	-18193	-339.05	D646	4.73	26.1	1.01	1.8
24094.93	-18193.5	-339.86	D646	3.94	15	0.57	1.18
24095.23	-18194	-340.67	D646	3.94	15	0.57	1.18
24098.2	-18199	-348.6	D646	3.91	18.6	0.5	1.4
24098.69	-18199.8	-349.89	D646	2.85	15.3	0.43	0.14
24093.72	-18191.5	-336.62	D646	2.5	11.7	0.51	1.64
24094.02	-18192	-337.43	D646	2.5	11.7	0.51	1.64
24093.12	-18190.5	-335.01	D646	1.71	4.8	0.21	0.19
24093.42	-18191	-335.82	D646	1.71	4.8	0.21	0.19
24090.69	-18186.5	-328.53	D646	1.68	5.4	0.19	0.12
24091	-18187	-329.34	D646	1.68	5.4	0.19	0.12
24107.69	-18214.8	-373.96	D646	1.44	2.4	0.03	0.01
24091.3	-18187.5	-330.15	D646	1.13	3.3	0.12	0.06
24091.6	-18188	-330.96	D646	1.13	3.3	0.12	0.06
24092.51	-18189.5	-333.39	D646	1.03	3.3	0.08	0.09
24092.81	-18190	-334.2	D646	1.03	3.3	0.08	0.09
23509.06	-17785.7	-38.43	D647	34.27	280.13	8.94	6.44
23508.88	-17785.2	-39.1	D647	27.02	76.5	4.57	6.3
23509.88	-17788.1	-35.33	D647	24.62	289	5.18	1.73
23509.26	-17786.3	-37.65	D647	23.47	201.38	6.29	4.36
23510.08	-17788.7	-34.55	D647	21.74	109	4.71	1.79
23509.67	-17787.5	-36.1	D647	20.09	121.5	2.23	0.31
23509.47	-17786.9	-36.88	D647	19.83	129.25	2.9	1.14
23510.75	-17790.6	-32.04	D647	10.66	45.5	3.05	1.7

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23507.88	-17782.3	-42.88	D647	5.69	12.8	0.98	0.4
23507.68	-17781.7	-43.65	D647	5.69	12.8	0.98	0.4
23508.29	-17783.5	-41.33	D647	5.55	9.2	0.59	0.55
23508.09	-17782.9	-42.11	D647	5.55	9.2	0.59	0.55
23510.95	-17791.2	-31.26	D647	5.4	18.95	1.25	0.47
23508.7	-17784.7	-39.78	D647	5.07	7.7	0.2	0.62
23508.49	-17784.1	-40.56	D647	5.07	7.7	0.2	0.62
23510.34	-17789.4	-33.58	D647	4.49	11.1	0.24	1.12
23510.21	-17789.1	-34.07	D647	4.49	11.1	0.24	1.12
23507.47	-17781.1	-44.43	D647	3.02	3	0.18	0.16
23507.28	-17780.5	-45.15	D647	3.02	3	0.18	0.16
23505.83	-17776.3	-50.63	D647	2.78	13.4	0.2	0.18
23505.63	-17775.7	-51.4	D647	2.78	13.4	0.2	0.18
23503.79	-17770.3	-58.37	D647	2.3	4.6	0.08	0.09
23503.58	-17769.7	-59.15	D647	2.3	4.6	0.08	0.09
23510.54	-17790	-32.81	D647	2.2	25.05	0.95	3.51
23506.07	-17777	-49.74	D647	1.06	2	0.11	0.11
23505.95	-17776.6	-50.18	D647	1.06	2	0.11	0.11
23508.6	-17787	-30.86	D648	30.65	54	5.09	1.04
23508.31	-17786.3	-31.51	D648	30.03	63.9	9.26	7.1
23506.03	-17780.7	-36.71	D648	28.67	158.25	4.53	7.32
23509.17	-17788.5	-29.55	D648	23.73	33.3	3.76	0.21
23508.88	-17787.7	-30.2	D648	21.43	24.3	3.09	0.01
23506.31	-17781.4	-36.06	D648	20.43	112.75	3.44	2.96
23505.74	-17780	-37.36	D648	16.28	121.7	3.17	8.82
23508.03	-17785.6	-32.16	D648	15.07	719.47	4.26	4.2
23504.89	-17777.9	-39.31	D648	10.15	245	6.38	4.3
23504.73	-17777.5	-39.67	D648	10.15	245	6.38	4.3
23507.74	-17784.9	-32.81	D648	10.08	938	2.6	3.24
23504	-17775.7	-41.33	D648	8.88	15.9	0.61	1.41
23503.72	-17775	-41.98	D648	8.88	15.9	0.61	1.41
23503.43	-17774.3	-42.63	D648	8.23	45	1.63	2.58
23503.15	-17773.6	-43.28	D648	8.23	45	1.63	2.58
23507.46	-17784.2	-33.46	D648	6.07	438.5	2	0.95
23506.6	-17782.1	-35.41	D648	5.5	60.9	0.92	2.16
23500.58	-17767.3	-49.14	D648	5.49	9.3	0.03	0.07
23500.29	-17766.6	-49.79	D648	5.49	9.3	0.03	0.07
23509.43	-17789.1	-28.97	D648	5.38	12.6	0.45	0.44
23502.86	-17772.9	-43.93	D648	4.83	23.4	1.06	1.54
23502.57	-17772.2	-44.58	D648	4.83	23.4	1.06	1.54
23507.17	-17783.5	-34.11	D648	4.36	250.83	1.63	0.2
23502.29	-17771.5	-45.23	D648	3.84	14.1	0.34	0.41
23502	-17770.8	-45.89	D648	3.84	14.1	0.34	0.41

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23505.46	-17779.3	-38.01	D648	3.15	52.35	1.31	2.57
23501.72	-17770.1	-46.54	D648	3.15	48.9	0.61	0.57
23501.43	-17769.4	-47.19	D648	3.15	48.9	0.61	0.57
23501.15	-17768.7	-47.84	D648	2.37	56.7	0.24	0.4
23500.86	-17768	-48.49	D648	2.37	56.7	0.24	0.4
23484.87	-17784.3	-24.06	D649	61.96	186.68	12.48	12.45
23467.26	-17774	-28.15	D649	60.07	12	0.6	6.59
23483.18	-17783.3	-24.45	D649	54.51	232.2	8.81	4.63
23484.03	-17783.8	-24.25	D649	50.69	419.75	18.88	10.83
23489.1	-17786.8	-23.08	D649	49.04	94.59	3.05	4.41
23470.64	-17776	-27.36	D649	47.52	153	5.57	9.03
23466.41	-17773.5	-28.34	D649	43.27	117.5	5.71	8.52
23487.41	-17785.8	-23.47	D649	42.29	160	5.39	2.02
23482.34	-17782.9	-24.65	D649	40.83	101.22	2.93	8.68
23468.1	-17774.5	-27.95	D649	39.33	219	6.33	6.34
23465.63	-17773	-28.52	D649	38.4	101	6.44	7.92
23471.48	-17776.5	-27.17	D649	35.86	236	10.9	3.47
23488.25	-17786.3	-23.27	D649	30.54	81.81	2.76	2.27
23472.33	-17777	-26.97	D649	28.32	249	10.5	4.06
23469.79	-17775.5	-27.56	D649	28.01	324	9.57	3.15
23468.95	-17775	-27.75	D649	27.36	143	4.69	13.8
23485.72	-17784.8	-23.86	D649	23.8	43.72	3.19	3.79
23489.94	-17787.3	-22.88	D649	20.36	216.3	6.91	5.39
23481.49	-17782.4	-24.84	D649	19.66	167.63	4.78	13.27
23490.79	-17787.8	-22.68	D649	19.56	282.05	8.53	10.43
23486.56	-17785.3	-23.66	D649	19.18	146.6	4.42	0.45
23473.17	-17777.4	-26.77	D649	17.69	577	17.8	6.28
23480.75	-17781.9	-25.01	D649	15.5	147	4.16	15
23491.63	-17788.3	-22.49	D649	10.09	355.88	10.65	17.59
23474.02	-17777.9	-26.58	D649	6.86	114.5	3.42	4.71
23480.01	-17781.5	-25.18	D649	3.67	60.3	2.4	1.01
23912.89	-18385	-368.51	D650	14.26	116	1.37	2.09
23915.63	-18393.3	-422.11	D650	11.38	183.5	5.81	8.03
23915.6	-18393.2	-421.5	D650	10.31	168.18	5.32	7.27
23912.93	-18385.1	-369.5	D650	10.05	81.92	0.97	1.47
23912.45	-18383.7	-359.06	D650	3.63	364	11	1.23
23912.85	-18384.9	-367.62	D650	1.47	13.2	0.07	0.14
23912.49	-18383.8	-359.8	D650	1.06	3.3	0.12	0.18
23506.92	-17792	-39.92	D651	12.69	40.5	1.85	4.79
23509.52	-17795.3	-31.98	D651	7.65	131	1.72	1.49
23502.59	-17786.4	-53.17	D651	5.83	17.1	0.5	0.8
23501.72	-17785.3	-55.82	D651	4.97	6.3	0.06	0.19
23499.98	-17783.1	-61.11	D651	4.36	4.8	0.04	0.14

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23502.88	-17786.8	-52.28	D651	4.32	5.4	0.07	0.31
23505.77	-17790.5	-43.46	D651	3.77	5.1	0.33	0.07
23499.7	-17782.7	-62	D651	3.57	4.5	0.04	0.23
23504.46	-17788.8	-47.43	D651	3.26	3.3	0.06	0.38
23505.48	-17790.1	-44.34	D651	2.98	12.9	0.11	0.8
23505.26	-17789.8	-45	D651	2.98	12.9	0.11	0.8
23506.05	-17790.8	-42.57	D651	2.91	3.3	0.05	0.04
23500.27	-17783.4	-60.23	D651	2.85	3.9	0.03	0.05
23502.01	-17785.7	-54.93	D651	2.74	2.7	0.04	0.2
23502.3	-17786	-54.05	D651	2.43	4.2	0.07	0.72
23509.23	-17794.9	-32.86	D651	2.37	3	0.15	0.33
23507.21	-17792.3	-39.04	D651	2.19	6.9	0.08	0.26
23507.5	-17792.7	-38.16	D651	1.92	23.4	0.23	0.28
23506.63	-17791.6	-40.81	D651	1.92	2.1	0.08	0.21
23506.34	-17791.2	-41.69	D651	1.92	2.1	0.08	0.21
23499.41	-17782.3	-62.88	D651	1.92	2.4	0.03	0.05
23504.18	-17788.4	-48.31	D651	1.82	1.8	0.05	0.31
23508.95	-17794.5	-33.74	D651	1.68	50.4	2.09	1.19
23508.37	-17793.8	-35.51	D651	1.44	3.9	0.15	0.29
23507.79	-17793.1	-37.27	D651	1.42	21.75	0.25	0.25
23508.08	-17793.4	-36.39	D651	1.32	3.75	0.13	0.25
23503.09	-17787.1	-51.62	D651	1.13	3	0.16	0.17
23501.43	-17784.9	-56.7	D651	1.1	3	0.04	0.08
23503.31	-17787.3	-50.96	D651	1.03	2.4	0.1	0.15
24066.85	-18685.6	-465.42	D652	30.04	11.93	0.37	1.12
24066.68	-18685.3	-464.78	D652	25.72	22.08	0.88	0.88
24065.47	-18683.2	-460.43	D652	15.29	83.4	3.15	7.15
24066.44	-18684.9	-463.91	D652	14.96	25.17	0.98	3.08
24066.19	-18684.5	-463.04	D652	14.09	71.98	2.57	10.34
24065.95	-18684	-462.17	D652	12.48	144.51	5.47	8.49
24073.77	-18698	-490.56	D652	11.86	86	3.27	11.47
24054.33	-18664.3	-421.03	D652	11.66	13.9	0.43	6.28
24054.58	-18664.7	-421.9	D652	10.97	72.2	2.55	8.72
24064.25	-18681.1	-456.06	D652	10.1	36.54	1.17	4.47
24064.01	-18680.6	-455.19	D652	9.6	60.54	2.06	4.15
24065.22	-18682.8	-459.55	D652	9.53	90	3.58	7.6
24074	-18698.5	-491.44	D652	8.88	281.5	10.19	8.06
24073.53	-18697.6	-489.69	D652	8.85	151.75	5.74	12.27
24064.98	-18682.3	-458.68	D652	8.81	95.15	3.78	7.3
24063.76	-18680.2	-454.32	D652	8.21	61.23	2.03	2.34
24072.82	-18696.3	-487.08	D652	7.82	76.2	2.9	4.88
24057.06	-18668.8	-430.56	D652	7.34	20.7	0.56	16
24065.71	-18683.6	-461.3	D652	7.17	49.38	1.95	4.73

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24073.05	-18696.7	-487.95	D652	6.99	70.05	2.57	10.91
24057.31	-18669.2	-431.44	D652	6.93	337	8.31	5.4
24072.58	-18695.9	-486.21	D652	6.74	54.6	2	8.66
24073.29	-18697.2	-488.82	D652	6.3	114.35	4.24	13.61
24072.34	-18695.4	-485.34	D652	6.21	82.35	3.09	11.2
24072.1	-18695	-484.47	D652	5.95	174	6.69	10.31
24063.03	-18679	-451.7	D652	5.75	27.42	0.99	4.59
24062.54	-18678.1	-449.96	D652	5.66	122.5	4.65	0.53
24071.86	-18694.6	-483.6	D652	5.66	346	13.85	7.93
24062.3	-18677.7	-449.08	D652	5.42	296	10.4	6.91
24062.79	-18678.5	-450.83	D652	5.4	81.06	3.07	0.36
24057.8	-18670.1	-433.19	D652	5.14	220.22	4.38	6.33
24071.62	-18694.2	-482.72	D652	5.14	452	18.5	6.13
24063.27	-18679.4	-452.57	D652	4.64	43.32	1.65	7.29
24058.52	-18671.3	-435.72	D652	4.35	390	13.5	11.8
24064.49	-18681.5	-456.94	D652	4.32	10.14	0.27	0.93
24074.22	-18698.8	-492.22	D652	4.25	506	18.2	8.37
24058.3	-18670.9	-434.93	D652	4.11	86.4	2.95	11.16
24064.74	-18681.9	-457.81	D652	2.44	128.1	5	4.23
24058.05	-18670.5	-434.06	D652	2.15	44.58	1.57	6.67
24076.33	-18702.6	-499.98	D652	1.81	16.98	0.75	2.87
24053.25	-18662.5	-417.26	D652	1.01	46.3	1.29	7.45
23572.9	-18255.1	-125.56	D653	31.13	92.9	2.55	4.11
23542.53	-18223.4	-129.33	D653	24.99	103.6	5.26	5.48
23572.24	-18254.4	-125.65	D653	22.7	224	8.09	10.7
23551.72	-18232	-128.36	D653	22.29	33	0.96	1.09
23541.78	-18222.8	-129.4	D653	21.4	88.55	4.34	6.89
23552.42	-18232.7	-128.28	D653	20.37	116	3.53	3.62
23579.43	-18262.5	-124.6	D653	17.28	157.5	5.06	1.01
23553.82	-18234.1	-128.11	D653	15.81	55.3	2.69	9.62
23578.82	-18261.9	-124.69	D653	13.75	772.47	26.26	6.07
23541.02	-18222.1	-129.48	D653	12.96	77.1	2.99	7
23553.12	-18233.4	-128.19	D653	12.96	97.3	3.11	6.61
23540.26	-18221.5	-129.55	D653	11.79	72.3	2.1	5.54
23578.17	-18261.1	-124.79	D653	11.68	303	10.1	8.34
23571.57	-18253.7	-125.75	D653	10.7	230	7.84	8.1
23551.01	-18231.3	-128.44	D653	9.74	71.3	2.19	2.57
23557.25	-18237.7	-127.69	D653	9.57	388	12.1	5.52
23577.51	-18260.4	-124.88	D653	9.29	291.1	9.37	8.39
23555.89	-18236.2	-127.86	D653	9.19	937	29.9	3.25
23539.5	-18220.9	-129.62	D653	8.53	77	2.48	4.06
23576.85	-18259.6	-124.98	D653	8.5	139.13	4.54	8.51
23557.92	-18238.4	-127.61	D653	8.06	98.8	3.18	11.1

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23574.87	-18257.4	-125.27	D653	7.99	68.9	4.24	3.13
23573.56	-18255.9	-125.46	D653	6.75	67.5	2.07	6.92
23543.28	-18224.1	-129.26	D653	5.62	118	3.58	0.26
23543.84	-18224.6	-129.2	D653	5.62	118	3.58	0.26
23538.73	-18220.2	-129.69	D653	5.28	81.7	2.87	2.58
23574.22	-18256.6	-125.37	D653	4.56	58.1	2.21	5.52
23556.57	-18236.9	-127.78	D653	3.6	215	6.44	8.34
23576.19	-18258.9	-125.08	D653	3.39	106.53	4.58	4.09
23554.51	-18234.8	-128.03	D653	2.98	23.3	1.3	0.85
23570.91	-18252.9	-125.84	D653	2.26	43.3	3.76	5.31
23555.2	-18235.5	-127.95	D653	1.78	17.8	0.9	1.21
23537.96	-18219.6	-129.76	D653	1.37	8.6	0.21	0.48
23558.6	-18239.1	-127.52	D653	1.17	5.9	0.21	0.08
23561.57	-18237.8	-125.88	D655	31.95	183.5	6.69	5.06
23562.41	-18238.3	-125.73	D655	29.45	118	4.28	3.05
23560.73	-18237.3	-126.03	D655	28.93	176.25	6.2	3.62
23563.25	-18238.8	-125.58	D655	26.25	91.4	3.21	1.75
23559.9	-18236.7	-126.17	D655	25.92	169	5.7	2.17
23540.62	-18223	-129.35	D655	24.07	59.1	2.23	1.51
23541.35	-18223.7	-129.23	D655	23.21	38.7	1.65	1.03
23564.09	-18239.4	-125.43	D655	23.04	64.8	2.14	0.45
23542.09	-18224.4	-129.12	D655	22.35	18.3	1.07	0.55
23542.55	-18224.8	-129.04	D655	22.35	18.3	1.07	0.55
23570.79	-18243.6	-124.2	D655	15.63	203.75	5.53	0.6
23564.93	-18239.9	-125.28	D655	15.15	111.5	3.68	1.89
23565.76	-18240.4	-125.13	D655	15.15	111.5	3.68	1.89
23559.06	-18236.2	-126.32	D655	11.97	318	12	13.2
23573.11	-18245	-123.75	D655	11.93	42	1.36	0.36
23571.63	-18244.1	-124.04	D655	11.26	119.1	3.37	0.45
23569.95	-18243	-124.35	D655	10.83	99.2	3.49	0.47
23557.38	-18235.2	-126.61	D655	10.77	297	9.35	12.2
23554.86	-18233.6	-127.04	D655	10.01	676	22.8	10.3
23558.22	-18235.7	-126.46	D655	9.98	229	9.38	17.2
23572.46	-18244.6	-123.88	D655	9.89	30.6	1.63	0.41
23538.47	-18221	-129.68	D655	9.25	54.6	1.39	3.88
23539.18	-18221.7	-129.57	D655	6.91	43.2	1.1	3.08
23537.77	-18220.3	-129.79	D655	5.83	7.8	0.34	0.59
23569.12	-18242.5	-124.51	D655	3.53	22.35	0.85	3.9
23539.89	-18222.4	-129.46	D655	3.43	16.2	0.46	1.19
23568.28	-18242	-124.66	D655	1.17	19.41	0.52	4.26
23550.89	-18231.1	-127.7	D655	1.1	44.7	1.6	0.83
23545.23	-18212.7	-127.29	D657	11.45	264	7.92	14.2
23545.85	-18212.3	-127.1	D657	11.45	264	7.92	14.2

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23538.68	-18216.9	-129.25	D657	7.22	57.35	1.67	3.13
23551.34	-18209	-122.94	D658	29.66	277	9.32	4.05
23549.76	-18210	-123.66	D658	20.33	224	7.94	8.3
23542.63	-18214.4	-126.9	D658	20.23	451	15.2	4.23
23541.84	-18214.9	-127.26	D658	20.09	152	4.5	6.58
23556.88	-18205.6	-120.43	D658	19.27	8.85	0.24	0.09
23556.09	-18206	-120.79	D658	15.26	4.8	0.06	0.24
23550.55	-18209.5	-123.3	D658	14.4	314	10.7	1.85
23557.67	-18205.1	-120.08	D658	13.51	15.15	0.48	0.17
23543.42	-18214	-126.54	D658	12	679	20.7	8.57
23538.67	-18216.9	-128.71	D658	11.21	144.75	4.14	9.76
23544.21	-18213.5	-126.18	D658	10.25	612	18.1	14.9
23555.3	-18206.5	-121.15	D658	9.88	8.4	0.16	0.51
23559.26	-18204.1	-119.36	D658	9.12	11.7	0.24	0.31
23554.51	-18207	-121.51	D658	8.6	19.5	0.63	1.39
23545.8	-18212.5	-125.45	D658	8.57	321	10.4	10.9
23553.72	-18207.5	-121.87	D658	8.47	43.8	1.78	3.8
23539.46	-18216.4	-128.35	D658	8.23	180	5.04	8.22
23558.47	-18204.6	-119.72	D658	7.89	16.8	0.54	0.21
23548.17	-18211	-124.38	D658	7.44	51.6	1.69	5.83
23552.13	-18208.5	-122.58	D658	7.41	158.5	5.27	2.95
23548.97	-18210.5	-124.02	D658	7.27	262	11.4	17.6
23552.92	-18208	-122.23	D658	6.14	152	5.06	7.88
23546.59	-18212	-125.09	D658	5.93	134.5	3.78	14.8
23547.38	-18211.5	-124.74	D658	4.9	147	5.24	5.22
23545.01	-18213	-125.81	D658	4.39	303	10.1	9.93
23553.74	-18179.9	-129.23	D659	33.33	380	10.6	8.91
23554.11	-18179	-129.22	D659	27.82	316.25	8.91	8.43
23567.37	-18147.5	-128.21	D659	24.48	207	6	9.01
23566.97	-18148.4	-128.25	D659	14.33	14.7	0.66	1.38
23554.49	-18178	-129.2	D659	12.53	182.95	5.47	9.23
23561.79	-18160.5	-128.74	D659	10.73	313.6	10.41	9.66
23561.4	-18161.4	-128.77	D659	10.62	270.3	8.63	9.49
23561.01	-18162.4	-128.8	D659	8.56	250.2	7.62	9.64
23562.18	-18159.6	-128.71	D659	8.32	249.5	7.74	8.59
23562.51	-18158.8	-128.68	D659	7.75	211	6.34	7.36
23567.76	-18146.5	-128.17	D659	6.96	278	9.21	19
23554.87	-18177.1	-129.18	D659	6.64	211.95	6.66	12.36
23560.24	-18164.2	-128.86	D659	6.58	267.1	7.61	19.58
23568.16	-18145.6	-128.12	D659	6.45	258	8.51	8.24
23559.85	-18165.1	-128.89	D659	5.48	418.1	11.94	19.38
23555.25	-18176.2	-129.17	D659	5.31	179.9	6.36	11.19
23557.93	-18169.7	-129.02	D659	4.38	275.1	8.17	12.82

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23556.78	-18172.5	-129.09	D659	4.23	126.18	4.2	14.89
23559.46	-18166	-128.92	D659	3.56	225.3	6.42	10.76
23555.63	-18175.3	-129.15	D659	3.42	161.35	5.62	16.31
23557.54	-18170.7	-129.04	D659	3.25	331.6	10.21	14.82
23556.39	-18173.4	-129.11	D659	3.06	332.15	10.42	15.04
23563.23	-18157.1	-128.61	D659	3.05	188	5.15	2.5
23557.16	-18171.6	-129.07	D659	3.04	136.47	3.8	19.12
23556.01	-18174.3	-129.13	D659	2.92	264.2	7.94	17.14
23558.69	-18167.9	-128.97	D659	2.84	150.2	4.3	6.88
23559.08	-18167	-128.95	D659	2.74	136.4	4.84	5.55
23564.53	-18154.1	-128.49	D659	2.26	200	4.89	6.79
23564.76	-18153.5	-128.47	D659	2.26	200	4.89	6.79
23560.62	-18163.3	-128.83	D659	2.09	279	8.13	10.9
23566.18	-18150.2	-128.33	D659	1.99	11.4	0.37	2.41
23558.31	-18168.8	-129	D659	1.92	143.6	3.86	4.18
23565.39	-18152.1	-128.41	D659	1.17	7.2	0.11	1.26
23568.96	-18143.8	-128.04	D659	1.1	41.7	1.03	0.29
23556.15	-18180.4	-126.41	D660	25.37	56.4	2.44	5.32
23555.27	-18182.2	-126.55	D660	14.61	341	11.7	9.56
23549.46	-18193.9	-127.49	D660	14.4	81.3	2.77	7.18
23555.71	-18181.3	-126.48	D660	14.26	170.5	5.71	13.9
23550.73	-18191.4	-127.28	D660	13.92	215	6.74	7.54
23550.36	-18192.1	-127.34	D660	13.05	190.63	5.95	6.73
23556.59	-18179.5	-126.34	D660	11.38	266	9.85	12.4
23549.91	-18193	-127.42	D660	9.07	56.82	1.65	2.89
23557.02	-18178.6	-126.27	D660	6.31	401	13.3	21.6
23557.46	-18177.7	-126.2	D660	3.77	349	10.3	14.7
23551.55	-18189.8	-127.15	D660	3.5	23.4	0.79	1.65
23973.84	-18316.3	-379.07	D662	18.55	229	9.39	7.92
23973.49	-18316.5	-378.16	D662	15.5	313	12.1	8.73
23973.14	-18316.7	-377.24	D662	4.9	269	10.8	13.7
23974.83	-18315.8	-381.63	D662	4.35	101	3.25	23.8
23972.43	-18317.1	-375.41	D662	3.39	284	10.7	15.9
23972.78	-18316.9	-376.33	D662	3.29	187.5	7.65	13.3
23972.08	-18317.3	-374.5	D662	2.35	349.32	9.32	8.13
23975.11	-18315.6	-382.36	D662	2.06	109.5	2.76	0.64
23974.55	-18315.9	-380.9	D662	1.92	304	11.3	27.2
23974.19	-18316.1	-379.98	D662	1.37	114.5	4.33	26.1
23576.01	-18262.9	-120.17	D663	33.94	41.7	1.36	3.89
23576.86	-18263.4	-120	D663	29.9	119	4.01	7.3
23575.15	-18262.4	-120.33	D663	24.48	18.3	0.89	6.47
23574.29	-18261.9	-120.49	D663	23.79	24.6	0.84	4.41
23577.72	-18263.9	-119.84	D663	22.08	232	7.61	4.47

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23570.02	-18259.5	-121.32	D663	17.71	92.85	2.83	7.31
23561.12	-18254.4	-123.03	D663	13.71	469	17	1.57
23560.26	-18253.9	-123.19	D663	13.2	478	17	2.6
23573.44	-18261.4	-120.66	D663	11.04	81.9	3.01	18
23561.97	-18254.9	-122.86	D663	10.46	78.9	1.98	13.8
23571.73	-18260.5	-120.99	D663	7.58	163.5	6.18	10.5
23567.96	-18258.3	-121.71	D663	6.99	8.4	0.78	0.21
23568.56	-18258.6	-121.6	D663	6.99	8.4	0.78	0.21
23562.83	-18255.4	-122.7	D663	5.86	182.5	6.92	0.42
23572.58	-18260.9	-120.82	D663	4.87	292	11.6	17.6
23554.61	-18250.6	-124.28	D663	4.08	30.3	1.66	2.96
23553.76	-18250.1	-124.44	D663	3.53	34.32	1.68	2.64
23570.87	-18260	-121.15	D663	1.98	33.9	1.29	2.83
23567.11	-18257.8	-121.88	D663	1.78	7.32	0.28	0.4
23565.4	-18256.8	-122.2	D663	1.34	10.8	0.3	2.1
23552.9	-18249.7	-124.6	D663	1.07	40.36	1.4	1.08
23497.42	-18022.5	-78.03	D666	14.74	184.5	5.06	5.2
23496.57	-18022.5	-78.22	D666	11.43	270.38	7.27	6.5
23491.7	-18022.3	-79.32	D666	9.81	27	0.27	1.11
23492.67	-18022.3	-79.1	D666	9.81	27	0.27	1.11
23495.59	-18022.4	-78.44	D666	4.74	111.43	2.32	2.43
23494.62	-18022.4	-78.66	D666	2.88	48.9	0.42	0.93
23490.76	-18036.6	-79.05	D667	4.18	8.7	0.22	0.19
23491.58	-18037.1	-78.85	D667	2.91	7.5	0.23	0.27
23492.4	-18037.7	-78.64	D667	2.88	15.9	0.21	0.68
23493.22	-18038.2	-78.44	D667	2.88	15.9	0.21	0.68
23489.94	-18036.1	-79.25	D667	2.78	22.62	0.6	0.85
23489.12	-18035.5	-79.46	D667	1.39	52.98	1.08	0.55
23944.23	-18335.8	-376.9	D668	3.6	472.8	17.29	3.93
23944.64	-18335.6	-378.84	D668	2.47	848	31.6	10.1
23944.84	-18335.5	-379.82	D668	1.34	801	30.4	15.6
24081.69	-18652.9	-469.75	D669	24.75	36	2.27	3.27
24081.99	-18653.2	-470.66	D669	18	102.5	3.76	9.87
24080.22	-18651.6	-465.23	D669	15.6	38.7	1.6	2.1
24079.94	-18651.3	-464.36	D669	9.31	168.12	6.19	7.87
24080.8	-18652.1	-467.01	D669	7.41	229	6.89	5.63
24079.64	-18651	-463.44	D669	7.1	49.84	1.86	10.12
24071.98	-18644.2	-440.33	D669	7.06	132.5	3.23	4.35
24072.23	-18644.4	-441.06	D669	7.06	132.5	3.23	4.35
24071.06	-18643.4	-437.59	D669	6.93	164.5	5.64	10.4
24079.34	-18650.8	-462.53	D669	6.46	21.87	0.73	8.67
24076.94	-18648.6	-455.22	D669	5.31	15.3	0.55	5.97
24078.45	-18649.9	-459.79	D669	4.97	27.9	1.07	8.52

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24071.68	-18643.9	-439.42	D669	4.46	9	0.22	7.77
24081.39	-18652.7	-468.83	D669	4.08	11.4	0.41	0.84
24068.34	-18641	-429.55	D669	3.64	29.1	0.96	3.27
24078.15	-18649.6	-458.88	D669	3.39	31.68	1.18	4.89
24077.25	-18648.8	-456.14	D669	3.29	78	2.83	1.68
24079.04	-18650.5	-461.62	D669	2.31	94.29	3.59	21.91
24068.95	-18641.6	-431.38	D669	1.89	6.3	0.22	0.58
24071.37	-18643.6	-438.5	D669	1.65	7.8	0.12	25.9
24065.85	-18638.9	-422.24	D669	1.34	200	7.77	19.2
24081.1	-18652.4	-467.92	D669	1.17	30	1.05	1.69
24067.1	-18640	-425.9	D669	1.16	139.95	3.98	5.01
23486.62	-18048.9	-85.07	D670	7.44	38.7	1.31	1.48
23483.17	-18044	-85.07	D670	3.7	20.1	0.13	0.6
23483.75	-18044.9	-85.07	D670	2.85	16.2	0.23	0.51
23482.6	-18043.2	-85.07	D670	2.06	11.4	0.1	0.38
23484.32	-18045.7	-85.07	D670	1.99	12.3	0.33	0.43
23488.24	-18051.8	-73.63	D671	21.67	186.5	5.04	7.16
24032.22	-18574.4	-461.03	D676	12.79	240	9.64	5.24
24032.13	-18574.4	-460.49	D676	12.73	236.9	9.49	5.3
24031.78	-18574.4	-458.52	D676	12.33	70.17	2.59	1.12
24031.96	-18574.4	-459.5	D676	12.19	194.79	7.6	5.36
24021.73	-18574.5	-401.5	D676	10.35	66.3	2.37	4.56
24031.61	-18574.4	-457.53	D676	9.06	102.14	3.81	7.54
24021.9	-18574.5	-402.48	D676	7.95	16.2	0.46	4.47
24021.56	-18574.5	-400.51	D676	7.13	185	6.7	5.26
24028.73	-18574.4	-441.18	D676	5.83	139.5	5.43	9.21
24028.89	-18574.4	-442.12	D676	5.62	127	4.71	15.2
24022.08	-18574.5	-403.47	D676	5.31	107.5	3.94	3.41
24022.25	-18574.4	-404.45	D676	5.21	18.6	0.63	10.3
24031.43	-18574.4	-456.55	D676	4.89	112.98	3.61	16.66
24022.42	-18574.4	-405.44	D676	4.87	197.5	7.31	17.4
24031.26	-18574.4	-455.56	D676	4.57	208.48	8.27	2.99
24022.6	-18574.4	-406.42	D676	1.92	265	9.17	6.85
24029.32	-18574.4	-444.53	D676	1.89	203	7.78	20.7
24028.5	-18574.4	-439.9	D676	1.23	6	0.2	1.69
24028.61	-18574.4	-440.54	D676	1.23	6	0.2	1.69
23849.55	-18526.9	-314.34	D677	9.33	43.44	2.16	2.73
23849.96	-18527.1	-313.44	D677	9.01	45.24	2.03	4.18
23850.76	-18527.4	-311.64	D677	7.2	43.54	1.52	12.04
23851.17	-18527.6	-310.75	D677	6.84	59	2.04	11.89
23850.36	-18527.2	-312.54	D677	6.83	37.88	1.39	7.01
23849.31	-18526.8	-314.88	D677	6.45	15	0.65	0.86
23846.64	-18525.7	-320.81	D677	4.66	5.8	0.1	0.11

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23851.57	-18527.7	-309.85	D677	2.58	30.2	1.05	4.25
23851.98	-18527.9	-308.95	D677	1.55	35.11	1.18	3.31
23845.42	-18525.2	-323.51	D677	1.18	5.4	0.1	0.03
23852.74	-18528.2	-307.24	D677	1.17	10	0.61	0.81
23852.38	-18528.1	-308.05	D677	1.03	75	2.64	4.87
24043.13	-18096.2	-304.41	D678	32.53	15.09	0.36	1.66
24042.58	-18096.2	-304.83	D678	22.29	5.1	0.07	1.71
24044.72	-18096.4	-303.2	D678	14.47	118.5	3.66	4.58
24043.92	-18096.3	-303.81	D678	13.71	231	7.36	15
24035.34	-18095.3	-310.45	D678	8.02	42.9	1.16	7.58
24034.66	-18095.2	-310.99	D678	8.02	42.9	1.16	7.58
24030.26	-18094.7	-314.45	D678	5.14	155	6.25	7.02
23946.74	-18665.4	-328.71	D681	23.42	164	6.44	1.26
23946.7	-18665.3	-329.41	D681	23.42	164	6.44	1.26
23946.01	-18665.1	-339.68	D681	4.29	22.4	0.76	2.66
23946.08	-18665.2	-338.68	D681	3.77	145	3.51	1.96
23945.95	-18665.1	-340.48	D681	3.09	45.8	1.7	0.05
23947.31	-18665.6	-319.73	D681	1.44	5.12	0	0
24072.74	-18572.3	-416.78	D683	7.13	172	6.43	15.6
24080.6	-18572.6	-437.86	D683	3.39	376.05	14.93	23.6
24073.09	-18572.3	-417.71	D683	3.02	389	14.6	16.1
24073.36	-18572.3	-418.42	D683	3.02	389	14.6	16.1
24069	-18572.2	-407.02	D683	2.67	431	14.9	11.3
24069.35	-18572.3	-407.93	D683	2.43	567	19.9	23.6
24080.95	-18572.6	-438.8	D683	1.1	171.53	6.77	6.66
24029.74	-18013.1	-302.54	D684	1.47	0.2	0.02	0.03
24030.4	-18013.8	-302.14	D684	1.12	0.23	0.02	0.03
23911.81	-17902.1	-202.08	D685	15.67	55	1.24	0.41
23911.74	-17902.6	-201.25	D685	11.11	196.93	4.25	17.67
23912.15	-17899.5	-206	D685	5.42	3	0.05	0.04
23912.23	-17898.9	-206.83	D685	4.34	2.44	0.04	0.03
23945.08	-18709.7	-283.65	D688	18.56	142.95	5.74	8
23945.15	-18709.2	-282.75	D688	18.27	101.82	4.05	2.09
23945.65	-18706.1	-276.52	D688	10.73	264	9.73	13.2
23945.36	-18707.9	-280.08	D688	10.48	357.7	14.55	5.76
23946.14	-18703	-270.28	D688	10.15	337	13.5	14.9
23945.01	-18710.1	-284.54	D688	9.76	189.8	7.34	10.78
23945.72	-18705.6	-275.63	D688	8.21	350.1	14.47	14.32
23945.51	-18707	-278.3	D688	7.41	301	11	21
23944.94	-18710.6	-285.43	D688	5.86	287	11.07	14.3
23944.88	-18710.9	-286.14	D688	4.42	349	13.6	17.7
23945.43	-18707.4	-279.19	D688	2.24	75.78	2.81	4.35
23945.29	-18708.3	-280.97	D688	1.57	282.45	11.74	7.8

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23989.56	-18653.7	-370.25	D690	9.12	5.2	0.22	0.74
23989.61	-18652.4	-367.53	D690	7.61	248	4.89	3.2
23989.62	-18652	-366.62	D690	7.27	5.5	0.16	2.85
23989.55	-18654.1	-371.16	D690	6.89	8.4	0.34	0.43
23989.53	-18654.5	-372.06	D690	3.36	32.5	0	0
23989.52	-18654.8	-372.67	D690	3.36	32.5	0	0
23989.31	-18661	-385.97	D690	2.07	30.9	0.4	0.54
23989.29	-18661.4	-386.88	D690	1.96	26.83	0.34	0.47
23913.58	-18663.9	-276.8	D693	19.57	55.2	2.28	1.78
23914.89	-18664.1	-274.11	D693	17.62	37.3	0.93	0.07
23915.33	-18664.1	-273.21	D693	12.55	85.9	1.8	0.33
23913.15	-18663.9	-277.7	D693	12.1	25	1.01	0.26
23915.76	-18664.2	-272.31	D693	10.01	51.1	1.59	0.09
23911.05	-18663.6	-282.04	D693	9.87	81	2.91	5.47
23912.71	-18663.8	-278.6	D693	8.7	42.07	1.16	1.39
23914.45	-18664	-275	D693	8.5	25	0.57	1.48
23911.4	-18663.6	-281.29	D693	7.08	27.24	0.86	13.33
23914.02	-18664	-275.9	D693	6.24	11.1	0.47	1.62
23912.28	-18663.8	-279.5	D693	2.91	15.77	0.47	0.48
23911.84	-18663.7	-280.4	D693	1.72	5.56	0.2	3.08
23987.44	-18652.5	-371.52	D697	10.32	6.3	0.2	1.15
23987.45	-18652.1	-370.62	D697	8.71	14	0.39	1.29
23987.15	-18660.2	-388.35	D697	8.02	180	5	3.28
23987.4	-18653.8	-374.25	D697	6.99	7.6	0.21	1.32
23987.39	-18654.2	-375.16	D697	6.99	7.6	0.21	1.32
23987.43	-18653	-372.43	D697	6.67	12.2	0.5	0.73
23987.46	-18651.7	-369.71	D697	6.32	9.84	0.26	1.77
23987.47	-18651.3	-368.8	D697	5.04	7.6	0.19	2.03
23987.42	-18653.4	-373.34	D697	3.02	18.1	0.79	0.31
23985.42	-18685.4	-444.96	D697	1.37	401	18.7	14.5
23987.17	-18659.8	-387.43	D697	1.34	16.4	0.7	0.4
23987.34	-18655.7	-378.34	D697	1.17	9.4	0.2	0.55
23987.33	-18656.1	-379.25	D697	1.17	9.4	0.2	0.55
23985.39	-18685.8	-445.87	D697	1.02	410.35	17.64	15.52
23866.23	-18658.2	-213.23	D699	7.68	223	7.19	7.92
23865.24	-18658.1	-213.32	D699	7.56	180.5	7.03	13.51
23864.6	-18658	-213.38	D699	7.54	173	7	14.5
23883.65	-18633.4	-269.55	D702	26.99	10.06	0.24	0.02
23882.99	-18633.1	-270.21	D702	25.54	8.74	0.22	0.06
23884.31	-18633.7	-268.89	D702	15.52	4.01	0.04	0.02
23882.32	-18632.7	-270.88	D702	15.08	42.16	1.53	5.43
23879	-18631	-274.2	D702	13.42	85.12	2.65	7.82
23880.33	-18631.7	-272.87	D702	12.37	9.52	0.29	6.05

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23881.66	-18632.4	-271.54	D702	11.63	52.2	1.96	2.38
23881	-18632	-272.21	D702	10.78	20.42	0.71	0.45
23879.67	-18631.3	-273.53	D702	8.77	6.82	0.22	5.5
23888.96	-18636.2	-264.24	D702	8.23	26.5	0.87	1.34
23878.34	-18630.7	-274.86	D702	7.45	91.52	3.15	10.3
23888.3	-18635.8	-264.9	D702	2.69	8.09	0.27	0.4
23893.94	-18638.7	-259.26	D702	2.23	0.8	0.01	0
23893.28	-18638.4	-259.92	D702	2.01	0.74	0.01	0
23882.43	-18679.9	-215.23	D704	3.83	327.03	13.33	15.49
23881.45	-18680.1	-215.39	D704	1.3	109.53	4.48	5.22
23922.55	-17924.8	-213.34	D707	12	218	4.93	6.54
23921.98	-17924.9	-211.22	D707	4.69	101.3	1.77	11.38
23923.88	-17924.6	-218.26	D707	3.91	3	0.01	0.04
23924.14	-17924.6	-219.23	D707	3.73	2.86	0.01	0.04
23924.66	-17924.5	-221.16	D707	1.91	0.28	0	0.02
23924.92	-17924.4	-222.12	D707	1.72	0.27	0	0.02
23922.24	-17924.8	-212.18	D707	1.54	4.5	0.23	1.06
23922.4	-17924.8	-212.76	D707	1.54	4.5	0.23	1.06
23973.67	-18737.8	-275.64	D709	6.15	280.4	10.17	11.06
23973.8	-18738.2	-276.06	D709	4.73	294	9.24	9.7
23976.24	-18746.2	-284.12	D709	3.68	279.02	10.8	16.02
23973.46	-18737.1	-274.95	D709	2.51	217.8	8.11	11.32
23946.21	-18601.4	-358.41	D710	16.63	37.8	1.67	2.16
23945.98	-18601.5	-359.37	D710	11.14	17.1	0.65	3.85
23945.74	-18601.6	-360.33	D710	10.22	10.2	0.43	7.05
23945.51	-18601.8	-361.29	D710	9.7	9.3	0.36	1.65
23945.28	-18601.9	-362.26	D710	9.12	6.6	0.28	0.2
23944.81	-18602.2	-364.18	D710	7.03	14.7	0.58	5.28
23943.17	-18603.2	-370.91	D710	6.86	11.7	0.42	0.14
23944.58	-18602.3	-365.14	D710	6.31	17.4	0.72	6.48
23944.11	-18602.6	-367.06	D710	5.86	119	1.33	1.27
23943.64	-18602.9	-368.99	D710	5.55	39.6	1.96	1.1
23944.35	-18602.5	-366.1	D710	4.87	154	3.57	1.08
23943.41	-18603.1	-369.95	D710	4.8	19.8	0.84	0.36
23945.05	-18602.1	-363.22	D710	4.39	3.6	0.11	0.54
23943.88	-18602.8	-368.03	D710	3.63	29.4	1.19	3.72
23935.3	-18607.8	-403.87	D710	3.36	350	13.8	5.87
23935.12	-18607.9	-404.64	D710	3.36	350	13.8	5.87
23946.35	-18601.3	-357.83	D710	2.19	5.7	0.23	0.17
23936.92	-18606.9	-396.91	D710	1.92	260.12	4.9	2.06
23946.49	-18601.2	-357.25	D710	1.81	4.62	0.19	0.15
24011.94	-18697.6	-354.66	D712	11.11	60	2.4	1.38
24011.59	-18697.4	-353.74	D712	6.76	65.7	2.71	0.84

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24012.98	-18698.2	-357.41	D712	4.15	87.6	3.19	1.62
24011.25	-18697.2	-352.83	D712	2.4	71.4	3.02	0.3
24013.32	-18698.4	-358.33	D712	1.85	45.6	0.71	0.2
24013.67	-18698.6	-359.25	D712	1.1	22.9	0.37	0.12
23996.98	-18177.6	-293.35	D713	18.42	337.5	10.33	20.67
23997.01	-18177.6	-292.36	D713	10.59	264	8.06	18.5
23996.94	-18177.6	-294.35	D713	10.06	380.2	10.95	23.49
23996.88	-18177.6	-296	D713	7.78	193	5.83	12.6
23996.91	-18177.6	-295.35	D713	7.09	241	7.07	15.52
23925.37	-18172.8	-292.75	D714	49.88	79.11	2.69	2.1
23926.21	-18172.9	-292.22	D714	49.17	93.7	3.07	5.62
23927.05	-18173	-291.69	D714	29.32	718.63	20.27	13.85
23924.53	-18172.8	-293.29	D714	26.38	166.88	5.72	4.43
23923.69	-18172.7	-293.82	D714	10.18	429	15.1	11.1
23922.85	-18172.6	-294.36	D714	8.7	562.5	18.3	14.3
23922.03	-18172.5	-294.88	D714	7.23	696	21.5	17.5
23927.58	-18173	-291.35	D714	2.98	1.5	0.06	0.02
23928.11	-18173.1	-291.02	D714	2.24	1.35	0.05	0.01
24005.11	-18546.3	-467.69	D715	54.99	244	9.75	9.12
24004.57	-18547.1	-459.85	D715	51.29	287	9.74	9.88
24005.04	-18546.4	-466.7	D715	32.95	174.5	6.72	4.51
24004.51	-18547.2	-459.05	D715	28.18	248	8.6	9.72
24003.64	-18548.4	-445.64	D715	19.23	411	12.6	13.7
24004.76	-18546.8	-462.73	D715	19.2	49.8	2.35	2.92
24004.9	-18546.6	-464.71	D715	17.28	48.9	1.65	5.84
24004.97	-18546.5	-465.71	D715	15.85	89.67	4.08	5.58
24004.45	-18547.3	-458.06	D715	11.09	313.1	10.23	15.7
24003.58	-18548.5	-444.65	D715	10.93	52.76	1.95	0.69
24004.83	-18546.7	-463.72	D715	10.77	245	6.39	5.66
24003.52	-18548.6	-443.65	D715	10.36	7.68	0.25	0
24003.19	-18549.1	-438.26	D715	10.11	231	8.27	10.7
24003.14	-18549.1	-437.44	D715	9.13	232.6	8.14	14.94
24002.74	-18549.7	-431	D715	6.45	164.5	5.59	8.78
24004.38	-18547.4	-457.07	D715	6.18	197.43	6.52	6.62
24004.21	-18547.6	-454.46	D715	5.35	441	11.9	9.54
24003.71	-18548.3	-446.63	D715	4.97	312.9	9.21	18.92
24000.48	-18553	-399.08	D715	4.81	455.3	14.55	17.57
24000.56	-18552.9	-400.07	D715	4.05	355	12	1.56
24005.39	-18545.9	-471.66	D715	3.54	299.6	11.65	21.02
24003.75	-18548.3	-447.28	D715	3.39	302	8.83	19.5
24005.32	-18546	-470.67	D715	3.37	484.75	18.13	17.13
24004.16	-18547.7	-453.74	D715	3.07	602.15	16.47	16.56
24000.63	-18552.8	-401.06	D715	2.71	465.4	18.32	16.95

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24000.71	-18552.7	-402.05	D715	2.54	343	12.1	1.72
24005.18	-18546.2	-468.68	D715	2.4	115	4.55	20.9
24005.25	-18546.1	-469.68	D715	2.31	191	7.18	17.76
24000.86	-18552.5	-404.03	D715	2.24	22.05	0.92	1.74
24004.62	-18547	-460.64	D715	2.16	123.5	3.49	5.68
24004.69	-18546.9	-461.64	D715	2	104.03	3.93	5.8
24004.73	-18546.9	-462.18	D715	1.99	103	3.95	5.81
24033.99	-18677.8	-389.21	D716	14.64	86.1	3.58	6.73
24033.61	-18677.8	-388.34	D716	11.87	307.62	11.04	8.07
24033.22	-18677.7	-387.43	D716	9.8	403.8	14.82	8.86
24032.83	-18677.6	-386.51	D716	5.1	514.2	15.6	6.65
24032.04	-18677.5	-384.67	D716	3.09	1140	27.2	1.23
24029.99	-18677.2	-379.91	D716	3.04	353.85	11.34	13.61
24032.43	-18677.6	-385.59	D716	2.19	581	15.8	5.1
24038.3	-18678.5	-399.26	D716	1.58	4.8	0.15	0.69
23955.74	-18232.8	-334.18	D718	11.86	244	8.9	11.2
23954.72	-18234	-336.25	D718	4.49	528	17.3	11.4
23954.96	-18233.7	-335.77	D718	4.28	505.2	16.67	12.77
23955.35	-18233.2	-334.98	D718	3.35	294.4	10.79	23.71
24049.83	-18508.3	-476.2	D719	4.36	123.33	6.59	5.67
23942.15	-18157.4	-318.29	D722	6.87	417.4	15.72	11.74
23945.41	-18158.5	-314.66	D722	6.34	155	5.93	14.7
23941.49	-18157.2	-319.02	D722	6.21	442.2	16.96	11.5
23944.76	-18158.3	-315.38	D722	5.09	260	9.83	14
23940.84	-18157	-319.74	D722	4.98	452.6	17.34	16.64
23939.52	-18156.6	-321.19	D722	4.93	501.9	18.69	8.16
23940.18	-18156.8	-320.47	D722	4.9	280.8	10.8	17.55
23938.21	-18156.2	-322.64	D722	4.79	434.6	15.16	11.96
23936.92	-18155.8	-324.05	D722	4.7	385	13.2	14.4
23942.8	-18157.6	-317.57	D722	4.65	339.6	12.66	11.88
23944.1	-18158.1	-316.11	D722	4.26	419.8	15.9	14.78
23938.87	-18156.4	-321.92	D722	4.2	714	25.96	8.2
23937.55	-18156	-323.37	D722	4.13	583.75	20.48	13.65
23943.45	-18157.8	-316.84	D722	3.52	465.6	17.62	14.48
23932.15	-18173.6	-297.53	D724	53.07	164	5.73	4.65
23936.6	-18173.9	-294.49	D724	47.11	186	6.53	7.57
23936.11	-18173.9	-294.83	D724	47.11	186	6.53	7.57
23931.33	-18173.5	-298.1	D724	44.06	163	5.44	7.6
23930.71	-18173.5	-298.52	D724	44.06	163	5.44	7.6
23973.47	-18648.6	-364.25	D725	13.1	18.3	0.57	1.63
23976.76	-18646	-388.99	D725	12.48	237.88	7.92	2.58
23973.6	-18648.5	-365.24	D725	12.14	20.4	0.59	4.79
23977.51	-18645.4	-394.71	D725	7.24	2.82	0.07	0.06

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23976.89	-18645.9	-389.98	D725	6.77	452.5	16.02	4.07
23977.14	-18645.7	-391.85	D725	5.55	207	6.15	6.93
23977.02	-18645.8	-390.96	D725	5.19	270.75	8.65	4.98
23973.73	-18648.4	-366.22	D725	4.8	3.6	0.14	5.88
23977.38	-18645.5	-393.73	D725	4.11	31.47	1.12	1.15
23974	-18648.2	-368.19	D725	3.7	12.3	0.51	0.42
23977.64	-18645.3	-395.7	D725	3.51	3.9	0.17	0.24
23974.38	-18647.9	-371	D725	3.5	20.1	0.8	0.34
23976.63	-18646.1	-388.01	D725	3.3	112.95	0.45	2.19
23977.25	-18645.6	-392.74	D725	2.4	43.8	1.57	1.63
23978.4	-18644.7	-401.63	D725	2.23	11.1	0.49	1.16
23978.02	-18645	-398.66	D725	1.61	18.6	0.84	2.71
23974.13	-18648.1	-369.18	D725	1.58	16.35	0.63	0.55
23978.53	-18644.6	-402.61	D725	1.47	3.46	0.15	0.17
23974.26	-18648	-370.16	D725	1.09	78.15	2.91	0.24
23975.28	-18647.1	-377.75	D725	1.05	0.2	0	0
24086.79	-18613.1	-473.42	D727	2.37	239	8.92	23.9
24086.62	-18613.1	-477	D727	2.19	236	7.55	9.05
24086.74	-18613.1	-474.42	D727	1.76	258.53	9.91	21.48
24086.65	-18613.1	-476.42	D727	1.29	134.58	4.33	5.18
23898.12	-18579.1	-329.32	D728	4.6	12.72	0.41	0.87
23898.08	-18579.3	-330.3	D728	2.95	12	0.48	3.37
23898.16	-18578.9	-328.34	D728	1.71	137.38	1.04	0.78
23898.4	-18577.7	-322.46	D728	1.37	46.5	1.05	0.43
23898.04	-18579.5	-331.28	D728	1.3	10.5	0.43	1.1
24085.06	-18584.5	-462.79	D731	37.51	282	10.5	3.35
24085.13	-18584.6	-461.82	D731	25.71	317	11.5	2.36
24088.06	-18589.9	-416.98	D731	16.52	152.2	5	11.73
24088.12	-18590.1	-415.99	D731	14.38	126	4.22	5
24088.17	-18590.2	-415	D731	11.42	288	9.78	6.72
24088	-18589.8	-417.97	D731	11.21	138.01	4.39	10.22
24085.2	-18584.7	-460.83	D731	9.46	429	15.4	13.8
24087.96	-18589.7	-418.79	D731	3.77	51.8	1.44	16.85
24088.25	-18590.3	-413.61	D731	2.46	270.32	9.57	1.74
24087.06	-18588	-433.49	D731	2.36	136.68	4.88	4.81
24086.8	-18587.6	-437.45	D731	1.3	121.07	4.41	5.65
24086.86	-18587.7	-436.46	D731	1.16	115.75	4.31	5.54
24085.27	-18584.9	-459.84	D731	1.1	884	31.2	18.25
23915.45	-17918.7	-209.69	D734	12.14	146	4.03	9.38
23915.77	-17918.3	-211.83	D734	10.66	188.5	4.97	5.33
23915.85	-17918.2	-212.34	D734	10.66	188.5	4.97	5.33
23915.92	-17918.1	-212.85	D734	2.74	124.64	4.32	2.17
23916.65	-17917.3	-217.73	D734	2.71	0.9	0.01	0.03

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23915.6	-17918.5	-210.66	D734	2.54	15	0.53	1.87
23915.69	-17918.4	-211.25	D734	2.54	15	0.53	1.87
23916.79	-17917.1	-218.7	D734	2.5	1.35	0.03	0.01
23916.94	-17916.9	-219.67	D734	2.43	1.5	0.03	0
23915.22	-17919	-208.13	D734	2.3	29.2	1.09	0.32
23916.5	-17917.4	-216.75	D734	2.21	2.33	0.06	0.05
23916.07	-17918	-213.83	D734	1.03	2.4	0.39	0.04
24108.95	-18570.7	-402.72	D735	11.52	1.2	0.03	0.02
24108.96	-18570.5	-403.7	D735	11.52	1.2	0.03	0.02
24109.1	-18567.8	-415.77	D735	4.73	464	13.3	4.9
24109.1	-18568	-415.01	D735	3.02	240	9.42	19.8
24109.08	-18568.2	-414.04	D735	1.37	773	26.8	20.6
24109.07	-18568.4	-413.06	D735	1.23	152	24	28.5
24109.45	-18560.7	-448.79	D735	1.16	148.27	3.39	3.18
23983.77	-17878.5	-230.78	D736	25.92	83.1	3.03	0.18
23983.74	-17878.4	-228.78	D736	25.85	68.4	3.14	5.18
23983.75	-17878.5	-229.78	D736	24.79	133	4	2.89
23983.87	-17878.5	-236.75	D736	21.22	74.4	3.11	6.47
23983.85	-17878.5	-235.78	D736	17.38	50.4	2.59	5.63
23983.84	-17878.5	-234.78	D736	15.61	29.28	1.63	2.7
23983.82	-17878.5	-233.78	D736	14.83	52.32	2.4	1.25
23983.79	-17878.5	-231.78	D736	13.51	38.79	1.52	0.15
23983.8	-17878.5	-232.78	D736	10.41	38.07	1.67	0.47
23983.72	-17878.4	-227.83	D736	1.17	3.3	0.22	0.24
23983.71	-17878.4	-226.88	D736	1.06	2.99	0.2	0.22
23959.41	-17899.4	-228.91	D737	27.05	34.2	0.85	6.62
23968.18	-17894.6	-239.66	D737	23.11	56.1	2.14	8.6
23968.57	-17894.4	-240.14	D737	23.11	56.1	2.14	8.6
23967.58	-17894.9	-238.93	D737	22.77	51.69	1.95	8.88
23958.81	-17899.8	-228.18	D737	21.46	43.8	1.13	2.57
23956.43	-17901.1	-225.25	D737	17.54	74.64	2.88	3.33
23960.01	-17899.1	-229.64	D737	16.17	29.52	0.87	3.84
23958.22	-17900.1	-227.45	D737	14.19	212	5.49	9.01
23966.99	-17895.2	-238.2	D737	13.61	19.35	0.76	2.81
23957.62	-17900.4	-226.72	D737	12.48	140	3.94	6.57
23965.2	-17896.2	-236	D737	8.37	4.14	0.2	0.21
23955.83	-17901.4	-224.52	D737	7.75	50.7	1.86	1.19
23964.6	-17896.6	-235.27	D737	6.83	15.42	0.54	0.55
23966.39	-17895.6	-237.47	D737	6.67	4.41	0.19	0.1
23960.6	-17898.8	-230.37	D737	5.86	7.2	0.25	0.66
23961.11	-17898.5	-230.99	D737	5.86	7.2	0.25	0.66
23954.04	-17902.4	-222.33	D737	5.81	200.25	6.03	7
23955.24	-17901.8	-223.79	D737	5.77	35.82	1.41	1.16

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23965.79	-17895.9	-236.73	D737	5.11	4.05	0.12	0.08
23964	-17896.9	-234.54	D737	4.25	23.1	0.72	0.72
23954.64	-17902.1	-223.06	D737	3.17	37.98	1.2	1.04
23968.95	-17894.1	-240.61	D737	1.99	30.6	1.06	0.28
23969.55	-17893.8	-241.34	D737	1.99	30.6	1.06	0.28
23963.41	-17897.2	-233.81	D737	1.41	12.24	0.51	0.49
23961.62	-17898.2	-231.62	D737	1.23	3.9	0.13	0.07
23909.95	-17888.8	-205.57	D738	10.8	108	2.68	7.25
23910	-17887.5	-206.94	D738	7.29	271.66	8.12	7.91
23909.93	-17889.5	-204.85	D738	6.23	19.26	0.49	1.16
23910.22	-17882	-212.65	D738	5.92	4.98	0.07	0.1
23910.2	-17882.7	-211.93	D738	5.05	4.13	0.06	0.08
23910.03	-17886.8	-207.59	D738	3.98	4.5	0.3	0.36
23910.14	-17884.1	-210.48	D738	2.06	0.9	0.03	0.04
23910.11	-17884.8	-209.76	D738	1.98	1.07	0.04	0.04
24114.96	-18555.7	-410.22	D739	3.05	620	15.1	9.04
24114.93	-18556	-409.28	D739	2.89	488.9	16.91	16.79
23980.9	-17862.9	-235.6	D741	46.29	45.17	1.81	5.86
23980.91	-17863	-234.66	D741	42.97	10.98	1.24	1.66
23980.94	-17863.4	-232.69	D741	28.06	65.04	11.9	0.53
23980.93	-17863.2	-233.68	D741	23.04	22.44	4.24	0.27
23980.96	-17863.6	-231.71	D741	13.99	44.4	7.11	0.39
23980.88	-17862.7	-236.53	D741	4.94	16.8	2.04	0.85
23980.87	-17862.5	-237.52	D741	1.51	5.67	0.63	0.31
23575.8	-17754.3	-59.98	D742	32.31	230.8	2.54	4.86
23575.7	-17754.3	-62.71	D742	16.8	158.5	0.88	6.88
23575.76	-17754.3	-60.98	D742	13.06	95.88	1.23	2.38
23575.73	-17754.3	-61.98	D742	12.05	109.45	0.87	4.46
23575.83	-17754.3	-58.98	D742	9.09	151	6.27	2.6
23575.23	-17754.3	-76.42	D742	2.81	10.5	0.05	0.06
23575.2	-17754.3	-77.42	D742	2.7	7.86	0.04	0.05
23575.16	-17754.3	-78.42	D742	2.54	3.9	0.03	0.03
23575.51	-17754.3	-68.43	D742	2.52	15.3	0.12	1.22
23575.47	-17754.3	-69.43	D742	2.44	6.06	0.05	1.07
23575.68	-17754.3	-63.43	D742	2.33	13.2	0.04	0.27
23575.54	-17754.3	-67.43	D742	2.3	22.5	0.18	1.12
23575.64	-17754.3	-64.43	D742	2.11	15	0.05	0.29
23575.44	-17754.3	-70.43	D742	1.99	3	0.04	0.7
23575.34	-17754.3	-73.43	D742	1.99	3.9	0.03	0.04
23575.3	-17754.3	-74.43	D742	1.99	3.9	0.03	0.04
23575.58	-17754.3	-66.43	D742	1.89	20.52	0.12	0.65
23575.61	-17754.3	-65.43	D742	1.61	19.2	0.08	0.34
24139.96	-18580.2	-469.58	D744	10.49	470	17.6	7.21

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24140.1	-18580.1	-470.57	D744	8.09	296	9.63	18.8
23554.77	-17732.1	-43.07	D745	46.73	104	3.37	2.71
23549.87	-17727.9	-50.69	D745	46.39	157	9.39	5.01
23550.37	-17728.3	-49.93	D745	40.85	116.28	9.14	5.85
23553.33	-17730.8	-45.35	D745	34.46	151	6.21	1.56
23554.29	-17731.6	-43.83	D745	32.56	118.4	6.38	3.39
23549.37	-17727.5	-51.45	D745	29.27	435.4	11.5	10.4
23550.87	-17728.7	-49.17	D745	26.16	106.32	7.33	7.52
23553.81	-17731.2	-44.59	D745	23.11	128	8.39	3.84
23549.09	-17727.3	-51.87	D745	17.86	621	12.9	14
23551.37	-17729.1	-48.4	D745	12.17	173.8	4.74	6.67
23552.36	-17729.9	-46.88	D745	11.9	97.47	2.85	3.46
23552.84	-17730.4	-46.12	D745	9.43	97.2	3.03	5.4
23551.86	-17729.5	-47.64	D745	6.21	153.75	3.97	4.37
23548.81	-17727.1	-52.29	D745	1.82	18.6	0.8	0.78
23548.3	-17726.7	-53.06	D745	1.82	18.6	0.8	0.78
23970.13	-17857.4	-232.18	D746	37.92	76.8	2.88	14
23970.29	-17857.7	-231.23	D746	31.68	50.1	1.96	0.17
23970.62	-17858.2	-229.32	D746	22.53	10.5	0.4	0.19
23970.79	-17858.5	-228.37	D746	20.23	1000	26.1	8.18
23970.96	-17858.7	-227.42	D746	19.54	254	8.45	4.33
23970.46	-17857.9	-230.28	D746	14.61	24.6	0.77	0.12
23969.98	-17857.2	-233.04	D746	14.33	115	3.96	6.99
23578.09	-17728.3	-71.31	D747	2.16	6.9	0.04	0.1
23578.11	-17728	-72.25	D747	2.16	6.9	0.04	0.1
23578.26	-17723.8	-83.52	D747	1.52	2.08	0.03	0.51
23578.17	-17726.2	-76.94	D747	1.23	1.2	0.01	0.16
23578.23	-17724.9	-80.7	D747	1.23	1.8	0.03	0.2
23577.99	-17730.8	-64.76	D747	1.13	11.7	0.09	0.17
23578.19	-17725.9	-77.88	D747	1.02	0.7	0.01	0.14
23578.21	-17725.2	-79.76	D747	1.02	1	0.02	0.16
23620.05	-17722	-67.6	D748	29.31	182.5	0.69	1.03
23620.43	-17721.7	-68.17	D748	29.31	182.5	0.69	1.03
23619.54	-17722.4	-66.83	D748	20.71	483	0.47	2.41
23619.04	-17722.8	-66.07	D748	15.65	1681.5	1.79	2.77
23617.27	-17724.2	-63.39	D748	10.9	33.9	0.82	0.98
23618.53	-17723.2	-65.3	D748	10.59	2880	3.12	3.12
23616.76	-17724.6	-62.62	D748	7.8	95.45	0.47	0.58
23616.25	-17725	-61.85	D748	4.7	157	0.13	0.18
23620.81	-17721.4	-68.75	D748	4.11	43.2	0.08	0.32
23621.32	-17721	-69.51	D748	2.06	21.7	0.05	0.17
23617.77	-17723.8	-64.15	D748	1.78	60.9	0.06	0.33
23618.15	-17723.5	-64.73	D748	1.78	60.9	0.06	0.33

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24145.09	-18650.8	-463.64	D749	5.59	253	8.94	6.89
23597.46	-17739.4	-65.67	D750	21.26	39.3	0.58	1.89
23598.91	-17738.3	-70.33	D750	20.67	169	0.46	1.68
23597.75	-17739.2	-66.61	D750	5.38	229	0.32	0.55
23598.04	-17739	-67.54	D750	5.38	229	0.32	0.55
23598.33	-17738.8	-68.47	D750	1.44	8.4	0.04	0.2
23598.62	-17738.5	-69.4	D750	1.44	8.4	0.04	0.2
23600.94	-17760.1	-70.51	D753	42.96	701.9	3.64	3.57
23600.63	-17760	-69.56	D753	8.59	134.85	0.72	0.75
24084.44	-18645.9	-451.01	D755	8.4	14.4	0.44	5.62
24083.61	-18647.2	-463.37	D755	8.09	137	4.96	6.92
24084.18	-18646.3	-454.98	D755	6.34	12.82	0.61	5.63
24084.11	-18646.4	-455.98	D755	5.97	14.1	0.58	6.78
24083.54	-18647.3	-464.36	D755	5.76	93	3.63	7.8
24084.05	-18646.5	-456.97	D755	5.55	21.9	0.81	10.65
24084.25	-18646.2	-453.99	D755	5.05	7.13	0.35	3.71
24083.91	-18646.7	-458.95	D755	4.66	35.4	1.49	8.01
24083.87	-18646.8	-459.5	D755	4.66	35.4	1.49	8.01
24084.9	-18645.2	-444.06	D755	4.52	490.59	16.74	10.57
24084.96	-18645.1	-443.07	D755	4.46	31.71	1	16.42
24085.28	-18644.6	-438.11	D755	4.32	367	12.7	5.49
24085.15	-18644.8	-440.09	D755	3.67	116.77	4.13	5.74
24085.03	-18645	-442.08	D755	3.48	70.02	2.44	13.25
24083.98	-18646.6	-457.96	D755	3.38	44.85	1.73	13.48
24084.83	-18645.3	-445.06	D755	3.27	358.4	11.88	20.08
24084.7	-18645.5	-447.04	D755	3.17	36.42	1.13	14.82
24084.64	-18645.6	-448.04	D755	3.17	34.5	1.13	19
24085.09	-18644.9	-441.09	D755	2.88	108.48	3.85	6.02
24084.38	-18646	-452.01	D755	2.77	3.83	0.12	1.44
24084.57	-18645.7	-449.03	D755	2.13	22.71	0.76	14.17
24084.77	-18645.4	-446.05	D755	2.07	79.41	2.43	15.68
24083.22	-18647.7	-468.88	D755	2.04	12.81	0.39	0.8
24084.31	-18646.1	-453	D755	1.81	1.58	0.08	0.82
24086.15	-18643.1	-424.21	D755	1.47	401.14	14.91	6.9
24085.22	-18644.7	-439.1	D755	1.11	86.12	2.98	1.65
23558.09	-17765.1	-63.19	D756	1.17	115	0.08	0.19
23557.77	-17765.2	-64.12	D756	1.17	115	0.08	0.19
23573.68	-17721.4	-44.53	D757	30.38	221	5.58	0.91
23573.64	-17721.1	-44.96	D757	30.38	221	5.58	0.91
23573.37	-17718.2	-48.48	D757	3.7	81.6	0.46	0.69
23573.02	-17714.5	-53.13	D757	3.33	9.3	0.69	0.71
23573.43	-17718.9	-47.71	D757	2.9	58.83	0.38	1
23572.96	-17713.8	-53.9	D757	2.33	6.57	0.49	0.5

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23573.31	-17717.6	-49.26	D757	2.12	42.12	0.2	0.75
23573.26	-17717	-50.03	D757	1.44	25.2	0.09	0.77
23573.08	-17715.1	-52.35	D757	1.12	4.05	0.23	0.42
23855.6	-17746.1	-142.97	D758	21.19	204	5.82	2.97
23855.54	-17746.1	-143.91	D758	19.61	165	5.89	6.11
24066.48	-18592	-456.34	D759	13.58	56.5	1.91	5.43
24065.73	-18591.4	-462.52	D759	12.75	190	6.97	0.83
24071.69	-18596.2	-412.66	D759	12	153	5.08	5.64
24071.57	-18596.1	-413.64	D759	11.57	208.8	6.9	11.18
24071.46	-18596.1	-414.63	D759	11.09	264.5	9.48	5.67
24070.87	-18595.6	-419.58	D759	11.07	89.98	3.05	16.77
24066.36	-18591.9	-457.33	D759	10.39	202	6.44	6.7
24070.78	-18595.5	-420.37	D759	10.29	118	4.02	13.95
24070.99	-18595.7	-418.59	D759	10.21	82.98	2.64	14.05
24071.34	-18596	-415.62	D759	8.39	225.9	7.63	7.61
24071.1	-18595.8	-417.6	D759	8.39	43.74	1.44	21.54
24066.24	-18591.8	-458.32	D759	7.37	613	19.55	8.72
24071.22	-18595.9	-416.61	D759	7.12	81.99	2.69	9.58
24066.12	-18591.7	-459.31	D759	5.21	825	26.8	12.8
24071.92	-18596.4	-410.78	D759	2.55	17.39	0.58	4.13
24070.45	-18595.2	-423.14	D759	1.06	17.2	0.33	1.06
24070.34	-18595.2	-424.12	D759	1.06	17.2	0.33	1.06
24007.83	-18744.9	-296.16	D761	12.34	45.3	1.07	0.62
24007.83	-18744.9	-308.86	D761	12.2	104.6	2.42	6.82
24007.83	-18744.9	-304.36	D761	9.43	436.8	14.48	6.54
24007.83	-18744.9	-306.36	D761	9.36	210	8.23	13.7
24007.83	-18744.9	-307.11	D761	9.36	210	8.23	13.7
24007.83	-18744.9	-297.16	D761	8.65	32.07	0.75	0.44
24007.83	-18744.9	-301.36	D761	5.52	700	23	8.49
24007.83	-18744.9	-303.36	D761	5.46	515.2	18.24	4.57
24007.83	-18744.9	-302.36	D761	3.15	378	14.6	1.93
24007.83	-18744.9	-309.86	D761	3.12	22.5	0.76	0.9
24007.83	-18744.9	-310.86	D761	1.98	9.67	0.3	0.46
24007.83	-18744.9	-311.86	D761	1.65	6	0.17	0.33
24120.64	-18688.6	-467.84	D765	71.69	292	4.74	4.31
24120.26	-18688.8	-466.93	D765	62.19	110.5	6.81	10.3
24121.02	-18688.4	-468.75	D765	46.9	64.5	3.34	8.2
24115.29	-18690.9	-455.1	D765	11.59	158	5.82	10.2
24128.46	-18685.3	-486.49	D765	9.84	36.9	0.97	3.35
24119.88	-18688.9	-466.02	D765	6.75	32.1	1.41	2.79
24118.35	-18689.6	-462.38	D765	6.58	37.5	1.31	4.78
24116.82	-18690.2	-458.74	D765	6.17	57.9	1.75	10.2
24114.91	-18691	-454.19	D765	6.1	51.9	1.87	3.5

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24116.44	-18690.4	-457.83	D765	5.9	214	0.4	1.56
24115.67	-18690.7	-456.01	D765	5.73	145	4.82	10.5
24119.49	-18689.1	-465.11	D765	4.97	112.5	3.86	4.78
24118.73	-18689.4	-463.29	D765	4.36	154.3	5.18	17.44
24128.85	-18685.1	-487.4	D765	4.22	5.7	0.19	0.24
24129.23	-18685	-488.31	D765	4.14	17.58	0.69	1.18
24121.4	-18688.3	-469.66	D765	3.91	41.1	1.59	1.99
24119.11	-18689.3	-464.2	D765	3.81	183.5	6.15	20.6
24129.61	-18684.8	-489.22	D765	3.46	124.5	5.18	9.69
24129.86	-18684.7	-489.81	D765	3.46	124.5	5.18	9.69
24127.51	-18685.7	-484.22	D765	2.81	35.4	1.51	3.38
24127.13	-18685.8	-483.31	D765	1.87	20.55	0.87	1.91
24123.31	-18687.5	-474.21	D765	1.28	93.75	3	1.63
24123.69	-18687.3	-475.12	D765	1.06	46.8	1.82	2.79
24124.07	-18687.1	-476.03	D765	1.06	46.8	1.82	2.79
23830.68	-17703.4	-130.89	D766	25.54	326	11	12.8
23830.48	-17703.1	-131.83	D766	24	63	2.9	6.38
23830.08	-17702.5	-133.71	D766	20.95	145.5	3.5	17.6
23830.88	-17703.6	-129.95	D766	18.69	177.5	4.86	4.79
23830.28	-17702.8	-132.77	D766	17.59	71.7	1.28	22.7
23829.9	-17702.3	-134.56	D766	11.79	476	11.7	15.2
23831.86	-17705	-125.35	D766	8.78	12.3	0.05	0.07
23831.7	-17704.8	-126.1	D766	8.78	12.3	0.05	0.07
24129.53	-18750.9	-413.76	D769	12.66	5.22	0.13	0.11
24128.51	-18750.8	-412.14	D769	11.81	58.82	2.08	2.96
24128.01	-18750.7	-411.36	D769	11.55	60.17	2.28	1.2
24127.48	-18750.6	-410.52	D769	11.33	192.96	7.52	4.75
24129	-18750.8	-412.92	D769	9.53	10.5	0.33	0.43
24130.07	-18750.9	-414.61	D769	7.52	12.81	0.43	0.46
24126.95	-18750.6	-409.67	D769	6.88	126.89	5.13	1.62
24130.6	-18751	-415.45	D769	2.67	20.1	0.71	0.81
24147.42	-18753	-441.41	D769	1.59	3.48	0.05	0.03
24131.14	-18751.1	-416.29	D769	1.24	10.36	0.34	0.38
23806.87	-17741.2	-119.34	D770	8.4	9.3	0.28	0.17
23806.51	-17741.1	-120.27	D770	8.4	9.3	0.28	0.17
23806.15	-17741.1	-121.21	D770	5.88	6.57	0.2	0.12
23878.01	-17795.7	-161.39	D771	47.86	51.6	2.46	3.09
23878.07	-17795.9	-162.36	D771	47.86	51.6	2.46	3.09
23878.26	-17796.6	-165.05	D771	22	203	10.61	5
23878.21	-17796.4	-164.3	D771	21.42	179.35	9.45	4.64
23878.14	-17796.2	-163.33	D771	18.1	45.3	2.85	2.6
23877.31	-17793.3	-151.3	D771	13.58	51.9	1.87	1.99
23877.25	-17793	-150.33	D771	11.73	69.6	2.14	0.73

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23876.75	-17791.3	-143.05	D771	10.99	12.27	0.94	0.4
23877.38	-17793.5	-152.27	D771	9.06	251.64	8.03	0.5
23876.81	-17791.5	-144.02	D771	8.98	101.5	2.98	0.29
23877.44	-17793.7	-153.16	D771	8.71	267	8.5	0.38
23433.46	-17759.7	-19.54	D773	9.67	224	5.13	18.9
23433.46	-17759.7	-18.61	D773	8.16	163.5	3.56	6.05
23515.41	-17760.7	-37.21	D776	88.03	73.06	2.25	3.96
23514.54	-17760.8	-37.7	D776	66.74	119.19	4.47	2.11
23513.67	-17760.9	-38.18	D776	56.76	133.8	4.47	4.34
23512.8	-17760.9	-38.67	D776	49.39	171.7	5.39	8.25
23499.88	-17761.9	-45.84	D776	41.76	30.3	0.56	1.62
23519.77	-17760.4	-34.79	D776	22.56	200	5.96	0.04
23500.41	-17761.8	-45.55	D776	21.91	22.05	0.52	0.95
23507.43	-17761.3	-41.65	D776	19.89	144	5.22	1.81
23506.97	-17761.4	-41.9	D776	19.89	144	5.22	1.81
23511.92	-17761	-39.15	D776	17.44	306.6	9.61	11.95
23517.16	-17760.6	-36.24	D776	11.74	299.5	7.31	15.66
23516.28	-17760.7	-36.73	D776	11.31	331	8.52	22
23518.03	-17760.5	-35.76	D776	11.24	258.24	6.13	11.69
23510.55	-17761.1	-39.92	D776	10.9	206	5.74	25.7
23511.05	-17761.1	-39.64	D776	10.69	232.4	6.71	23.09
23498.49	-17762	-46.62	D776	9.79	11.25	0.69	0.69
23497.62	-17762	-47.1	D776	7.55	8.7	0.5	0.53
23508.3	-17761.3	-41.17	D776	5.02	39.75	1.34	0.48
23518.9	-17760.5	-35.27	D776	5.01	8.4	0.2	0.36
23510.05	-17761.1	-40.2	D776	3.05	9.6	0.51	0.34
23509.18	-17761.2	-40.68	D776	2.3	8.45	0.4	0.26
23496.74	-17762.1	-47.59	D776	1.65	2.1	0.09	0.1
23499.36	-17761.9	-46.13	D776	1.27	1.8	0.16	0.05
23495.87	-17762.1	-48.07	D776	1.24	1.8	0.06	0.13
23519.2	-17795.1	-71.93	D777	9.91	299	0.83	1.24
23541.78	-17779.9	-46.37	D777	6.82	31.69	2	2.43
23540.15	-17781	-48.22	D777	6.46	211.85	5.44	2.31
23517.54	-17796.2	-73.82	D777	3.02	140.5	0.43	0.26
23522.06	-17793.2	-68.67	D777	2.42	48.39	0.09	0.84
23523.78	-17792	-66.71	D777	2.26	7.8	0.06	0.21
23523.22	-17792.4	-67.35	D777	2.26	7.8	0.06	0.21
23524.39	-17791.6	-66.03	D777	1.89	21.06	0.03	0.21
23524.99	-17791.2	-65.34	D777	1.69	17	0.1	0.39
23541.18	-17780.3	-47.06	D777	1.61	95.7	0.99	0.45
23540.57	-17780.7	-47.75	D777	1.61	95.7	0.99	0.45
23522.66	-17792.8	-67.98	D777	1.58	37.8	0.04	0.22
23516.94	-17796.6	-74.51	D777	1.51	70.35	0.22	0.14

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23526.2	-17790.4	-63.98	D777	1.44	5.1	0.24	0.73
23525.59	-17790.8	-64.66	D777	1.44	5.1	0.24	0.73
23521.46	-17793.6	-69.35	D777	1.32	174.85	0.14	0.6
23535.49	-17784.1	-53.49	D777	1.19	4.8	0.03	0.44
23440.67	-17753.6	-19.69	D778	13.23	303	7.56	16.15
23441.25	-17753.1	-19.05	D778	12.17	298.5	7.22	15.6
23441.74	-17752.6	-18.51	D778	6.14	273	5.28	12.45
23438.91	-17765.5	-21.62	D780	15.43	41.7	1.27	12.7
23440.5	-17767.2	-19.75	D780	12.41	623	13.35	6.78
23440.87	-17767.6	-19.32	D780	12.41	623	13.35	6.78
23438.37	-17764.9	-22.24	D780	12.14	472	9.08	18.95
23439.44	-17766.1	-21	D780	12.07	336	9.3	12.6
23439.97	-17766.6	-20.38	D780	11.42	797	22.3	5.75
23442.3	-17769.2	-17.64	D780	2.87	82.2	1.22	0.51
23442.83	-17769.7	-17.01	D780	2.86	81.24	1.21	0.5
23978.09	-18773.4	-245.64	D781	1.03	0.9	0.01	0.08
24126.41	-18717.7	-481.3	D784	12.82	299	10	10
24126.4	-18717.7	-482.3	D784	12.07	440	16.85	5.19
24127.06	-18717.8	-444.1	D784	10.63	10.5	0.28	4.43
24126.43	-18717.7	-480.3	D784	7.95	791	30	12.85
24126.38	-18717.7	-483.29	D784	7.68	296	9.91	4.13
24127.04	-18717.8	-445.1	D784	7.67	15.36	0.55	4.28
24126.36	-18717.7	-484.29	D784	7.41	1055	37.3	9.75
24127.03	-18717.8	-445.65	D784	7.34	15.9	0.58	4.26
24126.89	-18717.8	-453.8	D784	6.11	33.18	1.17	10.96
24127.18	-18717.8	-437.03	D784	5.07	3.4	14.1	8.18
24126.88	-18717.8	-454.7	D784	4.35	48.3	1.6	16.5
24126.33	-18717.7	-486.29	D784	3.98	714	23.6	8.72
24126.91	-18717.8	-452.8	D784	3.96	32.97	1.06	5.58
24127.08	-18717.8	-443.1	D784	3.63	44.7	1.52	11.8
24126.31	-18717.7	-487.29	D784	2.88	362	13.9	15
24126.94	-18717.8	-450.8	D784	2.33	12.9	0.55	3.03
24126.62	-18717.7	-469.6	D784	1.16	112.32	4.14	3.99
24126.34	-18717.7	-485.29	D784	1.1	119	4.26	26
23987.24	-17918.4	-239.06	D785	33.53	169	4.75	12.9
23987.29	-17918.9	-239.92	D785	28.18	77.7	1.7	5.3
23987.34	-17919.4	-240.79	D785	28.18	77.7	1.7	5.3
23987.18	-17917.9	-238.19	D785	23.73	370	10.15	7.24
23986.8	-17914.5	-232.16	D785	21.42	122.69	4.02	9.17
23986.74	-17914	-231.29	D785	20.38	134.2	4.09	16.47
23986.68	-17913.5	-230.42	D785	17.89	209.07	6.38	18.66
23987.07	-17916.9	-236.45	D785	16.87	49.5	1.76	12.3
23987.13	-17917.4	-237.32	D785	12.48	295	7.4	11.85

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
23986.85	-17914.9	-233	D785	11.59	12.3	0.81	7.35
23986.9	-17915.4	-233.85	D785	3.63	6.3	0.61	0.56
23986.96	-17915.9	-234.72	D785	3.5	6.07	0.58	0.54
23986.64	-17913.1	-229.75	D785	1.85	15.3	0.55	0.57
23987.02	-17916.4	-235.59	D785	1.1	1.8	0	0.12
23986.6	-17912.7	-229.08	D785	1.02	9.15	0.3	0.33
23948.97	-17843.4	-209.67	D787	4.05	72.9	4.51	3.14
23948.6	-17843	-210.17	D787	4.05	72.9	4.51	3.14
23924.23	-17818	-195.42	D788	76.19	239	5.08	10.95
23924.77	-17818.5	-195.15	D788	53.83	157.87	3.44	8.24
23931.34	-17825.3	-191.91	D788	25.66	145.5	4.31	5.7
23930.68	-17824.6	-192.23	D788	13.49	62.55	1.98	4.29
23927.4	-17821.2	-193.85	D788	11.59	408.27	10.99	4.26
23926.74	-17820.6	-194.18	D788	9.45	303.98	8.55	3.12
23925.43	-17819.2	-194.83	D788	8.71	9.51	0.42	2.73
23930.03	-17824	-192.56	D788	3.17	8.72	0.26	0.27
23926.09	-17819.9	-194.5	D788	3.04	54.29	1.71	1.64
23929.37	-17823.3	-192.88	D788	2.05	10.3	0.22	0.23
23961.9	-17863.7	-225.99	D791	35.61	70.43	2.43	8.69
23962.21	-17863.9	-225.06	D791	35.37	84.15	2.64	7.82
23961.65	-17863.6	-226.71	D791	34.63	85.5	2.97	9.44
23962.52	-17864.1	-224.12	D791	23.6	231.63	7.16	10.39
23962.84	-17864.3	-223.19	D791	16.87	143.5	4.29	5.72
23853.28	-17849.7	-165.47	D792	3.02	9.9	0.3	0.22
23852.29	-17849.5	-165.44	D792	1.97	6.51	0.2	0.15
23926.57	-17842.6	-197.8	D793	32.71	364	8.81	17.75
23928.95	-17845.4	-196.03	D793	28.36	5.28	0.16	0.76
23930.05	-17846.6	-195.25	D793	24.69	57.6	1.99	3.64
23930.57	-17847.1	-194.89	D793	23.15	108.72	3.27	3.74
23925.5	-17841.2	-198.65	D793	16.5	628.9	17.44	8.84
23928.36	-17844.8	-196.45	D793	13.24	3.06	0.1	0.44
23934.27	-17850.4	-192.48	D793	10.81	208.89	6.23	6.13
23926.03	-17841.9	-198.23	D793	10.69	366.85	12.22	20.36
23933.59	-17849.8	-192.9	D793	6.02	116.3	3.47	3.42
23924.98	-17840.5	-199.07	D793	4.69	234.7	6.6	3.32
23929.54	-17846	-195.61	D793	2.5	4.8	0.14	0.37
23924.68	-17840.1	-199.32	D793	2.47	160	4.59	2.58
23931.1	-17847.6	-194.53	D793	1.68	2.1	0.05	0.1
23931.64	-17848.1	-194.17	D793	1.51	1.14	0.07	0.09
23932.28	-17848.7	-193.75	D793	1.48	0.93	0.07	0.09
24109.42	-18727.8	-469.02	D795	9.98	14.7	0.36	0.46
24115.5	-18725.9	-416.31	D795	9.87	7.2	0.18	3.24
24109.67	-18727.8	-467.04	D795	8.88	6.9	0.12	0.16

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24109.55	-18727.8	-468.03	D795	8.88	6.9	0.12	0.16
24108.65	-18728.1	-474.96	D795	8.66	155.34	5.3	1.33
24108.39	-18728.1	-476.95	D795	7.91	113.4	3.62	7.93
24108.52	-18728.1	-475.95	D795	7.39	121.8	4.23	3.84
24115.39	-18725.9	-417.3	D795	6.99	14.34	0.47	4.19
24115.28	-18725.9	-418.24	D795	5.76	17.4	0.6	4.6
24109.29	-18727.9	-470.01	D795	5.56	7.74	0.22	0.46
24108.91	-18728	-472.98	D795	5.42	161.5	6.35	4.75
24108.78	-18728	-473.97	D795	4.32	48.86	1.82	1.59
24109.17	-18727.9	-471	D795	3.88	12.51	0.47	1.23
24109.04	-18728	-471.99	D795	3.81	29.92	1.17	1.88
24108.26	-18728.2	-477.94	D795	3.56	316.7	11.44	14.48
24114.6	-18726.1	-424.35	D795	3.22	45.6	1.67	2.17
24114.49	-18726.1	-425.34	D795	3.22	45.6	1.67	2.17
24114.84	-18726	-422.17	D795	2.38	3.96	0.09	0.12
23954.24	-17932.2	-234.96	D798	3.14	5.1	0.41	0.13
23954.25	-17932.3	-235.96	D798	2.67	6.24	0.46	0.14
23974.9	-17968.4	-241.68	D805	2.54	5.4	0.13	0.55
23975.47	-17968.1	-242.44	D805	1.53	3.32	0.08	0.33
23809.13	-17726.1	-115.47	D806	32.63	99.09	4.02	1.46
23809.13	-17726	-119.1	D806	29.9	89.4	4.35	0.61
23809.13	-17726	-118.47	D806	25.78	154.84	4.17	0.72
23809.13	-17726	-117.47	D806	17.91	219.41	3.43	0.82
23809.13	-17726.1	-113.47	D806	12.34	115	3.62	2.37
23809.13	-17726.3	-103.87	D806	10.75	232.55	4.96	4.71
23809.13	-17726.1	-116.47	D806	8.3	29.1	0.81	0.43
23809.13	-17726.1	-114.47	D806	4.91	20.06	0.66	0.62
23809.13	-17726.1	-112.67	D806	4.77	2.1	0.08	0.23
23809.13	-17726.3	-104.87	D806	2.79	35.33	0.88	0.98
23809.13	-17726.1	-111.87	D806	2.64	1.95	0.08	0.17
23809.13	-17726.3	-101.87	D806	1.17	89.13	3.7	0.14
24161.46	-18782.8	-416.83	D820	21.67	5	0.01	0.03
24161.46	-18782.8	-417.53	D820	21.67	5	0.01	0.03
24161.46	-18782.8	-468.13	D820	14.19	48.56	1.31	1.71
24161.46	-18782.8	-469.13	D820	11.5	75.11	2.7	2.23
24161.46	-18782.8	-489.58	D820	9.94	51.79	1.81	13.71
24161.46	-18782.8	-473.13	D820	9.87	12.19	0.4	1.89
24161.46	-18782.8	-488.58	D820	9.87	74.48	2.81	6.91
24161.46	-18782.8	-467.13	D820	9.73	45.65	1.67	0.53
24161.46	-18782.8	-470.13	D820	8.98	265.96	1.4	1.26
24161.46	-18782.8	-490.58	D820	8.9	70.95	2.63	17.91
24161.46	-18782.8	-487.58	D820	7.93	108.2	4.16	12.18
24161.46	-18782.8	-463.13	D820	7.66	14.15	0.31	1.09

LOCATION X	LOCATION Y	LOCATION Z	HOLE-ID	Au g/t	Ag g/t	Pb %	Zn %
24161.46	-18782.8	-492.58	D820	7.18	119.51	4.56	8.56
24161.46	-18782.8	-491.58	D820	6.73	96.49	3.7	14.14
24161.46	-18782.8	-474.08	D820	5.92	36.38	1.4	8.5
24161.46	-18782.8	-493.58	D820	5.7	112.92	4.24	6.5
24161.46	-18782.8	-495.58	D820	5.34	22.75	0.89	2.96
24161.46	-18782.8	-465.13	D820	5.14	31.4	1.28	1.24
24161.46	-18782.8	-472.13	D820	5.03	10	0.3	0.68
24161.46	-18782.8	-499.58	D820	4.88	49.18	1.87	4.18
24161.46	-18782.8	-471.13	D820	4.46	7.15	0.2	0.32
24161.46	-18782.8	-494.58	D820	4.24	60.08	2.19	4.75
24161.46	-18782.8	-498.58	D820	4.24	162	5.78	6.06
24161.46	-18782.8	-464.13	D820	4.12	6.55	0.22	0.24
24161.46	-18782.8	-500.58	D820	3.5	25.1	0.98	10.32
24161.46	-18782.8	-496.58	D820	3.18	26.55	1.04	2.28
24161.46	-18782.8	-413.93	D820	3.11	106.5	4.26	2.96
24161.46	-18782.8	-432.23	D820	2.96	3.88	0.01	0.04
24161.46	-18782.8	-501.38	D820	2.58	26.3	1.06	14.94
24161.46	-18782.8	-466.13	D820	2.54	31.42	1.28	0.47
24161.46	-18782.8	-413.03	D820	2.48	953.85	32.11	10.05
24161.46	-18782.8	-419.23	D820	2.46	8	0.27	0.44
24161.46	-18782.8	-497.58	D820	2.43	166.72	5.72	4.47
24161.46	-18782.8	-515.73	D820	1.97	176.3	6.41	[19.7
24161.46	-18782.8	-509.08	D820	1.87	76.7	2.98	25.14
24161.46	-18782.8	-515.08	D820	1.85	165.07	6.02	18.36
24161.46	-18782.8	-510.08	D820	1.78	219	8.58	19.88
24161.46	-18782.8	-433.23	D820	1.67	70.69	2.93	2.88
24161.46	-18782.8	-418.23	D820	1.65	4.68	0.17	0.08
24161.46	-18782.8	-511.08	D820	1.65	323.8	13.68	15.05
24161.46	-18782.8	-507.08	D820	1.44	13.5	0.39	2.87
24161.46	-18782.8	-456.23	D820	1.36	3.95	0.01	0.22
24161.46	-18782.8	-513.08	D820	1.31	130.5	5.33	22.11
24161.46	-18782.8	-512.08	D820	1.22	159.8	6.94	18.23